

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 49069017 Date 7/24/12 Initials Raj Region (A B C D) D  
 Site \_\_\_\_\_ Location NE corner of Carthage on 425 Ave  
 $Q_{100} =$  5350 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 5350 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

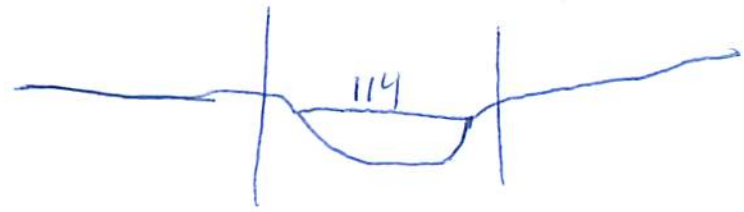
#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 132 ft. Flow angle at bridge = 35 ° Abut. Skew = 30 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 132 111 119 114  
 Avg. flow depth at bridge,  $y_2$  iteration = 9 9.8 9.5 9.7  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 132 cos 35 = 113.57 ft\*  $q_2 = Q_2/W_2 =$  47.1 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.9 ft/s Final  $y_2 = q_2/V_2 =$  9.7 ft  $\Delta h =$  0.5 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  10.2 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

47.1  
40.7  
17.6  
5.2  
12.4  
5.2 - 3.8  
1cc  
32

Water Surface Elev. = 0-3 ft 20.3  
 Low Steel Elev. = 16.2 ft 4.1  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.030  
 Pier Width = 2.8 ft  
 Pier Length = 2.9 ft  
 # Piers for 100 yr = 2 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  114 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  0.57 From Figure 9  $W_2$  (effective) = 108 ft  $y_{cs} =$  0.9 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

$L/a$  ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.28 Using pier width  $a$  on Figure 11,  $\xi =$  10.2 Pier scour  $y_{ps} =$  8.4 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  0  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

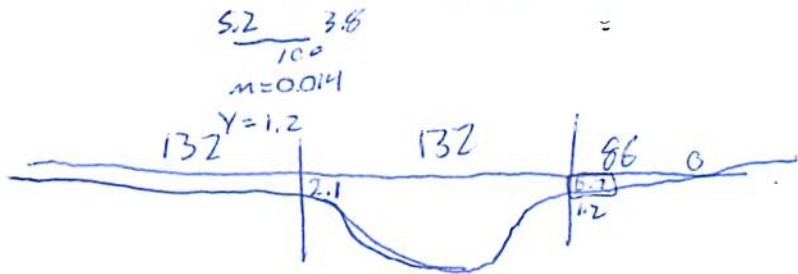
Bridge Structure No. 49069017 Date 7/24/12 Initials RAJ Region (A B C D) D  
 Site \_\_\_\_\_ Location NE corner of Carthage on 425 Ave  
 $Q_{500} =$  10400 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 10400 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 132 ft. 132 Flow angle at bridge = 33 ° Abut. Skew = 30 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 132 12.8  
 Avg. flow depth at bridge,  $y_2$  iteration = 12.5 12.7  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 127.51 ft\*  $q_2 = Q_2/W_2 =$  81.6 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  6.4 ft/s Final  $y_2 = q_2/V_2 =$  12.7 ft  $\Delta h =$  0.9 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  13.6 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-3 ft  
 Low Steel Elev. = 16.2 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.035  
 Pier Width = 2.8 ft  
 Pier Length = 2.8 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  132 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  132 ft Average left overbank flow depth,  $y_{lob} =$  2.1 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  86 ft Average right overbank flow depth,  $y_{rob} =$  0.7 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  2.2 From Figure 9  $W_2$  (effective) = 121.9 ft  $y_{cs} =$  2.7 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.32 Using pier width  $a$  on Figure 11,  $\xi =$  10.2 Pier scour  $y_{ps} =$  8.6 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  2.1 ft right abutment,  $y_{aRT} =$  0.7 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  8.6 and  $\psi_{RT} =$  3.1  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  8.6 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  3.1 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

49.1767

97.71311

2.2h, 2h db

49.1767

$$\begin{array}{r} 2.2h \\ \times 2h \\ \hline 4.4h \\ \hline 44.0h \\ \hline 88.0h \\ \hline 176.0h \\ \hline 352.0h \end{array}$$

Route 425 Ave Stream Redstone Ck MRM \_\_\_\_\_ Date 7/24/12 Initials Lat  
 Bridge Structure No. 49069017 Location NE corner of Carthage on 425 Ave  
 GPS coordinates: N 44° 10' 27.5" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 97° 42' 45.8" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 143.03 sq. mi. 20.3  
 The average bottom of the main channel was 20.3 ft below top of guardrail at a point 85 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>5350</u>			Q <sub>500</sub> = <u>10400</u>		
Estimated flow passing through bridge	<u>5350</u>			<u>10400</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

8/24

2	475
5	1530
10	2750
25	5030
50	7320
100	10200
500	19200

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know some pier/contraction  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

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2	212
5	725
10	1340
25	2550
50	3750
100	5350
500	10400

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1). left ab  
 2). main channel  
 3). right ab  
 4). pier  
 5-6). right abutment  
 7). pier scour  
 8-9). left abutment  
 10). main channels

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>5350</u>	<u>10400</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>2.1</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>0.7</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>0.9</u>	<u>2.7</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>8.4</u>	<u>8.6</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>0</u>	<u>8.6</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>0</u>	<u>3.1</u>
Flow angle of attack	<u>5</u>	<u>5</u>

See Comments/Diagram for justification where required