

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 50072100 Date 8/26/12 Initials RT Region (A B C D) C
 Site _____ Location 5 mi N + 1.8 mi W of Hartford on 254 St
 $Q_{100} = Q_{50}$ 3790 by: drainage area ratio _____ flood freq. anal. _____ regional regression eq. X
 Bridge discharge (Q_2) = 3790 (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 93 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °
 Width (W_2) iteration = _____

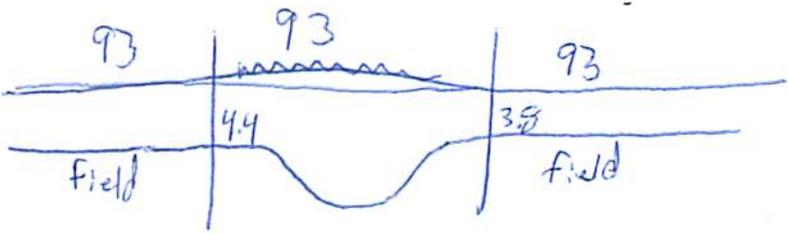
Avg. flow depth at bridge, y_2 iteration = _____
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 93 ft* $q_2 = Q_2/W_2 = \underline{40.6}$ ft²/s

Bridge Vel, $V_2 = \underline{4.5}$ ft/s Final $y_2 = q_2/V_2 = \underline{9}$ ft $\Delta h = \underline{0.4}$ ft

Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \underline{9.4}$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(\alpha) + a \cos(\alpha)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-0.5 ft
 Low Steel Elev. = 9.1 ft
 n (Channel) = 0.033
 n (LOB) = 0.030
 n (ROB) = 0.030
 Pier Width = 2 ft
 Pier Length = 2 ft
 # Piers for 100 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = \underline{93}$ ft
 Width of left overbank flow at approach, $W_{lob} = \underline{93}$ ft Average left overbank flow depth, $y_{lob} = \underline{4.4}$ ft
 Width of right overbank flow at approach, $W_{rob} = \underline{93}$ ft Average right overbank flow depth, $y_{rob} = \underline{3.8}$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
 $x = \underline{5.86}$ From Figure 9 W_2 (effective) = 89 ft $y_{cs} = \underline{6.6}$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
 Estimated bed material $D_{50} = \underline{\quad}$ ft Average approach velocity, $V_1 = Q_{100}/(y_1 W_1) = \underline{\quad}$ ft/s
 Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} = \underline{\quad}$ ft/s
 If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 = \underline{\quad}$ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$
 Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\quad}$ From Figure 10, $y_{cs} = \underline{\quad}$ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), $K_2 = \underline{1}$
 Froude # at bridge = 0.26 Using pier width a on Figure 11, $\xi = \underline{8}$ Pier scour $y_{ps} = \underline{6.5}$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = \underline{4.4}$ ft right abutment, $y_{aRT} = \underline{3.8}$ ft
 Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \underline{14}$ and $\psi_{RT} = \underline{12.9}$
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = \underline{14}$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = \underline{12.9}$ ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

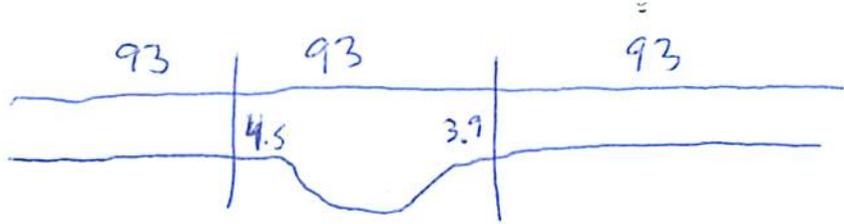
Bridge Structure No. 50072100 Date 4/26/12 Initials Raj Region (A B C D) D
 Site _____ Location 5 mi N + 1.8 mi W of Hartford on 254 St
 $Q_{500} = Q_{ce}$ 4770 by: drainage area ratio _____ flood freq. anal. _____ regional regression eq. X
 Bridge discharge (Q_2) = 3967 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 93 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °
 Width (W_2) iteration = _____
 Avg. flow depth at bridge, y_2 iteration = _____
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 93 ft* $q_2 = Q_2/W_2 = 41.6$ ft²/s
 Bridge Vel, $V_2 = 4.6$ ft/s Final $y_2 = q_2/V_2 = 9.1$ ft $\Delta h = 0.4$ ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 9.5$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2
 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 00.4 ft
 Low Steel Elev. = 9.1 ft
 n (Channel) = 0.033
 n (LOB) = 0.030
 n (ROB) = 0.030
 Pier Width = 2 ft
 Pier Length = 2 ft
 # Piers for 500 yr = 2



