| | SCOUR ANALYSIS AND REPORTING FORM | | | | | | |
|--|--|--|--|--|--|--|--|
| | Bridge Structure No. 47/16360 Date 9-19-12 Initials PFT Region (ABCD) | | | | | | |
| | Site Location 1,2 m; No F HWY 34 on Nike Mile Rd | | | | | | |
| | Q ₁₀₀ = 974 by: drainage area ratio flood freq. anal. regional regression eq. | | | | | | |
| | Bridge discharge $(Q_2) = Q74$ (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping) | | | | | | |
| | Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method | | | | | | |
| | Bridge Width = 107 ft. Flow angle at bridge = 7 ° Abut. Skew = 0 ° Effective Skew = 7 ° | | | | | | |
| | Width (W_2) iteration = 71 72 | | | | | | |
| OnD | Avg. flow depth at bridge, y_2 iteration = 3.0 3.0 | | | | | | |
| Regi | Corrected channel width at bridge Section = W_2 times cos of flow angle = $71.4 L$ ft* $q_2 = Q_2/W_2 = 13.L$ ft²/s | | | | | | |
| 01 | Bridge Vel, $V_2 = 4.5$ ft/s Final $y_2 = q_2/V_2 = 3.0$ ft $\Delta h = 0.4$ ft | | | | | | |
| nC", | Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 3.4$ ft | | | | | | |
| legic | * NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L\sin(q) + a\cos(q)$ | | | | | | |
| - | If y ₂ is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD, | | | | | | |
| | Water Surface Elev. = dry ft high left bank (no enclose flow) | | | | | | |
| | Low Steel Elev. = 9,6 ft | | | | | | |
| | $n \text{ (Channel)} = \frac{0.045}{0.0000}$ | | | | | | |
| | $ \begin{array}{c} \text{n (LOB)} = \\ \text{n (ROB)} = \\ \hline \end{array} \begin{array}{c} \text{0 50} \\ \text{0 65} \end{array} $ | | | | | | |
| | Pier Width = 0.8 ft | | | | | | |
| | Pier Length = 0.83 ft | | | | | | |
| | # Piers for 100 yr = \underline{Z} ft | | | | | | |
| | CONTRACTION SCOUR | | | | | | |
| | Width of main channel at approach section $W_1 = 7\lambda$ ft | | | | | | |
| | Width of left overbank flow at approach, $W_{lob} = $ ft Average left overbank flow depth, $y_{lob} = $ ft | | | | | | |
| | Width of right overbank flow at approach, $W_{rob} = 0$ ft Average right overbank flow depth, $y_{rob} = 0$ ft | | | | | | |
| | Live Bed Contraction Scour (use if bed material is small cobbles or finer) | | | | | | |
| | $x =$ ft $y_{cs} =$ ft | | | | | | |
| | | | | | | | |
| | Clear Water Contraction Scour (use if bed material is larger than small cobbles) | | | | | | |
| | Estimated bed material $D_{50} = ft$ Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = ft/s$ Critical approach velocity, $V_2 = \frac{11.17y_1^{1/6}D_{50}^{1/3}}{11.17y_1^{1/6}D_{50}^{1/3}} = \frac{ft}{11.17y_1^{1/6}D_{50}^{1/3}} = \frac{ft}{11.17y_1^{1/$ | | | | | | |
| | If $V \le V$ and $D_{xx} = 0.2$ ft. use clear water equation below, otherwise are live had score equation above. | | | | | | |
| | If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above. $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3$ If $D_{50} >= D_{c50}$, $\chi = 0.0$ | | | | | | |
| | | | | | | | |
| | Otherwise, $\chi = 0.122 y_1 [\dot{q}_2/(D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =ft$ | | | | | | |
| | PIER SCOUR CALCULATIONS | | | | | | |
| L/a ratio = $\frac{1}{1}$ Correction factor for flow angle of attack (from Table 1), K2 = $\frac{1}{1}$ Using pier width a on Figure 11, $\xi = 3$, $\frac{1}{2}$ Pier scour $y_{rs} = 3$. | | | | | | | |
| | L/a ratio = $\frac{1}{1}$ Correction factor for flow angle of attack (from Table 1), K2 = $\frac{1}{1}$ Froude # at bridge = $\frac{1}{1}$ Using pier width a on Figure 11, $\xi = \frac{1}{1}$ Pier scour $y_{ps} = \frac{1}{1}$ ft | | | | | | |
| | ABUTMENT SCOUR CALCULATIONS | | | | | | |
| | Average flow depth blocked by: left abutment, $y_{aLT} = 0$ ft right abutment, $y_{aRT} = 0$ ft Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through | | | | | | |
| | Snape coefficient K ₁ = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through | | | | | | |
| | Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = $ | | | | | | |
| | Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = $ transfer abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = $ ft | | | | | | |

