SCOUR ANALYSIS AND REPORTING FORM Bridge Structure No. 47378444 Date 9-19-12 Initials RFT Region (ABCD) Location 5 mi NE Hereford on Now Underwood Rd Site by: drainage area ratio\_\_\_\_ flood freq. anal. \_\_\_\_ regional regression eq. \_\_\_\_ Bridge discharge  $(Q_2) = 38100$  (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping) Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method Bridge Width = 388 ft. Flow angle at bridge = 56 ° Abut. Skew = 0 ° Effective Skew = 5 ° Width (W<sub>2</sub>) iteration = 388 301 343 327 333 Avg. flow depth at bridge,  $y_2$  iteration = 12.0 13.7 12.9 13.1 13.0Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 331.73 ft\*  $q_2 = Q_2/W_2 = 14.9$  ft²/s Bridge Vel,  $V_2 = 5.8$  ft/s Final  $y_2 = q_2/V_2 = 13.0$  ft  $\Delta h = 1.6$  ft Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 14 / L$ • NOTE: repeat above calculations until y 2 changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$ If y, is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD, than outer two pier sets are different than outer two for this analysis, treat all sets like center two Water Surface Elev. = Low Steel Elev. = = 20,0 irrigation ridges on either side of the channel will help quide flow toward bridge; may mitigate n (Channel) = .033n (LOB) = \_\_\_\_, 0りし some abutment scour n(ROB) =Pier Width = \_\_\_ Pier Length = \_\_\_ # Piers for 100 yr = \_\_\_\_ **CONTRACTION SCOUR** Width of main channel at approach section  $W_1 = 338$  ft Width of left overbank flow at approach,  $W_{lob} = 388$  ft Average left overbank flow depth,  $y_{lob} = 2.5$  ft Average right overbank flow depth,  $y_{rob} = 2 - 85$  ft Width of right overbank flow at approach,  $W_{rob} = 388$  ft Live Bed Contraction Scour (use if bed material is small cobbles or finer)  $x = \frac{9.02}{\text{From Figure 9}}$  From Figure 9  $W_2$  (effective) = 3.9.7 ft  $v_{cr} = 4.7 \, \mathrm{ft}$ Clear Water Contraction Scour (use if bed material is larger than small cobbles) Estimated bed material  $D_{50}$  = Average approach velocity,  $V_1 = Q_{100}/(y_1W_1) =$ \_\_\_\_\_ft/s Critical approach velocity,  $Vc = 11.17y_1^{1/6}D_{50}^{1/3} =$ If V<sub>1</sub><V<sub>c</sub> and D<sub>50</sub> >= 0.2 ft use clear water equation below, otherwise use live bed scour equation above. If  $D_{50} > = D_{c50}$ ,  $\chi = 0.0$  $D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$ Otherwise,  $\chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 =$ From Figure 10, y<sub>cs</sub> = PIER SCOUR CALCULATIONS L/a ratio =  $\frac{1}{2}$ Froude # at bridge = 0.43Correction factor for flow angle of attack (from Table 1), K2 = 1Using pier width a on Figure 11,  $\xi = 10.7$  Pier scour  $y_{ps} = 9.4$  ft **ABUTMENT SCOUR CALCULATIONS** left abutment,  $y_{aLT} = 2.5$  ft right abutment,  $y_{aRT} = 0.85$  ft Average flow depth blocked by:

Shape coefficient  $K_1$  = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \frac{10.2}{10.2}$  and  $\psi_{RT} = \frac{3.7}{10.2}$ 

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 10.2$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 3.7$  ft

PGRM: Pier

PGRM: Contract

PGRM: CWCSNEW

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 22.2$  ft Right abutment scour  $y_{as} = \psi_{RI}(K_1/0.55) = 20.8$  ft

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Route Underwood Elstream West E	Ilm	<u>Ck</u>	MRM	Da	te	Ini	tials
Bridge Structure No. 47378444	Loc	ation <u>5 mi</u>	NE from	Hercfor	d on N	en Unde	rwood Rd
GPS coordinates: <u>V 44° 23.920</u> , <u>W 102° 48.501</u>		taken from:	USL abutmer	1t	centerline o	of II MRM	end
W 102° 48,501		Datum of co	ordinates: W	GS84_ <u>√</u>	NAD27		
Drainage area $=$ 392 s							
The average bottom of the main channel was	s 27	the below	w top of guard	rail at a poin	. 141	ft from le	ft abutment.
Method used to determine flood flows:							
	_		_				
<b>F</b>	MIS	CELLANE	<b>EOUS CONSI</b>	DERATIO	NS		-
Flows		$Q_{100} =$	3810	<u>ს</u>	Q <sub>500</sub> =	9800	
Estimated flow passing through bridge			38100	<u> </u>		9800	D
Estimated road overflow & overtopping			U U	T = 14.4		D	
Consideration		Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping			V_	<del>-</del>			
Chance of Pressure flow Armored appearance to channel			1/	<del>- </del>		1/	<del> </del>
Lateral instability of channel			<del>                                     </del>	1		<del>                                     </del>	
						<u> </u>	
Riprap at abutments? Yes	١ ،	/No	Maroinal			cont	_
Fuidence of next Scour?	·	, No	Don't bear	w alore	בטט ב	Scau	ר ספפן טי
Evidence of past Scour?	·	INU	Doug Kno	M Big, 3	200	<b>Q</b>	•
Debris Potential? Hig	μ1 <u> </u>		_Low tree	es upsti	cam		
Does scour countermeasure(s) appear to have	e been	designed?					
Riprap		_	NoDo	m't know	) NI A		
Spur Dike	Y	zs^	NoDo	on't Know	_\_NA		
Other guide banh	<b>√</b> Y6	esN	NoDo	n't know	NA		
Dad M	otorial :	Classificatio	on Based on M	adian Dawi-	la Sina (D. 1	`	
~*							D
·			Gravel		Cobbles		Boulders
Size range, in mm <0.062 0.	062-2.	00	2.00-64		64-250		>250
Comments Diagrams & orientation of digital	al mbae	ne			_		
Comments, Diagrams & orientation of digital Str. No.  approach from brital LOB from chan  ROB from char  ROB irrigation  ROB irrigation	ar buote	02	L.	oridge	Ew	0.000	oach
Stri has from bell	dae		•	onay c	,	775	side bridge
approach	nel		(	center	pier	sets	. 1
LOB tion Class				a.ter	oters	let+	side
ROB from char	180 61			$\mathcal{L}^{(1)}$		، مارد	baides
PAR irrigation	Dern	~		let+ c	ibut, i	Mae	puradi
Tob irrigation	Deir	~		ct. c	hut.	under	bridge
STOP 1117		•		, , ,			
Summary of Results							
			Q100			Q500	
Bridge flow evaluated			38100			9800	0
Flow depth at left abutment (yaLT), in feet			2,5			11	
Flow depth at right abutment (yaRT), in feet			0.85			9,35	
Contraction scour depth (ycs), in feet			4,7			11,9	
Pier scour depth (yps), in feet			9,4			9.7	
Left abutment scour depth (yas), in feet			10,2 3,7	-	ļ	22,2	
Right abutment scour depth (yas), in feet		<u> </u>	3,7		L	20.8	

IFlow angle of attack