

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 50186235 Date 6/21/12 Initials RT Region (A B C D) C  
 Site \_\_\_\_\_ Location Big Sioux R + 49th St  
 $Q_{100} = Q_{50} = 41700 by: drainage area ratio _____ flood freq. anal. _____ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 41700 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)$

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 263 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

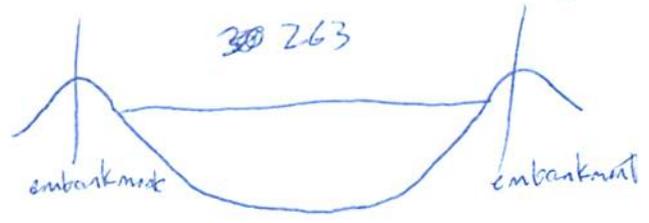
Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 259 ft\*  $q_2 = Q_2/W_2 =$  161 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  9 ft/s Final  $y_2 = q_2/V_2 =$  17.9 ft  $\Delta h =$  1.7 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  19.5 ft

\*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1.7 ft  
 Low Steel Elev. = 20.1 ft  
 n (Channel) = 0.030  
 n (LOB) = 0.013 asphalt  
 n (ROB) = 0.013  
 Pier Width = 3.5 ft  
 Pier Length = 3.5 ft  
 # Piers for 100 yr = 4 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  263 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  1.43 From Figure 9  $W_2$  (effective) = 245 ft  $y_{cs} =$  1.9 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.37 Using pier width a on Figure 11,  $\xi =$  11.9 Pier scour  $y_{ps} =$  10.3 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

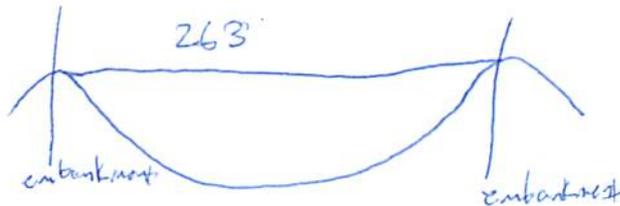
Bridge Structure No. 50186235 Date 6/21/12 Initials RA Region (A B C D) D  
 Site \_\_\_\_\_ Location Big Sioux R + 49th St  
 $Q_{500} = Q_{pu}$  53200 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 52665 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = \_\_\_\_\_ ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 259 ft\*  $q_2 = Q_2/W_2 = \underline{203.3}$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = \underline{10.1}$  ft/s Final  $y_2 = q_2/V_2 = \underline{20.1}$  ft  $\Delta h = \underline{2.1}$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{22.2}$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1.7 ft  
 Low Steel Elev. = 20.1 ft  
 n (Channel) = 0.030  
 n (LOB) = 0.013  
 n (ROB) = 0.013  
 Pier Width = 3.5 ft  
 Pier Length = 3.5 ft  
 # Piers for 500 yr = 4 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = \underline{263}$  ft  
 Width of left overbank flow at approach,  $W_{lob} = \underline{0}$  ft Average left overbank flow depth,  $y_{lob} = \underline{0}$  ft  
 Width of right overbank flow at approach,  $W_{rob} = \underline{0}$  ft Average right overbank flow depth,  $y_{rob} = \underline{0}$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = \underline{1.63}$  From Figure 9  $W_2$  (effective) = 245 ft  $y_{cs} = \underline{2.1}$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1}$   
 Froude # at bridge = 0.4 Using pier width a on Figure 11,  $\xi = \underline{11.9}$  Pier scour  $y_{ps} = \underline{10.4}$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{0}$  ft right abutment,  $y_{aRT} = \underline{0}$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{0}$  and  $\psi_{RT} = \underline{0}$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = \underline{0}$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = \underline{0}$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie:

PGRM: Abutment

43.50819

96.75928

96 45' 33.408"  
43° 30' 29.448"

Route 49th St Stream Big Sioux River MRM \_\_\_\_\_ Date 6/21/12 Initials KAT  
 Bridge Structure No. 50186235 Location Big Sioux River + 49th St  
 GPS coordinates: N 43° 30' 29.7" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 96° 45' 33.9" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 3749.05 sq. mi.  
 The average bottom of the main channel was 25.7 ft below top of guardrail at a point 61 ft from left abutment.  
 Method used to determine flood flows:      Freq. Anal.      drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = Q <sub>50</sub> <u>41700</u>			Q <sub>500</sub> = Q <sub>100</sub> <u>53200</u>		
Estimated flow passing through bridge	<u>41700</u>			<u>52665</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>535</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow			<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

6/15  
 2 5520  
 5 13300  
 10 20300  
 25 31600  
 50 41700  
 100 53200  
 500 84800

Riprap at abutments?      Yes  No      Marginal  
 Evidence of past Scour?  Yes      No      Don't know *some contraction + pier in the abutment*  
 Debris Potential?      High      Med      Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap      Yes  No      Don't know      NA  
 Spur Dike      Yes  No      Don't know      NA  
 Other       Yes      No      Don't know      NA *embankment blocking overbank*

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand      Gravel      Cobbles      Boulders       
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1). left ab.  
 2). main channel  
 3). right ab.  
 4). piers  
 5-7). left abutment  
 8-9). right abutment  
 10). left abutment  
 11). main channel

Summary of Results

	Q <sub>100</sub> Q <sub>50</sub>	Q <sub>500</sub> Q <sub>100</sub>
Bridge flow evaluated	<u>41700</u>	<u>52665</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>0</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>1.9</u>	<u>2.1</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>10.3</u>	<u>10.4</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>0</u>	<u>0</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>0</u>	<u>0</u>
IFlow angle of attack	<u>10</u>	<u>10</u>

See Comments/Diagram for justification where required