

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 47379444 Date 8/11/11 Initials CW Region (A B C D) B  
 Site \_\_\_\_\_ Location 5 mi NE of Hereford on New Underwood Rd  
 $Q_{100} =$  36100 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 36100 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

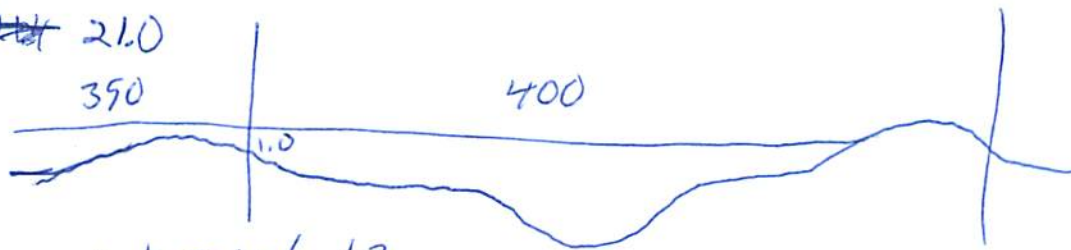
#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 390 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = 390 258 343 301 340 301 340  
 Avg. flow depth at bridge,  $y_2$  iteration = 12.0 15.0 12.9 13.8 12.9 13.4 13.4  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = ~~390~~ ft \* 0.983  $Q_2 = Q_2/W_2 =$  113.8 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.8 ft/s Final  $y_2 = q_2/V_2 =$  12.9 ft  $\Delta h =$  1.6 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  14.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = ~~222.4~~ 210 ft  
 $n$  (Channel) = 0.033  
 $n$  (LOB) = 0.037  
 $n$  (ROB) = 0.037  
 Pier Width = 3.0 ft  
 Pier Length = 3.0 ft  
 # Piers for 100 yr = 4 ft



Different sized piers → just use largest or make equivalent?

#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  400 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  390 ft Average left overbank flow depth,  $y_{lob} =$  1.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0.0 ft Average right overbank flow depth,  $y_{rob} =$  0.0 ft

PGRM: Contract

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  3.26 From Figure 9  $W_2$  (effective) = 328 ft  $y_{cs} =$  4.0 ft  
3.65 322.4 4.3

PGRM: CWCSNEW

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

PGRM: Pier

#### PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.43 Using pier width  $a$  on Figure 11,  $\xi =$  10.7 Pier scour  $y_{ps} =$  2.4 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  1.0 ft right abutment,  $y_{aRT} =$  0.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  4.3 and  $\psi_{RT} =$  0.0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  4.3 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  0.0 ft

PGRM: Abutment

2  
1.6  
1.7  
3.6  
6.1  
26.2  
6.1  
-2.1  
2.4  
1.5  
5.1  
6.6  
2.4  
9.0

**SCOUR ANALYSIS AND REPORTING FORM**

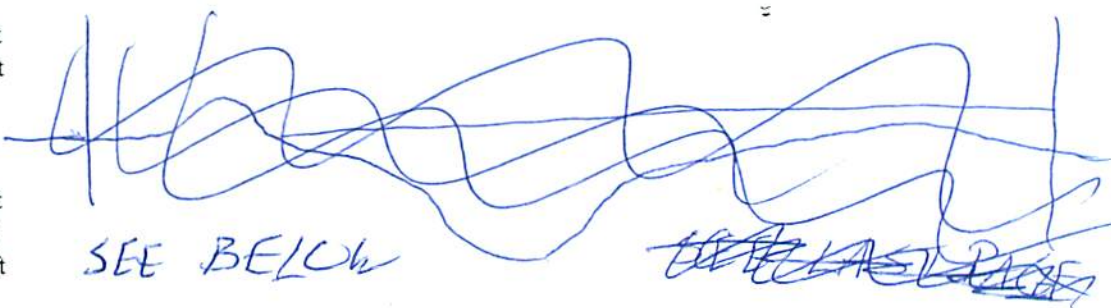
Bridge Structure No. 47378444 Date 8/11/11 Initials CW Region (A B C D) B  
 Site \_\_\_\_\_ Location 5 mi NE of Hereford on New Underwood Rd  
 $Q_{500} =$  98000 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 94000 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 390 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = 390  
 Avg. flow depth at bridge,  $y_2$  iteration = 19.8 → vert wall  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 384.08 ft\*  $q_2 = Q_2/W_2 =$  256.2 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  12.9 ft/s Final  $y_2 = q_2/V_2 =$  19.8 ft  $\Delta h =$  3.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  23.2 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 210 ft  
 $n$  (Channel) = 0.033  
 $n$  (LOB) = 0.037  
 $n$  (ROB) = 0.037  
 Pier Width = 3.0 ft  
 Pier Length = 3.0 ft  
 # Piers for 500 yr = 4 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  400 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  390 ft Average left overbank flow depth,  $y_{lob} =$  9.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  390 ft Average right overbank flow depth,  $y_{rob} =$  7.8 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  9.74 From Figure 9  $W_2$  (effective) = 372.1 ft  $y_{cs} =$  10.7 ft

