

OK RT

## SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 50124050 Date 6/27/12 Initials FAT Region (A B C D)  
 Site Location 0.5 mi N & 0.5 mi W of Lyons on 252 St  
 $Q_{100} = \underline{2950}$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 2950 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

## Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 142 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °

Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 142 ft\*  $q_2 = Q_2/W_2 = \underline{21}$  ft²/s

Bridge Vel,  $V_2 = \underline{3.2}$  ft/s Final  $y_2 = q_2/V_2 = \underline{6.5}$  ft  $\Delta h = \underline{0.2}$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{6.7}$  ft

\*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PGRM: "RegionA", "RegionB",  
"RegionC", or "RegionD"

Water Surface Elev. = 0-1.0 ft

Low Steel Elev. = 8.2 ft

n (Channel) = 0.060 *very weedy*

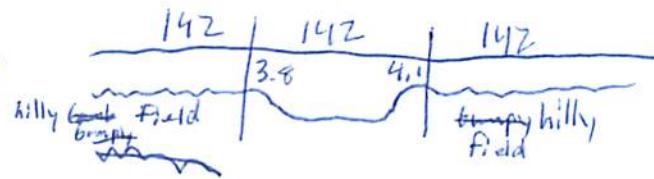
n (LOB) = 0.045 *hilly grass*

n (ROB) = 0.043

Pier Width = 1.85 ft

Pier Length = 1.65 ft

# Piers for 100 yr = 4 ft



## CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = \underline{142}$  ft

Width of left overbank flow at approach,  $W_{lob} = \underline{142}$  ft Average left overbank flow depth,  $y_{lob} = \underline{3.8}$  ft

Width of right overbank flow at approach,  $W_{rob} = \underline{142}$  ft Average right overbank flow depth,  $y_{rob} = \underline{4.1}$  ft

## Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = \underline{8.19}$  From Figure 9  $W_2$  (effective) = 134.6 ft  $y_{cs} = \underline{9}$  ft

## Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} = \underline{\text{ft}}$  Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) = \underline{\text{ft/s}}$

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} = \underline{\text{ft/s}}$

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} = \underline{\text{ft}}$  If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2/(D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\text{ft}}$  From Figure 10,  $y_{cs} = \underline{\text{ft}}$

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

## PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1}$

Froude # at bridge = 0.22 Using pier width a on Figure 11,  $\xi = \underline{7.5}$  Pier scour  $y_{ps} = \underline{6}$  ft

## ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{3.8}$  ft right abutment,  $y_{aRT} = \underline{4.1}$  ft

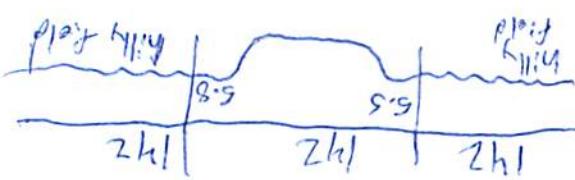
Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls,  $0.55$  for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{12.9}$  and  $\psi_{RT} = \underline{13.4}$

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = \underline{12.9}$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = \underline{13.4}$  ft

