

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 50189140 Date 9-11-10 Initials RRL Region (A B C D)

Site Location From I-29 Exit 86, IE

Q\_100 = 33,200 by: drainage area ratio [checked] flood freq. anal. regional regression eq.

Bridge discharge (Q\_2) = 33,200 (should be Q\_100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 322.5 ft Flow angle at bridge = 15 degrees Abut. Skew = 0 Effective Skew = 15 degrees

Width (W\_2) iteration = 308 295

Avg. flow depth at bridge, y\_2 iteration = 14.9 15.2

Corrected channel width at bridge Section = W\_2 times cos of flow angle = 284.95 ft\* q\_2 = Q\_2/W\_2 = 116.5 ft^2/s

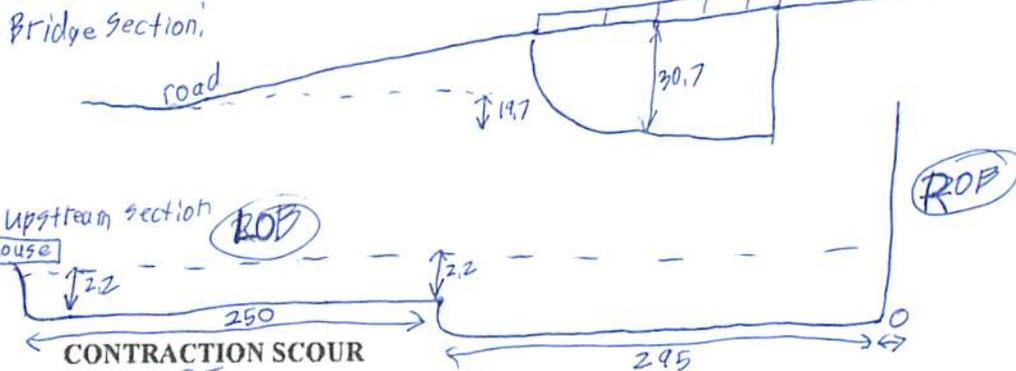
Bridge Vel. V\_2 = 7.7 ft/s Final y\_2 = q\_2/V\_2 = 15.2 ft Delta h = 1.2 ft

Average main channel depth at approach section, y\_1 = Delta h + y\_2 = 16.4 ft

\* NOTE: repeat above calculations until y\_2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)

If y\_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 5.2 ft
Low Steel Elev. = 27.7 ft
n (Channel) = 0.035
n (LOB) = 0.035
n (ROB) = 0.040
Pier Width = 2.2 ft
Pier Length = 31 ft
# Piers for 100 yr = 3



Width of main channel at approach section W\_1 = 295 ft

Width of left overbank flow at approach, W\_lob = 250 ft Average left overbank flow depth, y\_lob = 2.2 ft

Width of right overbank flow at approach, W\_rob = 0 ft Average right overbank flow depth, y\_rob = 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 1.19 From Figure 9 W\_2 (effective) = 278.4 ft y\_cs = 1.7 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D\_50 = ft Average approach velocity, V\_1 = Q\_100/(y\_1 W\_1) = ft/s

Critical approach velocity, V\_c = 11.52 y\_1^(1/6) D\_50^(1/3) = ft/s
If V\_1 < V\_c and D\_50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

D\_c50 = 0.0006 (q\_2/y\_1^(7/6))^3 = ft If D\_50 >= D\_c50, zeta = 0.0
Otherwise, zeta = 0.122 y\_1 [q\_2 / (D\_50^(1/3) y\_1^(7/6))]^(5/7) - y\_1 = From Figure 10, y\_cs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 14 Correction factor for flow angle of attack (from Table 1), K\_2 = 2.5
Froude # at bridge = 0.35 Using pier width a on Figure 11, zeta = 8.6 Pier scour y\_ps = 18.4 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, y\_al,T = 2.2 ft right abutment, y\_ar,T = 0 ft
Shape coefficient K\_1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for y\_al,T and y\_ar,T on figure 12, psi\_L,T = 9 and psi\_R,T = 0
Left abutment scour, y\_as = psi\_L,T (K\_1/0.55) = 9 ft Right abutment scour y\_as = psi\_R,T (K\_1/0.55) = 0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 50189140 Date 9-11-10 Initials RAL Region (A B C D)

Site \_\_\_\_\_ Location From I-29 Exit 86, 1E

$Q_{500} =$ 55,600 $$ by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_

Bridge discharge ( $Q_2$ ) = 55,600 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 322.5 ft. Flow angle at bridge = 15 ° Abut. Skew = 0 Effective Skew = 15 °

