	SCOUR ANALYSIS AND REPORTING FORM							
	Bridge Structure No. 43043180 Date 10/10/11 Initials Ch. Region (ABCD)							
	Site Location $\frac{1}{2}$ m; $\frac{1}{2}$ Mai F of Vivian on 239 Ave $Q_{100} = \frac{1}{4}$ 760 by: drainage area ratio flood freq. anal regional regression eq.							
	Q <sub>100</sub> = 7/60 by: drainage area ratio flood freq. anal. regional regression eq.							
	Bridge discharge $(Q_2) = \underline{4760}$ (should be $Q_{100}$ unless there is a relief bridge, road overflow, or bridge overtopping)							
	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method							
	Bridge Width = 64 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °							
PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"	Width $(W_2)$ iteration = $64$							
Reg	Avg. flow depth at bridge, $y_2$ iteration = $10.4 + Vert - Wall$							
A", '	Corrected channel width at bridge Section = $W_2$ times cos of flow angle = $63$ , $6$ ft* $q_2 = Q_2/W_2 = \frac{14}{2}$ , $\frac{1}{2}$ ft <sup>2</sup> /s							
gion or "F	Corrected channel width at bridge Section = $W_2$ times cos of flow angle = $63.76$ ft* $q_2 = Q_2/W_2 = 74.7$ ft²/s Bridge Vel, $V_2 = 7.2$ ft/s Final $y_2 = q_2/V_2 = 10.4$ ft $\Delta h = 1$ ft							
"Re	Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 1$ ft							
iRM	* NOTE: repeat above calculations until y $_2$ changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$							
PG "R	If y 2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,							
	Water Surface Elev. = ft							
	Low Steel Elev. = 13.7 ft 64 70							
	n  (Channel) = 0.050							
	n(LOB) = 0.050 $5.8$							
0.7	n (ROB) = 0.050 Pier Width = 1.3 ft							
1	Pier Length = $\frac{30}{100}$ ft							
4	# Piers for $100 \text{ yr} = $ ft							
	COMMUNICATION OF COMMUN							
4	CONTRACTION SCOUR							
	Width of main channel at approach section $W_1 = \frac{70}{4 + 6}$ ft							
ontra	Width of left overbank flow at approach, $W_{lob} = \frac{64}{64}$ ft Average left overbank flow depth, $y_{lob} = \frac{5}{64}$							
PGRM: Contract	Width of right overbank flow at approach, $W_{rob} = \cancel{64}$ ft Average right overbank flow depth, $y_{rob} = \cancel{5.8}$ f							
GR	Live Bed Contraction Scour (use if bed material is small cobbles or finer)							
144	$x = 9.30$ From Figure 9 $W_2$ (effective) = 61, 2 ft $y_{es} = 10, 3$ ft							
	$\underline{\underline{\hspace{1cm}}}$							
EW	Clear Water Contraction Scour (use if bed material is larger than small cobbles)							
CSN	Estimated bed material $D_{50} = ft$ Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = ft/s$ Critical approach velocity, $V_c = 11.17y_1^{1/6}D_{50}^{1/3} = ft/s$ If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.							
CW	Critical approach velocity, $Vc = 11.17y_1^{1/6}D_{50}^{1/3} = $ ft/s							
PGRM: CWCSNEW	If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.							
