

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 44006170 Date 6/29/12 Initials RT Region (A B C D) (D)  
 Site \_\_\_\_\_ Location 1 mi. E of Emery on 281 St  
 $Q_{100} =$   $Q_{100}$  1490 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1490 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

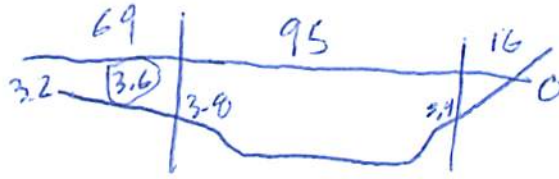
Bridge Width = 69 ft. Flow angle at bridge = 50 ° Abut. Skew = 0 ° Effective Skew = 50 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 44.35 ft\*  $q_2 = Q_2/W_2 =$  33.6 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  4.1 ft/s Final  $y_2 = q_2/V_2 =$  8.2 ft  $\Delta h =$  0.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  8.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 1.9 ft  
 Low Steel Elev. = 11.1 ft <sup>2.0</sup>  
 $n$  (Channel) = 0.040 <sup>1.3</sup>  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 1.35 ft  
 Pier Length = 1.35 ft  
 # Piers for 100 yr = 2 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  95 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  69 ft Average left overbank flow depth,  $y_{lob} =$  3.6 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  16 ft Average right overbank flow depth,  $y_{rob} =$  2.7 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  15.29 From Figure 9  $W_2$  (effective) = 46.7 ft  $y_{cs} =$  15.7 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use Clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.25 Using pier width  $a$  on Figure 11,  $\xi =$  6 Pier scour  $y_{ps} =$  4.8 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.6 ft right abutment,  $y_{aRT} =$  2.7 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  12.6 and  $\psi_{RT} =$  11  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  22.8 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  20.0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PGRM: Contract  
 PGRM: CWCNEW  
 PGRM: Pier  
 PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

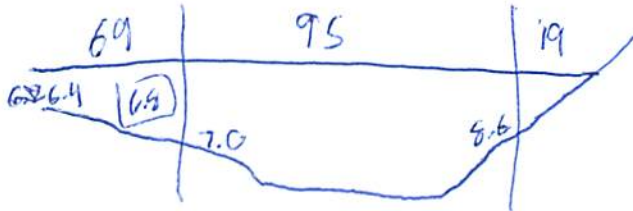
Bridge Structure No. 44006170 Date 6/29/12 Initials Ral Region (A B C D) D  
 Site 3070 Location 1.0 mi. E of Emory on 281 St  
 $Q_{500} =$  Q<sub>25</sub> 2749 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 2749 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 69 ft. Flow angle at bridge = 50 ° Abut. Skew = 0 ° Effective Skew = 50 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 44.35 ft\*  $q_2 = Q_2/W_2 =$  62 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  5.956 ft/s Final  $y_2 = q_2/V_2 =$  11.1 ft  $\Delta h =$  0.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  11.7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 1.9 ft  
 Low Steel Elev. = 4.1 ft  
 $n$  (Channel) = 0.070  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 1.35 ft  
 Pier Length = 1.35 ft  
 # Piers for 500 yr = 3



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  95 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  69 ft Average left overbank flow depth,  $y_{lob} =$  6.4 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  19 ft Average right overbank flow depth,  $y_{rob} =$  4.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  26.34 From Figure 9  $W_2$  (effective) = 40.3 ft  $y_{cs} =$  21.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.7 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.3 Using pier width  $a$  on Figure 11,  $\xi =$  6 Pier scour  $y_{ps} =$  5 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  6.9 ft right abutment,  $y_{aRT} =$  4.3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  18.2 and  $\psi_{RT} =$  13.8  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  33.1 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  25.1 ft

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment



43 600594  
97.595276

81556

43 36 2.13541  
97 35 42.99361

Route 281 St Stream Wolf ck MRM \_\_\_\_\_ Date 6/29/12 Initials Qaj  
 Bridge Structure No. 44006170 Location 1 mi. E of Emery on 281 St  
 GPS coordinates: N 43° 36' 2.3" taken from: USL abutment  centerline of  MRM end \_\_\_\_\_  
W 97° 35' 43.1" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 171.71 sq. mi.  
 The average bottom of the main channel was 14.7 ft below top of guardrail at a point 52 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	$Q_{100} = Q_{10}$ <u>1490</u>			$Q_{500} =$ <del>172</del> $Q_{25}$ <u>3070</u>		
Estimated flow passing through bridge	<u>1490</u>			<u>2749</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>321</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

6/14  
 2 | 173  
 5 | 725  
 10 | 1490  
 25 | 3070  
 50 | 4790  
 100 | 7060  
 500 | 14900

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal Some on outside left abutment  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know I believe the abutments used to be a spill way, lots of contraction & abutment scour.  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size ( $D_{50}$ )

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1). left ab  
 2). main channel  
 3). right ab  
 4). right abutment erosion  
 5). pier  
 6-8). right abutment  
 9). left abutment  
 10). left abutment  
 11). main channel

Summary of Results

	$Q_{100}$ $Q_{10}$	$Q_{500}$ $Q_{25}$
Bridge flow evaluated	<u>1490</u>	<u>2749</u>
Flow depth at left abutment (yaLT), in feet	<u>3.6</u>	<u>6.9</u>
Flow depth at right abutment (yaRT), in feet	<u>2.7</u>	<u>4.3</u>
Contraction scour depth (yca), in feet	<u>15.1</u>	<u>21.1</u>
Pier scour depth (ypr), in feet	<u>4.8</u>	<u>5</u>
Left abutment scour depth (yab), in feet	<u>22.8</u>	<u>4.3 33.1</u>
Right abutment scour depth (yab), in feet	<u>2.0</u>	<u>25.1</u>
Flow angle of attack	<u>50</u>	<u>50</u>

See Comments/Diagram for justification where required