Width ( $W_2$ ) iteration = 316.5 310

Avg. flow depth at bridge,  $y_2$  iteration = 19.2 19.2

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 299.44 ft\*  $q_2 = Q_2/W_2 =$ 185.7 ft<sup>2</sup>/s

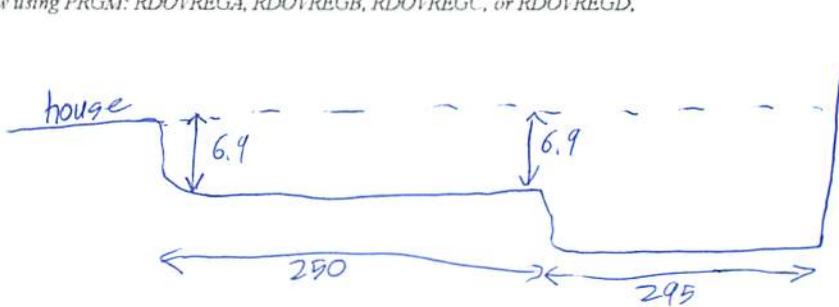
Bridge Vel.  $V_2 =$ 9.7 ft/s Final  $y_2 = q_2/V_2 =$ 19.2 ft  $\Delta h =$ 1.9 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$ 21.1 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 5.2 ft  
 Low Steel Elev. = 23.7 ft  
 $n$  (Channel) = 0.035  
 $n$  (LOB) = 0.085  
 $n$  (ROB) = 0.040  
 Pier Width = 2.2 ft  
 Pier Length = 31 ft  
 # Piers for 500 yr = 3 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$ 295 ft

Width of left overbank flow at approach,  $W_{lob} =$ 250 ft Average left overbank flow depth,  $y_{lob} =$ 6.9 ft

Width of right overbank flow at approach,  $W_{rob} =$ 0 ft Average right overbank flow depth,  $y_{rob} =$ 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ 1.3 From Figure 9  $W_2$  (effective) = 292.9 ft  $y_{cs} =$ 1.8 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(Y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 14 Correction factor for flow angle of attack (from Table 1),  $K_2 =$ 2.5

Froude # at bridge = 0.39 Using pier width  $a$  on Figure 11,  $\xi =$ 8.6 Pier scour  $y_{ps} =$ 18.7 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$ 6.9 ft right abutment,  $y_{aRT} =$ 0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$ 18.4 and  $\psi_{RT} =$ 0

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$ 18.4 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$ 0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Abutment

Route 2589+ Stream Big Sioux River MRM Date 9-11-10 Initials RRZ  
 Bridge Structure No. 50189140 Location from I29 Exit 86, IE  
 GPS coordinates: N43° 38.730' taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W96° 45.049' Datum of coordinates: WGS84 \_\_\_\_\_ NAD27 \_\_\_\_\_

Drainage area = 3089 sq. mi.  
 The average bottom of the main channel was 30.7 ft below top of guardrail at a point 167 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio \_\_\_\_\_ regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>33,200</u>			Q <sub>500</sub> = <u>55,600</u>		
Estimated flow passing through bridge	<u>33,200</u>			<u>55,600</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>

Riprap at abutments? \_\_\_\_\_ Yes \_\_\_\_\_ No  Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  
 Debris Potential?  High \_\_\_\_\_ Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?

Riprap  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know \_\_\_\_\_ NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- Pictures: 1 - Bridge Deck  
 2 - Left Overbank  
 3 - Right Overbank  
 4 - Looking Upstream  
 5 - Looking Downstream  
 6 - Left Abutment  
 7 - Right Abutment  
 8 - Pier 9

Notes: Extreme foliage caused difficulty seeing. Elevations were triangulated, Note Q500 very close to road overflow conditions.

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>33,200</u>	<u>55,600</u>
Flow depth at left abutment (yaLT), in feet	<u>2.2</u>	<u>6.9</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>0</u>
Contraction scour depth (yca), in feet	<u>1.7</u>	<u>1.8</u>
Pier scour depth (yps), in feet	<u>18.4</u>	<u>18.7</u>
Left abutment scour depth (yas), in feet	<u>9</u>	<u>18.4</u>
Right abutment scour depth (yas), in feet	<u>0</u>	<u>0</u>
IFlow angle of attack	<u>15</u>	<u>15</u>

See Comments/Diagram for justification where required