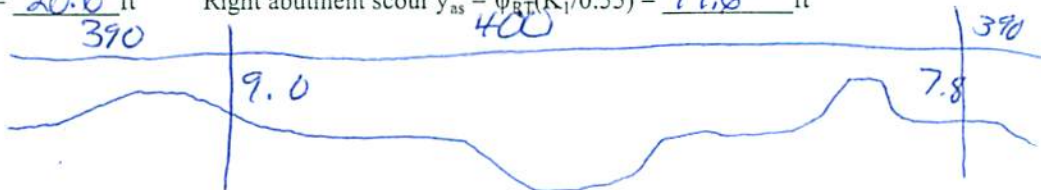
Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{cs0} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{cs0}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.51 Using pier width  $a$  on Figure 11,  $\xi =$  10.7 Pier scour  $y_{ps} =$  9.7 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  9.0 ft right abutment,  $y_{aRT} =$  7.8 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  20.6 and  $\psi_{RT} =$  19.6  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  20.6 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  19.6 ft



PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

2.12  
14.5  
8.17

Route New Underwood Rd Stream West Elm Ck MRM \_\_\_\_\_ Date 8/11/11 Initials Cu  
 Bridge Structure No. 47348444 Location 5 mi NE of Hereford on New Underwood Rd  
 GPS coordinates: N 44° 23' 54.7" taken from: USL abutment X centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 102° 48' 31.2" Datum of coordinates: WGS84 X NAD27 \_\_\_\_\_

Drainage area = 392 sq. mi.  
 The average bottom of the main channel was 23.2 ft below top of guardrail at a point 137 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>38100</u>			Q <sub>500</sub> = <u>98000</u>		
Estimated flow passing through bridge	<u>38100</u>			<u>98000</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<u>X</u>				<u>X</u>
Chance of Pressure flow		<u>X</u>		<u>X</u>		<u>X</u>
Armored appearance to channel		<u>X</u>			<u>X</u>	
Lateral instability of channel		<u>X</u>			<u>X</u>	

pk calcd 8/8  
 PK2 706  
 5 2870  
 10 6200  
 25 14100  
 50 23800  
 100 38100  
 500 98000

Riprap at abutments? \_\_\_ Yes X No \_\_\_ Marginal  
 Evidence of past Scour? X Yes \_\_\_ No \_\_\_ Don't know  
 Debris Potential? \_\_\_ High X Med \_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes \_\_\_ No \_\_\_ Don't know X NA  
 Spur Dike X Yes \_\_\_ No \_\_\_ Don't know X NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA

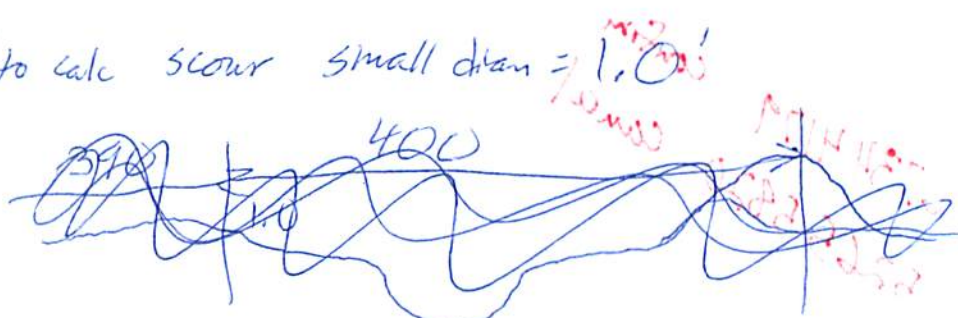
Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay X Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

2 sizes of piers  $\rightarrow$  larger used to calc scour small diam = 1.0'

- Photos  
 1382 - ID  
 83 - US  
 84 - US RB spur dike  
 85 - US LB  
 86 - LB Spur Dike  
 87 - LB Spur Dike  
 88 - R. Abut  
 89 - L. Abut  
 90 - US Face  
 91 - US Face



Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>38100</u>	<u>98000</u>
Flow depth at left abutment (yaLT), in feet	<u>1.0</u>	<u>9.0</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>7.8</u>
Contraction scour depth (yca), in feet	<u>4.3</u>	<u>10.7</u>
Pier scour depth (yps), in feet	<u>9.4</u>	<u>9.7</u>
Left abutment scour depth (yas), in feet	<u>4.3</u>	<u>20.6</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<u>19.6</u>
Flow angle of attack	<u>10</u>	<u>10</u>

See Comments/Diagram for justification where required