PG	$\begin{array}{lll} D_{e50} = 0.0006 (q_2/y_1^{7/6})^3 = \underline{\qquad} & \text{ft} & \text{If } D_{50} >= D_{e50},  \chi = 0.0 \\ \text{Otherwise, } \chi = 0.122 y_1 [q_2/(D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\qquad} & \text{From Figure 10, } y_{cs} = \underline{\qquad} & \text{ft} \end{array}$							
	Otherwise, $\chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 =ft$							
h								
f: Pi	PIER SCOUR CALCULATIONS  Correction for the form and the form Table 1) K2 = 1.5							
PGRM: Pier	El/a ratio = $23.1$ Correction factor for flow angle of attack (from Table 1), $K2 = 1.5$ Froude # at bridge = $0.39$ Using pier width a on Figure 11, $\xi = \underline{5.8}$ Pier scour $y_{ps} = \underline{7.6}$ ft							
Д	Trouble " at bridge 5.07 Cosing piet width a on Figure 11, $\zeta = 5$ . Fiet scout $y_{ps} = 77.8$ It							
Ħ	ABUTMENT SCOUR CALCULATIONS							
PGRM: Abutment	Average flow depth blocked by: left abutment, $y_{aLT} = 5$ ft right abutment, $y_{aRT} = 5$ ft Shape coefficient $K_1$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through							
f: Ab	Shape coefficient K <sub>1</sub> = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through							
GRN	Using values for $y_{aLT}$ and $y_{aRT}$ on figure 12, $\psi_{LT} = 16.5$ and $\psi_{RT} = 16.5$ Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 16.5$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 16.5$ ft							
Ъ.	Lett abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = \frac{70.55}{10.55}$ It Kight abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = \frac{70.55}{10.55}$ It							

Paula 739 Are Stroom MedicMa	14	MDM	De	10/10/	/// To:	tials C1			
Route 2) [ Five stream   Worlding		VIKIVI	Da	te 10/10/	11 Ini	mais			
Bridge Structure No. 43043180 Lo	cation /2	mit/2m	it of	Vivian	on 15	1 Arc			
Route 239 Ave Stream MedicMe  Bridge Structure No. 43043180 Lo  GPS coordinates: 43°56′03,2′′  W 100°16′45,0′′  Drainage area = \$7.3.2 cm	taken from: Datum of co	USL abutmen oordinates: Wo	d GS84	centerline o NAD27	f ii MRM	end			
Drainage area = 87.32 sq. mi.				_					
				77	0.0 1				
The average bottom of the main channel was $17.2$ ft below top of guardrail at a point $27$ ft from left abutment.									
Method used to determine flood flows:Freq. Analdrainage area ratioregional regression equations.									
MIGGRIA I ANDONO GOMOTORO ESTANO									
MISCELLANEOUS CONSIDERATIONS									
Flows		$Q_{100} = 4760$			$Q_{500} = 7976$				
Estimated flow passing through bridge	4760			7970					
Estimated road overflow & overtopping		N	D 21.1	17		I B 71			
Consideration	Yes	No	Possibly	Yes	No	Possibly			
Chance of overtopping Chance of Pressure flow		X			V				
		X			-				
Armored appearance to channel		X							
Lateral instability of channel		X			X				
Discount I was a second of the									
Riprap at abutments? Yes No Marginal Evidence of past Scour? Yes No Don't know 1. Abut									
Evidence of past Scour? YesNoDon't know L. Hout									
Debris Potential?HighHowLow									
Does scour countermeasure(s) appear to have been designed?									
Riprap Yes No Don't know NA									
Spur Dike Yes No Don't know NA									
Other YesNoDon't knowNA									
Bed Material Classification Based on Median Particle Size (D <sub>50</sub> )									
	1		dian Partic						
				Annual Control of the		Boulders			
Size range, in mm <0.062 0.062-2	.00	2.00-64		64-250		>250			
Comments, Diagrams & orientation of digital photos									
16/4/11 2099-10		06- Cha							
2017-10									
6 960 a100- us	2 318 5 960 01 - US RB 08 - US Face								
10 1160 01- US KB		08- US	tace						
25 2680 02- USLB									
60 3650 03- L. Abut S.	lows								
100 4760 AH 1 NL +									
500 7970									
Summary of Results 05 - R. Abut									
	Q100			Q500					
Bridge flow evaluated	4760			79.70					
Flow depth at left abutment (yaLT), in feet	5.8			9.7					
Flow depth at right abutment (yaRT), in feet	5,8			9.7					
Contraction scour depth (ycs), in feet	/	10.3			16.2				
Pier scour depth (yps), in feet	7,6			7, 7					
Left abutment scour depth (yas), in feet		16,5		Ċ	21,1				
Right abutment scour depth (yas), in feet	/	6.5		9	21.				
1Flow angle of attack	1			4					