

ok-RAT

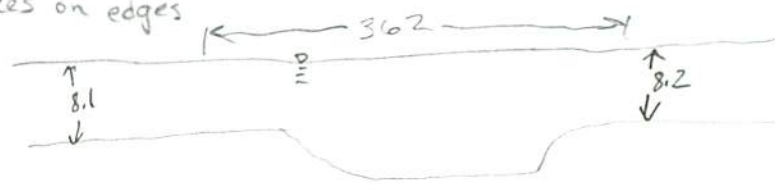
### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 4829 8103 Date 10-12-12 Initials RFT Region (A B C D) B  
 Site \_\_\_\_\_ Location 1.8 mi E of HWY 63 on 254 St  
 $Q_{100} =$  41100 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 41100 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 362 ft. Flow angle at bridge = 20 ° Abut. Skew = 0 ° Effective Skew = 20 °  
 Width ( $W_2$ ) iteration = 362  
 Avg. flow depth at bridge,  $y_2$  iteration = 13.4  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 340.17 ft\*  $q_2 = Q_2/W_2 =$  120.8 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  9.0 ft/s Final  $y_2 = q_2/V_2 =$  13.4 ft  $\Delta h =$  1.7 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  15.0 ft  
 \*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 20.3 ft  
 Low Steel Elev. = 14.8 ft  
 $n$  (Channel) = .035 mostly smooth + sandy, trees on edges  
 $n$  (LOB) = .065  
 $n$  (ROB) = .065 } woods + brush  
 Pier Width = 3.0 ft  
 Pier Length = 28 ft  
 # Piers for 100 yr = 4 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  362 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  362 ft Average left overbank flow depth,  $y_{lob} =$  8.1 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  362 ft Average right overbank flow depth,  $y_{rob} =$  8.2 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  7.99 From Figure 9  $W_2$  (effective) = 328.2 ft  $y_{cs} =$  8.8 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 9.33 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  2.4  
 Froude # at bridge = 0.43 Using pier width  $a$  on Figure 11,  $\xi =$  10.7 Pier scour  $y_{ps} =$  22.6 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  8.1 ft right abutment,  $y_{aRT} =$  8.2 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  19.8 and  $\psi_{RT} =$  19.9  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  19.8 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  19.9 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 48298103 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D) B  
 Site \_\_\_\_\_ Location 1.6 mi E of Hwy 63 on 254 St  
 $Q_{500} = 105000$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 76376 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

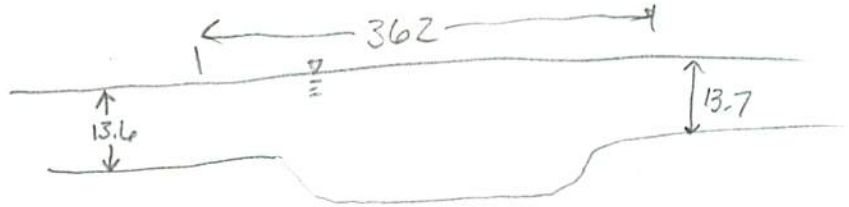
Bridge Width = 362 ft. Flow angle at bridge = 20 ° Abut. Skew = 0 ° Effective Skew = 20 °  
 Width ( $W_2$ ) iteration = 362  
 Avg. flow depth at bridge,  $y_2$  iteration = 18.5  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 340.17 ft\*  $q_2 = Q_2/W_2 = 224.5$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 12.1$  ft/s Final  $y_2 = q_2/V_2 = 18.5$  ft  $\Delta h = 3.0$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 21.5$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

road overflow will occur at  $y_2 \approx 18.5$

Water Surface Elev. = 0.3 ft  
 Low Steel Elev. = 14.8 ft  
 n (Channel) = 0.35  
 n (LOB) = 0.065  
 n (ROB) = 0.065  
 Pier Width = 3.0 ft  
 Pier Length = 28 ft  
 # Piers for 500 yr = 4 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 362$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 362$  ft Average left overbank flow depth,  $y_{lob} = 13.6$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 362$  ft Average right overbank flow depth,  $y_{rob} = 13.7$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 14.19$  From Figure 9  $W_2$  (effective) = 328.2 ft  $y_{cs} = 14.6$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^{3/2} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 9.33 Correction factor for flow angle of attack (from Table 1),  $K_2 = 2.4$   
 Froude # at bridge = 0.5 Using pier width a on Figure 11,  $\xi = 10.7$  Pier scour  $y_{ps} = 23.1$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 13.6$  ft right abutment,  $y_{aRT} = 13.7$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 24.3$  and  $\psi_{RT} = 24.4$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 24.3$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 24.4$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment



Route Co HWY 11 Stream Little White River MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 46298103 Location 1.8 mi E of HWY 83 on 254 St  
 GPS coordinates: N 43° 43.133' taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 100° 39.238' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 1570.14 sq. mi.  
 The average bottom of the main channel was 20.8 ft below top of guardrail at a point 123 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>41100</u>			Q <sub>500</sub> = <u>105000</u>		
Estimated flow passing through bridge	<u>41100</u>			<u>76376</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>28624</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>

PK calcd 8/8  
 2 1190  
 5 3080  
 10 7800  
 25 16000  
 50 26200  
 100 41100  
 500 105000

Riprap at abutments?  Yes \_\_\_ No \_\_\_ Marginal  
 Evidence of past Scour? \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  
 Debris Potential?  High \_\_\_ Med \_\_\_ Low lots of timber upstream

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike on left & rt with riprap  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_ Sand  Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 Str. no. bridge from rt. approach  
 LOB  
 ROB  
 rt. abut.  
 rt. spur dike  
 left abut.  
 left spur dike  
 Spur dikes will probably mitigate some of the estimated abutment scour

Summary of Results

	Q100	Q500 MAX SCOUR
Bridge flow evaluated	<u>41100</u>	<u>76376</u>
Flow depth at left abutment (yaLT), in feet	<u>8.1</u>	<u>13.6</u>
Flow depth at right abutment (yaRT), in feet	<u>8.2</u>	<u>13.7</u>
Contraction scour depth (yca), in feet	<u>8.8</u>	<u>14.6</u>
Pier scour depth (yp), in feet	<u>22.6</u>	<u>23.1</u>
Left abutment scour depth (yas), in feet	<u>19.8</u>	<u>24.3</u>
Right abutment scour depth (yas), in feet	<u>19.9</u>	<u>24.4</u>
Flow angle of attack	<u>20°</u>	<u>20°</u>

See Comments/Diagram for justification where required