

ok-RAT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 47.363476 Date 9-19-12 Initials RFT Region (A B C D) B  
 Site \_\_\_\_\_ Location ~2.5 mi E + 2.7 mi S of Hereford on New Underwood Rd  
 $Q_{100} = 51900$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 51900 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

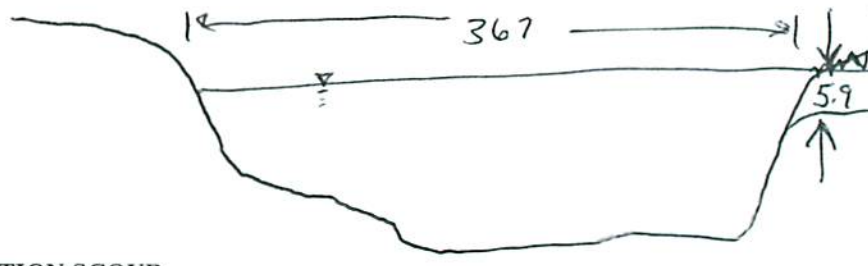
#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 352 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 286 314 318  
 Avg. flow depth at bridge,  $y_2$  iteration = 16.6 15.8 15.7  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 316.79 ft\*  $q_2 = Q_2/W_2 = 163.8$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 10.5$  ft/s Final  $y_2 = q_2/V_2 = 15.7$  ft  $\Delta h = 2.2$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 17.9$  ft

\*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.  
road overflow occurs at  $y_2 \approx 26$  south of bridge

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = \_\_\_\_\_ ft  
 n (Channel) = .025  
 n (LOB) = .030  
 n (ROB) = .030  
 Pier Width = 2.0 ft  
 Pier Length = 23.0 ft  
 # Piers for 100 yr = 3



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 367$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 0$  ft Average left overbank flow depth,  $y_{lob} = 0$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 352$  ft Average right overbank flow depth,  $y_{rob} = 5.9$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 5.89$  From Figure 9  $W_2$  (effective) = 310.8 ft  $y_{cs} = 6.6$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 1.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 11.5 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1.5$   
 Froude # at bridge = 0.47 Using pier width a on Figure 11,  $\xi = 8$  Pier scour  $y_{ps} = 10.7$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 0$  ft right abutment,  $y_{aRT} = 5.9$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 0$  and  $\psi_{RT} = 16.6$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 0$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 16.6$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

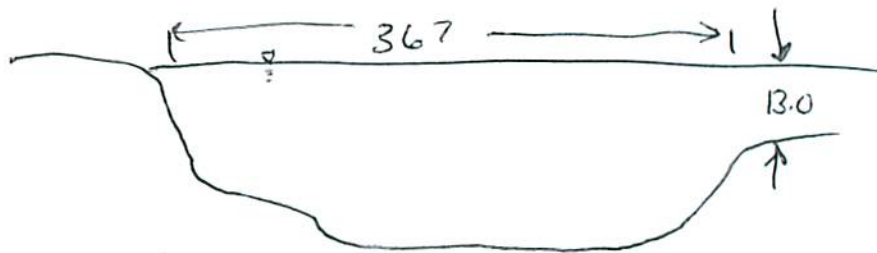
Bridge Structure No. 47363476 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D) B  
 Site \_\_\_\_\_ Location ~2.5 mi E + 2.7 mi S of Hereford on New Underwood Rd  
 $Q_{500} = 98400$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 98400 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 352 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 352 340 342  
 Avg. flow depth at bridge,  $y_2$  iteration = 20.8 21.2 21.1  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 340.7 ft\*  $q_2 = Q_2/W_2 = 288.8$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 13.7$  ft/s Final  $y_2 = q_2/V_2 = 21.1$  ft  $\Delta h = 3.9$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 25.0$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = \_\_\_\_\_ ft  
 n (Channel) = .025  
 n (LOB) = .030  
 n (ROB) = .030  
 Pier Width = 2.0 ft  
 Pier Length = 23 ft  
 # Piers for 500 yr = 3 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 367$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 0$  ft Average left overbank flow depth,  $y_{lob} = 0$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 352$  ft Average right overbank flow depth,  $y_{rob} = 13.0$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 9.78$  From Figure 9  $W_2$  (effective) = 334.7 ft  $y_{cs} = 10.7$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 1.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [(q_2/(D_{50}^{1/3} y_1^{7/6}))^{6/7} - 1] =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 11.5 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1.5$   
 Froude # at bridge = 0.53 Using pier width a on Figure 11,  $\xi = 8$  Pier scour  $y_{ps} = 10.9$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 0$  ft right abutment,  $y_{aRT} = 13.0$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 0$  and  $\psi_{RT} = 23.8$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 0$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 23.8$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment



Route New Underwood Rd Stream Belle Fourche Rv MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 47363476 Location ~2.5 mi E + 2.7 mi S of Hereford on New Underwood Rd  
 GPS coordinates: N 44° 21.062' taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 102° 50.247' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 6369.06 sq. mi.

The average bottom of the main channel was 35.4 ft below top of guardrail at a point 75 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>51900</u>			Q <sub>500</sub> = <u>98400</u>		
Estimated flow passing through bridge	<u>51900</u>			<u>98400</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>

7/2  
 2 | 2960  
 5 | 9320  
 10 | 16500  
 25 | 27200  
 50 | 38300  
 100 | 51900  
 500 | 98400

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour? \_\_\_ Yes  No \_\_\_ Don't know  
 Debris Potential? \_\_\_ High  Med \_\_\_ Low

no riprap, but old road grade on rt. side may protect abut.

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Str. no  
 approach from bridge  
 high left bank from bridge  
 ROB from bridge  
 Bridge from left

left abut. from under bridge  
 right abut. from left downstream

Summary of Results

	Q <sub>100</sub>	Q <sub>500</sub>
Bridge flow evaluated	<u>51900</u>	<u>98400</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>5.9</u>	<u>13.0</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>6.6</u>	<u>10.7</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>10.7</u>	<u>10.9</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>0</u>	<u>0</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>16.6</u>	<u>23.8</u>
lFlow angle of attack	<u>5°</u>	<u>5°</u>

See Comments/Diagram for justification where required