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = 93$ ft
 Width of left overbank flow at approach, $W_{lob} = 93$ ft Average left overbank flow depth, $y_{lob} = 4.5$ ft
 Width of right overbank flow at approach, $W_{rob} = 93$ ft Average right overbank flow depth, $y_{rob} = 3.9$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
 $x = 6.05$ From Figure 9 W_2 (effective) = 89 ft $y_{cs} = 6.8$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
 Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s
 Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s
 If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$
 Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), $K_2 = 1$
 Froude # at bridge = 0.27 Using pier width a on Figure 11, $\xi = 8$ Pier scour $y_{ps} = 6.6$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = 4.5$ ft right abutment, $y_{aRT} = 3.9$ ft
 Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = 14.1$ and $\psi_{RT} = 13.1$
 Left abutment scour, $y_{as} = \psi_{LT} (K_1 / 0.55) = 14.1$ ft Right abutment scour $y_{as} = \psi_{RT} (K_1 / 0.55) = 13.1$ ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie:

PGRM: Abutment

96.98717
43.70313

96.59
13.812
12.348

W. J. ...
...

Route 254 St Stream W. Br. Skunk Cr MRM _____ Date 4/26/12 Initials RAT
 Bridge Structure No. 50072100 Location 5 mi N + 1.8 mi W of Hartford on 254 St
 GPS coordinates: N 43° 42' 12.4" taken from: USL abutment centerline of MRM end _____
W 96° 59' 13.7" Datum of coordinates: WGS84 NAD27 _____

Drainage area = 57.67 sq. mi.

The average bottom of the main channel was 13 ft below top of guardrail at a point 57 ft from left abutment.

Method used to determine flood flows: ___ Freq. Anal. ___ drainage area ratio y regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	$Q_{100} = Q_{50}$ <u>3780</u>			$Q_{500} = Q_{100}$ <u>4770</u>		
Estimated flow passing through bridge	<u>3780</u>			<u>3867</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>903</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>
Chance of Pressure flow	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

8 57.67
 0115
 2 469
 5 1190
 10 1880
 25 2880
 50 3780
 100 4770
 500 7400

Riprap at abutments? ___ Yes No ___ Marginal
 Evidence of past Scour? Yes ___ No ___ Don't know *some pier/contraction minor abutment*
 Debris Potential? ___ High ___ Med Low

Does scour countermeasure(s) appear to have been designed?

Riprap ___ Yes No ___ Don't know ___ NA
 Spur Dike ___ Yes No ___ Don't know ___ NA
 Other ___ Yes No ___ Don't know ___ NA

Bed Material Classification Based on Median Particle Size (D_{50})

Material Silt/Clay Sand ___ Gravel ___ Cobbles ___ Boulders ___
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1) left ab
- 2) main channel
- 3) right ab
- 4) pier
- 5-6) right abutment
- 7-8) left abutment
- 9) pier scour
- 10) main channel

Summary of Results

	Q_{100} <u>Q_{50}</u>	Q_{500} <u>Q_{100}</u>
Bridge flow evaluated	<u>3780</u>	<u>3867</u>
Flow depth at left abutment (yaLT), in feet	<u>4.4</u>	<u>4.5</u>
Flow depth at right abutment (yaRT), in feet	<u>3.8</u>	<u>3.9</u>
Contraction scour depth (yca), in feet	<u>6.6</u>	<u>6.9</u>
Pier scour depth (yca), in feet	<u>6.5</u>	<u>6.6</u>
Left abutment scour depth (yca), in feet	<u>14</u>	<u>14.1</u>
Right abutment scour depth (yca), in feet	<u>12.9</u>	<u>13.1</u>
Flow angle of attack	<u>0</u>	<u>0</u>

See Comments/Diagram for justification where required