PGRM: "RegionA", "RegionB",

PGRM: Contract

PGRM: CWCSNEW

PGRM: Abutment PGRM: Pier

| Route Mine Mile Rd Stream Spring (| ck | MRM | Dat | e | Ini | tials | | | | |
|---|--|----------------|-----------------|-------------|-------------|-------------|------|--------|--|--|
| Bridge Structure No. 4711 0380 Lo | eation 12 | mi N | of Hall | × 34 | n 1/0 | w M.1. | EL | | | |
| GPS coordinates 440 29.420' | taken from: | USL abutmer | 0 11 00/ | contarling | of I MDM | e / 4/e 1 | (a) | | | |
| W 103° 20.813' | | oordinates: W | | | | | | | | |
| Drainage area = 66.75 sq. mi. | | | | | | | | | | |
| The average bottom of the main channel was | 3.7 ft belov | w top of guard | rail at a point | 25 | ft from le | ft abutment | | | | |
| Method used to determine flood flows:Freq | | | | | | | | | | |
| | | | | | ression equ | ations. | | | | |
| | SCELLANE | EOUS CONSI | DERATION | IS - | | | 7/ | 3 | | |
| Flows | $Q_{100} =$ | 974 | | $Q_{500} =$ | 1870 | | > 1 | 14.4 | | |
| Estimated flow passing through bridge | | 974 | | | 1870 | | 3 | 159 | | |
| Estimated road overflow & overtopping | | O | | | . 0 | | 10 | 159 | | |
| Consideration | Yes | No | Possibly | Yes | No | Possibly | 25 | 459 | | |
| Chance of overtopping | | V | | | V | | 50 | 698 | | |
| Chance of Pressure flow | | V . | | | V | | | 974 | | |
| Armored appearance to channel | | V | | | V | 1 | 500 | 1870 | | |
| Lateral instability of channel | | | V | | | = 1 | | | | |
| | | | | | | | | 1 | | |
| | No | | | | | E THE E | | | | |
| Evidence of past Scour? X Yes | No | Don't know | v contrac | tion suc | DUT 100 | ol (dry) | und | ler br | | |
| Evidence of past Scour? X Yes Debris Potential? High | X_Med | _Low tre | es upst | ream, | some à | lebris | on p | rsier | | |
| | | | • | , | | | | | | |
| Does scour countermeasure(s) appear to have been | the state of the s | | | | | | | | | |
| RiprapY | esN | loDo | n't know | NA | | | | | | |
| Spur Dike Y | es N | loDo | n't know | ✓ NA | | | | | | |
| • | | lo Do | | - | | | | | | |
| 1 | <u> </u> | | - Literature | V_III | | | | | | |
| Bed Material | Classification | n Based on M | edian Particle | Size (Dec) | ř. | | | | | |
| Bed Material Classification Based on Median Particle Size (D ₅₀) | | | | | | | | | | |
| Material Silt/Clay X Sand Gravel Cobbles Boulders Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250 Some cobbles in bottom of low-flow channel, but the rest is fines | | | | | | | | | | |
| Size range, in mm <0.062 0.062-2 | .00 | 2.00-64 | \ \ | 64-250 | 1 | >250 | | | | |
| Comments, Diagrams & orientation of digital pho | m o + 10 | ow-tlow | channel, | , but t | the res | it is ti | ne s | | | |
| Str.no- | | 1 (1 -1 | | | | | | | | |
| | | left ak | | | | | | | | |
| approach from bridge | | rt. ak | out. | | | | | | | |
| high left bank | | 1 1 1 | | | | | | | | |
| DOB Com boidge | | debris | on pi | 61 | | | | | | |
| 700 | | | 1 | | | | | | | |
| approach from bridge high left bank ROB from bridge bridge from approach | | | | | | | | | | |
| Summary of Results | | | | | | | | | | |
| | To the second | Q100 | | | Q500 | | 1 | | | |
| Bridge flow evaluated | | 974 | |) | 870 | | 1 | | | |
| Flow depth at left abutment (yaLT), in feet | | 0 0 | | | | | 1 | | | |
| Flow depth at right abutment (yaRT), in feet 0 0 | | | | | | | | | | |
| Contraction scour depth (ycs), in feet | | D | | | 0.2 | | 1 | | | |
| Pier scour depth (yps), in feet | | 3.5 | | | 3.6 | | 1 | | | |
| Left abutment scour depth (yas), in feet | | 0 | | | 0 | | 1 | | | |
| Right abutment scour depth (yas), in feet | | | | | | | 1 | | | |
| | I | D | | | 1,4 | | 1 | | | |