| | SCOUR ANALYSIS AND REPORTING FORM | | | | | | | |
|-------------|--|--|--|--|--|--|--|--|
| | Bridge Structure No. 50144020 Date 612611 Initials 1261 Region (ABCD) Site Location 3.2 m ; Wof $1-90 \text{ on } 246 \text{ SF}$ Q ₁₀₀ = 1260 by ; drainage area ratio flood freq. anal. regional regression eq. 1260 m | | | | | | | |
| | Site Location 3.2 m; Wot I-90 on 246 5t | | | | | | | |
| | Q ₁₀₀ = Q ₅ 2760 by: drainage area ratio flood freq. anal. regional regression eq. | | | | | | | |
| | Bridge discharge $(Q_2) = \underline{2760}$ (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping) | | | | | | | |
| | | | | | | | | |
| | Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method | | | | | | | |
| r "RegionD" | Bridge Width = $\frac{95}{}$ ft. Flow angle at bridge = $\frac{15}{}$ $^{\circ}$ Abut. Skew = $\frac{0}{}$ $^{\circ}$ Effective Skew = $\frac{15}{}$ $^{\circ}$ Width (W ₂) iteration = | | | | | | | |
| | Width (W ₂) iteration = | | | | | | | |
| | Corrected channel width at bridge Section = W_2 times cos of flow angle = 91.76 ft* $q_2 = Q_2/W_2 = \frac{30}{100}$ ft²/s | | | | | | | |
| | Bridge Vel, $V_2 = 3.7$ ft/s Final $y_2 = q_2/V_2 = 7.7$ ft $\Delta h = 6.3$ ft | | | | | | | |
| 0,0 | Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \frac{\mathcal{C}}{2}$ ft | | | | | | | |
| gion | * NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$ | | | | | | | |
| Ke | fy 2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD, | | | | | | | |
| | W. C. C. Fl. 62-17-0 | | | | | | | |
| | Water Surface Elev. = $6.3 \cdot 1.3$ ft Low Steel Elev. = $6.1 \cdot 1.3$ ft 9.5 | | | | | | | |
| | Low Steel Elev. = $\frac{6.1}{0.090}$ ft n (Channel) = $\frac{0.090}{0.030}$ | | | | | | | |
| | $n \text{ (LOB)} = \frac{G.030}{G.030}$ | | | | | | | |
| | n (ROB) = World B.O.C. | | | | | | | |
| | n (ROB) = | | | | | | | |
| | # Piers for $100 \text{ yr} = 3 \text{ ft}$ | | | | | | | |
| | | | | | | | | |
| | CONTRACTION SCOUR | | | | | | | |
| | Width of main channel at approach section $W_1 = \frac{94.95}{95}$ ft Width of left overbank flow at approach, $W_{lob} = \frac{95}{95}$ ft Average left overbank flow depth, $y_{lob} = \frac{95}{95}$ ft | | | | | | | |
| | | | | | | | | |
| | Width of right overbank flow at approach, $W_{rob} = \frac{9975}{15}$ ft Average right overbank flow depth, $y_{rob} = \frac{300}{15}$ ft | | | | | | | |
| | ive Bed Contraction Scour (use if bed material is small cobbles or finer) | | | | | | | |
| | $x = 6.43$ From Figure 9 W_2 (effective) = 66.8 ft $y_{cs} = 9.3$ ft | | | | | | | |
| | | | | | | | | |
| | Clear Water Contraction Scour (use if bed material is larger than small cobbles) | | | | | | | |
| | Estimated bed material $D_{t0} = ft$ Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = ft/s$ | | | | | | | |
| | Critical approach velocity, $VC = 11.1/y_1$ $D_{50} = 11.5$ | | | | | | | |
| | Critical approach velocity, $V_c = 11.17y_1^{1/6}D_{50}^{1/3} =$ | | | | | | | |
| | $D_{c50} = 0.0000(q_2/y_1) = \frac{1}{100000}$ Otherwise $y = 0.122y_1 \text{ fb} / \text{(D. } \frac{1/3}{2}, \frac{7/6}{2}) \frac{6/7}{2}, y = \frac{1}{100000}$ | | | | | | | |
| | Otherwise, $\chi = 0.1229_1[4_2/(D_{50} \ y_1)] = y_1 =1$ | | | | | | | |
| | PIER SCOUR CALCULATIONS | | | | | | | |
| | L/a ratio = Correction factor for flow angle of attack (from Table 1), K2 = | | | | | | | |
| | Froude # at bridge = 0.25 PIER SCOUR CALCULATIONS Correction factor for flow angle of attack (from Table 1), K2 = 1.5 Using pier width a on Figure 11, $\xi = 6.9$ Pier scour $y_{ps} = 5.6$ ft | | | | | | | |
| | ABUTMENT SCOUR CALCULATIONS | | | | | | | |
| | Average flow depth blocked by: left abutment, $v_{al,T} = 4.5$ ft right abutment, $v_{aRT} = 3.3$ ft | | | | | | | |
| | Shape coefficient K ₁ = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, [0.85 for spill-through] | | | | | | | |
| | Shape coefficient K_1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, Using values for y_{aLT} and y_{aRT} on figure 12, ψ_{LT} = 14.1 and ψ_{RT} = 12 | | | | | | | |
| | Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 12$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 12$ ft | | | | | | | |