Bridge Structure No.	56124080	Date	6/21/12
Location	D.5 mi N + 0.5 mi W of Lyons on 352 S	Region (A B C D)	A
Site	Bridge discharge ( $Q_2$ ) = 41620 (should be $Q_{500}$ unless there is a relief bridge, road overflow, or bridge overtopping) by: drainage area ratio Flood freq. anal. regional regression eq.		
Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method	Width (W <sub>2</sub> ) iteration = Bridge Width = 142 ft Flow angle at bridge = 0°. Abut. Skew = 0°. Effective Skew = 0°		
Avg. flow depth at bridge, $y_2$ iteration =	Corrected channel width at bridge Section = $W_2$ times cos of flow angle = 142 ft* $q_2 = Q^2/W^2 = 32.5 \text{ ft}^2/\text{s}$		
Bridge Vel, $V_2 = 4 \text{ ft/s}$	Average main channel depth at approach section, $y_1 = Ah + y_2 = 8.1 \text{ ft}$		
* NOTE: repeat above calculations until $y_2$ changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$			
Water Surface Elev. = 0.10 ft	Low Steel Elev. = 9.2 ft		
$n(\text{Channel}) = 0.060$	$n(\text{LOB}) = 0.045$		
Pier Length = 1.85 ft	Pier Width = 1.85 ft		
# Piers for 500 yr = 4			
If $y_2$ is above LS, then account for Road Overflow using PRGM, RDVREGA, RDVREGC, or RDVREGD.			
Contraction Scour (use if bed material is larger than small cobbles)			
$x = 12.67$ From Figure 9	$W_2(\text{effective}) = 134.6 \text{ ft}$		
$y_{cs} = 13.7 \text{ ft}$			
Live Bed Contraction Scour (use if bed material is smaller than small cobbles or fine)			
$x = 12.67$ From Figure 9	$W_2(\text{effective}) = 134.6 \text{ ft}$		
$y_{cs} = 13.7 \text{ ft}$			
Cleat Water Contraction Scour (use if bed material is larger than small cobbles)			
$x = 12.67$ From Figure 9	$W_2(\text{effective}) = 134.6 \text{ ft}$		
$y_{cs} = 13.7 \text{ ft}$			
Estimated bed material $D_{50} = \frac{\text{ft}}{\text{ft/s}}$ Critical approach velocity, $V_c = \frac{\text{ft}}{\text{ft/s}}$ Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) = \frac{\text{ft/s}}{\text{ft/s}}$			
If $V_1 < V_c$ , and $D_{50} > 0.2 \text{ ft}$ , use deeper water equation below, otherwise use live bed scour equation above.			
$D_{50} = 0.0006(q^2/y_1^{7/6})^3 = \frac{\text{ft}}{\text{ft}}$ If $D_{50} > D_{500}$ , $\chi = 0.0$			
Otherwise, $\chi = 0.122y_1^{1/2}/(D_{50}^{1/3}y_1^{7/6})^{6/7} - \chi_1 = \frac{\text{ft}}{\text{ft}}$			
From Figure 10, $y_{cs} = \frac{\text{ft}}{\text{ft}}$			
PIER SCOUR CALCULATIONS			
$1/a \text{ ratio} = 1$	Froude # at bridge = 0.25		
Correlation factor for flow angle of attack (from Table 1), $K_2 = 1$			
Using pier width a on Figure 11, $\xi = 7.5$ Pier scour $y_{ps} = 6.1 \text{ ft}$			
Average flow depth blocked by: Left abutment, $y_{LT} = 5.5 \text{ ft}$ Right abutment, $y_{RT} = 5.8 \text{ ft}$			
Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through			
Left abutment scour, $y_{as} = \sqrt{LT}(K_1/0.55) = 15.9 \text{ ft}$ Right abutment scour, $y_{ar} = \sqrt{RT}(K_1/0.55) = 16.5 \text{ ft}$			

## CONTRACTATION SCOUR



Width (W<sub>2</sub>) iteration =

$$\text{Corrected channel width at bridge Section} = W_2 \times \cos(\text{flow angle}) = 142 \text{ ft}^*$$

$$q_2 = Q^2/W^2 = 32.5 \text{ ft}^2/\text{s}$$

Avg. flow depth at bridge,  $y_2$  iteration =

$$\text{Bridge Vel}, V_2 = 4 \text{ ft/s}$$

$$\text{Final } y_2 = q/V_2 = 8.1 \text{ ft}$$

$$Ah = 0.3 \text{ ft}$$

$$\text{Average main channel depth at approach section}, y_1 = Ah + y_2 = 8.1 \text{ ft}$$

$n(\text{Channel}) = 0.060$

$n(\text{LOB}) = 0.045$

Pier Length = 1.85 ft

Pier Width = 1.85 ft

# Piers for 500 yr = 4

If  $y_2$  is above LS, then account for Road Overflow using PRGM, RDVREGA, RDVREGC, or RDVREGD.

