

OK T2T

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 44095080 Date 6/18/12 Initials Dat Region (A B C D) D  
 Site \_\_\_\_\_ Location 1.3 mi W of Sakon on 252 St  
 $Q_{100} = Q_3$  655 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 655 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 35 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 30.31 ft\*  $q_2 = Q_2/W_2 = 21.6$  ft<sup>2</sup>/s

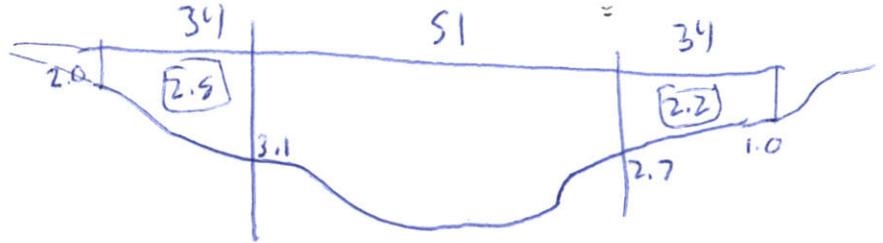
Bridge Vel,  $V_2 = 3.3$  ft/s Final  $y_2 = q_2/V_2 = 6.6$  ft  $\Delta h = 6.6 - 0.2$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 6.4$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 1.0 ft  
 Low Steel Elev. = 9.1 ft  
 $n$  (Channel) = 0.033  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.035  
 Pier Width = 1.35 ft  
 Pier Length = 1.35 ft  
 # Piers for 100 yr = 1



#### CONTRACTION SCOUR

3.1 2.0

Width of main channel at approach section  $W_1 = 51$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 34$  ft Average left overbank flow depth,  $y_{lob} = 2.8$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 34$  ft Average right overbank flow depth,  $y_{rob} = 2.2$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer) *see notes*  
 $x = 8.32$  From Figure 9  $W_2$  (effective) = 29 ft  $y_{cs} = 9.2$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.23 Using pier width  $a$  on Figure 11,  $\xi = 6$  Pier scour  $y_{ps} = 4.8$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 2.8$  ft right abutment,  $y_{aRT} = 2.2$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 11.2$  and  $\psi_{RT} = 9$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = 20.3$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = 16.4$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 44095080 Date 6/18/12 Initials hoj Region (A B C D) 0  
 Site \_\_\_\_\_ Location 1.3 mi. w of Salem on 252 St  
 $Q_{500} = 640$  1320 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1260 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 35 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 35 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 30.31 ft\*  $q_2 = Q_2/W_2 = 41.6$  ft<sup>2</sup>/s

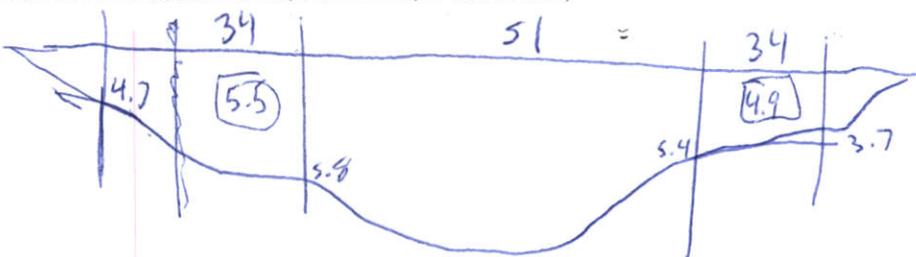
Bridge Vel,  $V_2 = 4.6$  ft/s Final  $y_2 = q_2/V_2 = 9.1$  ft  $\Delta h = 0.4$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 9.5$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 1.0 ft  
 Low Steel Elev. = 9.1 ft  
 $n$  (Channel) = 0.033  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.035  
 Pier Width = 1.35 ft  
 Pier Length = 1.35 ft  
 # Piers for 500 yr = 1 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 51$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 34$  ft Average left overbank flow depth,  $y_{lob} = 5.5$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 34$  ft Average right overbank flow depth,  $y_{rob} = 4.9$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 15.65$  From Figure 9  $W_2$  (effective) = 29 ft  $y_{cs} = 15.3$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.27 Using pier width  $a$  on Figure 11,  $\xi = 6$  Pier scour  $y_{ps} = 4.9$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 5.5$  ft right abutment,  $y_{aRT} = 4.9$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 15.9$  and  $\psi_{RT} = 14.8$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = 28.9$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = 27$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

Route 252 St Stream W Fk Vermillion River MRM \_\_\_\_\_ Date 6/16/12 Initials kat  
 Bridge Structure No. 44095080 Location 1.3 mi W of Salem on 252 St  
 GPS coordinates: N 43° 43' 53.91" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 97° 25' 16.5" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 137.68 sq. mi.  
 The average bottom of the main channel was 13.6 ft below top of guardrail at a point 23 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

137.67  
 6/18  
 8/24

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = Q <sub>5</sub> <u>655</u>			Q <sub>500</sub> = Q <sub>10</sub> <u>1320</u>		
Estimated flow passing through bridge	<u>655</u>			<u>1260</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>60</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

2 | 159  
 5 | 655  
 10 | 1320  
 25 | 2720  
 50 | 4220  
 100 | 6190  
 500 | 12900

Riprap at abutments?  Yes \_\_\_ No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *very minor contraction/abutment. maybe some pier*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA *rose quartz around abutment*  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No  Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)  
 Material Silt/Clay  Sand  Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1) left ab  
 2) main channel  
 3) right ab  
 4-5) left abutment  
 6) pier  
 7) creek  
 8-9) right abutment  
 10) main channel

Note: fair amount of riprap in main channel under bridge. consider clear water scours.

Summary of Results

	Q <sub>100</sub> <u>5</u>	Q <sub>500</sub> <u>10</u>
Bridge flow evaluated	<u>655</u>	<u>1260</u>
Flow depth at left abutment (yaLT), in feet	<u>2.8</u>	<u>5.5</u>
Flow depth at right abutment (yaRT), in feet	<u>2.2</u>	<u>4.9</u>
Contraction scour depth (yca), in feet	<u>9.2</u>	<u>8 15.3</u>
Pier scour depth (yps), in feet	<u>4.8</u>	<u>4.9</u>
Left abutment scour depth (yas), in feet	<u>20.3</u>	<u>28.9</u>
Right abutment scour depth (yas), in feet	<u>16.4</u>	<u>27</u>
Flow angle of attack	<u>30</u>	<u>30</u>

See Comments/Diagram for justification where required