PGRM: "RegionA", "RegionB",

PGRM: Contract

PGRM: CWCSNEW

PGRM: Abutment PGRM: Pier

1613.5P

1,96.3 , pp 054

| Route 246 St Stream Skunk C | K | MRM | Dat | te 612-611 | 7 Ini | itials LaT | | | |
|---|---------------|----------------|----------------|---------------------------|------------------------------------|---------------|-----------|--|--|
| Bridge Structure No. 60144020 Location 3.2 mail 1 90 0. 246 St | | | | | | | | | |
| GPS coordinates: $\frac{U}{\sqrt{3}} \frac{\sqrt{9}}{\sqrt{9}} \frac$ | | | | | | | | | |
| W 96° 50' 40.911 | Datum of co | ordinates: W | GS84 X | NAD27 | I II IVIRIVI | end | | | |
| Drainage area = 273.62 sq. mi. | | | 7 | _ | | | | | |
| The average bottom of the main channel was | 2.4 ft below | w top of guard | rail at a poin | t 21 | ft from le | eft abutment. | | | |
| Method used to determine flood flows:Freq | | | | | | | 273.52 | | |
| | | | | 0 0 | iveresestive involte d l in | | 6113 | | |
| | SCELLANE | OUS CONSI | | NS - | | | | | |
| Flows | Que Q | | | Q509_= Q | 10 BR | 4280 | 2 1100 | | |
| Estimated flow passing through bridge | 2760 | | | 3251 | | | 5 2760 | | |
| Estimated road overflow & overtopping | | 0 | | | | 1029 | 10 4280 | | |
| Consideration | Yes | No | Possibly | Yes | No | Possibly | 25 6690 | | |
| Chance of overtopping | | X | | \rightarrow | | | 50 8820 | | |
| Chance of Pressure flow | | X | | \sim | | | 10e 11200 | | |
| Armored appearance to channel | | X | | | X | | 500 17600 | | |
| Lateral instability of channel | | X | | | \times | ÷ | | | |
| Riprap at abutments? Evidence of past Scour? Debris Potential? Yes No Marginal mostly on risht, and outside left abutment No Marginal mostly on risht, and outside left abutment No Don't know some contraction of pier, minor abutment Low | | | | | | | | | |
| Does scour countermeasure(s) appear to have been | n designed? | | | ē | | ł_ | | | |
| Riprap | esN | loDo | n't know | NA C | sequar | 18 | | | |
| Spur Dike Y | es > N | lo Do | n't know | NA | | | | | |
| Riprap Yes No Don't know NA rose quality Spur Dike Yes No Don't know NA Other Yes No Don't know NA | | | | | | | | | |
| | | | - | | | | | | |
| Bed Material | Classificatio | n Based on M | edian Particl | e Size (D ₅₀) | | | | | |
| Material Silt/Clay Sand Sand | | Gravel | | Cobbles | | Boulders | | | |
| Size range, in mm < 0.062 0.062-2 | .00 | | | 64-250 | _ | >250 | | | |
| 0.002 2 | .00 | 2.00-01 | | 04-250 | | - 250 | | | |
| Comments, Diagrams & orientation of digital photos | | | | | | | | | |
| Q. Latt CB 9), last abut ment | | | | | | | | | |
| Districts 2) main channel 3) right on, 4), right abulment 85-6). 1-H abulment 7), pler scorn 8), prers | | | | | | | | | |
| 3) right on [2], mal a changer | | | | | | | | | |
| 4) ight between (2) mal a change | | | | | | | | | |
| KC-1) left abutment | | | | | | | | | |
| 8) -0/. 1 Carolina | | | | | | | | | |
| of pres score | | | | | | | | | |
| 8). pre15 | | | | | | | | | |
| Summary of Results | | | | | | | a | | |
| 9 | Q100 Q5 | | | Q500 Q1B | | | | | |
| Bridge flow evaluated | 2760 | | | 3251 | | | | | |
| Flow depth at left abutment (yaLT), in feet | 4,5 | | | 5.3 | | | | | |
| Flow depth at right abutment (yaRT), in feet | | | | 4.1 | | | | | |
| Contraction scour depth (ycs), in feet | | 9.3 | | | 11, 7 | | | | |
| Pier scour depth (yps), in feet | | 5.6 | | | 5,6 | | | | |
| Left abutment scour depth (yas), in feet | 14.1 | | | 15.6 | | | | | |

12

15

13.4

15

Right abutment scour depth (yas), in feet 1Flow angle of attack