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

Bridge Width = 142 ft Flow angle at bridge = 0°. Abut. Skew = 0°. Effective Skew = 0°

Width (W<sub>2</sub>) iteration =

$$\text{Corrected channel width at bridge Section} = W_2 \times \cos(\text{flow angle}) = 142 \text{ ft}^*$$

$$q_2 = Q^2/W^2 = 32.5 \text{ ft}^2/\text{s}$$

Bridge discharge ( $Q_2$ ) = 41620 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

$Q_{500} = 41620$  by: drainage area ratio Flood freq. anal. regional regression eq.

Bridge discharge ( $Q_2$ ) = 41620

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 142 ft Flow angle at bridge = 0°. Abut. Skew = 0°. Effective Skew = 0°

Width (W<sub>2</sub>) iteration =

$$\text{Corrected channel width at bridge Section} = W_2 \times \cos(\text{flow angle}) = 142 \text{ ft}^*$$

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\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

43.73225

46.64678

~~43.73225~~

~~46.64678~~

43.43 36.11

46.0 39.4 46.1081

Route 262 St Stream Skunk Ck MRM \_\_\_\_\_ Date 6/27/12 Initials JAT  
 Bridge Structure No. 50124040 Location 0.5 mi N + 0.5 mi W of Lyons on 262 St  
 GPS coordinates: N 43° 43' 58.91" taken from: USL abutment  centerline of MRM end \_\_\_\_\_  
 W 96° 52' 56.51" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 290.15 sq. mi.

The average bottom of the main channel was 11.9 ft below top of guardrail at a point 56 ft from left abutment.  
 Method used to determine flood flows: Freq. Anal. drainage area ratio regional regression equations.

6.52

6.18

2 231  
 5 571  
 10 871  
 25 1333  
 50 1720  
 100 2150  
 500 3234

6.18

2 17.0  
 5 42  
 10 10.6  
 25 10.7  
 50 13.7  
 100 16.5  
 500 24.2

6.17

2 17.0  
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 100 16.5  
 500 24.2

6.17

#### MISCELLANEOUS CONSIDERATIONS

Flows	$Q_{100} = Q_5$	$Q_{500} = Q_{10}$				
Estimated flow passing through bridge	2980	4620				
Estimated road overflow & overtopping	0	0				
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		X			X	
Chance of Pressure flow	X			X		
Armored appearance to channel	X			X		
Lateral instability of channel	X			X		

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal \_\_\_\_\_

Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ pier/construction/abutment

Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med \_\_\_\_\_ Low \_\_\_\_\_

Does scour countermeasure(s) appear to have been designed?

Riprap  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

#### Bed Material Classification Based on Median Particle Size ( $D_{50}$ )

Material	Silt/Clay <input checked="" type="checkbox"/>	Sand _____	Gravel _____	Cobbles _____	Boulders _____
Size range, in mm	<0.062	0.062-2.00	2.00-64	64-250	>250

Comments, Diagrams & orientation of digital photos

- 1) left abutment
- 2) main channel
- 3) right abutment
- 4) pier
- 5) pier scour
- 6) main channel

#### Summary of Results

	$Q_{100}^5$	$Q_{500}^{10}$
Bridge flow evaluated	2980	4620
Flow depth at left abutment (yaLT), in feet	3.8	5.5
Flow depth at right abutment (yaRT), in feet	4.1	5.8
Contraction scour depth (ycs), in feet	9	13.7
Pier scour depth (yps), in feet	6	6.1
Left abutment scour depth (yas), in feet	12.9	15.9
Right abutment scour depth (yas), in feet	13.4	16.5
Flow angle of attack	0	0

See Comments/Diagram for justification where required