	SCOUR ANALYSIS AND REPORTING FORM Bridge Structure No. 50 192132 Date 9-12-10 Initials AAL Region (ABCD)							
	Bridge Structure No. 40192132 Date 9-12-10 Initials XXZ Region (ABCD) Site Location From Crooks, 3,3 E							
	Site Location From Crook9, 3,3 E $Q_{100} = 33,200$ by: drainage area ratio Vew flood freq. anal. regional regression eq. Bridge discharge (Q ₂) = $21,298$ (should be Q ₁₀₀ unless there is a relief bridge, road overflow, or bridge overtopping)							
PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method Bridge Width = $\frac{276}{100}$ ft. Flow angle at bridge = $\frac{3}{100}$ ° Abut. Skew = $\frac{3}{100}$ ° Effective Skew = $\frac{3}{100}$ ° Width (W ₂) iteration = $\frac{13}{100}$ Corrected channel width at bridge Section = W ₂ times cos of flow angle = $\frac{225}{100}$ Tft* $\frac{3}{100}$ q ₂ = $\frac{9}{100}$ q ₃ ft/s Bridge Vel, V ₂ = $\frac{6}{100}$ q ft/s Final y ₂ = $\frac{9}{100}$ q ₂ $\frac{9}{100}$ q ₃ ft *NOTE: repeat above calculations until y ₂ changes by less than 0.2 Effective pier width = L sin(a) + a cos(a) If y ₂ is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD, Water Surface Elev. = $\frac{1}{100}$ ft Low Steel Elev. = $\frac{1}{100}$ ft Low Steel Elev. = $\frac{1}{100}$ ft Channel) = $\frac{1}{100}$ $\frac{1}{100}$ ft ROB ROB Pier Width = $\frac{1}{100}$ ft Pier Length = $\frac{1}{100}$ ft ROB Pier Field) $\frac{1}{100}$ = $\frac{1}{100}$ ft ROB							
	CONTRACTION SCOUR 226							
PGRM: Contract	Width of main channel at approach section $W_1 = \frac{226}{1226}$ ft Width of left overbank flow at approach, $W_{lob} = \frac{226}{1226}$ ft Width of right overbank flow at approach, $W_{rob} = \frac{226}{1226}$ ft Average left overbank flow depth, $y_{lob} = \frac{2}{1226}$ ft Average right overbank flow depth, $y_{rob} = \frac{2}{1226}$ ft							
	<u>Live Bed Contraction Scour</u> (use if bed material is small cobbles or finer) $x = 1.98 \text{From Figure 9} W_2 \text{ (effective)} = 217.7 \text{ ft} y_{cs} = 2.5 \text{ ft}$							
PGRM: CWCSNEW								
PGRM: Pier	PIER SCOUR CALCULATIONS Correction factor for flow angle of attack (from Table 1), $K2 = 13$ Using pier width a on Figure 11, $\xi = 8$ Pier scour $y_{ps} = 8$ ft							
PGRM: Abutment	ABUTMENT SCOUR CALCULATIONS Average flow depth blocked by: left abutment, $y_{aLT} = 2$ ft right abutment, $y_{aRT} = 9$ ft Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through) Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = 9$ and $\psi_{RT} = 1.00$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 1.00$ ft							

Route Maple ton Rd Stream Big 9100X Bridge Structure No. 50192132 Loc	Rugr			9-17	-10	Del			
Route Maple ton Na Stream 119 1100x	NIVE	MRM	D	ate	Init	tials_ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	_		
Bridge Structure No. 50192132 Loc	cation _ Fr	om Crool	(9,71	25			_		
GPS coordinates: $1/43^{\circ}$ 39,442	taken from: USL abutment			centerline of î MRM end					
W96° 44,710	Datum of coordinates: WGS84			NAD27					
Bridge Structure No. $\frac{50192132}{43^{\circ}}$ Location From Crooks, $\frac{3.36}{3.36}$ GPS coordinates: $\frac{1000}{43^{\circ}}$ Location From Crooks, $\frac{3.36}{3.36}$ Taken from: USL abutment Coenterline of $\frac{1000}{1000}$ MRM end Datum of coordinates: WGS84 NAD27 Drainage area = $\frac{3688,62}{3688,62}$ sq. mi.									
The average bottom of the main channel was 10,7 ft below top of guardrail at a point 70 ft from left abutment.									
Method used to determine flood flows:Freq. Analdrainage area ratioregional regression equations.									
MISCELLANEOUS CONSIDERATIONS									
Estimated flow passing through bridge	$Q_{100} = 37,200$			$Q_{500} = 55,600$					
Estimated flow passing through bridge Estimated road overflow & overtopping		11.902		34,302					
Consideration	Yes No Possibly						à.		
Chance of overtopping	×	110	1 0001019	X	110	1 ossioly			
Chance of Pressure flow	×			×					
Armored appearance to channel		X			×				
Lateral instability of channel		7			X				
Riprap at abutments? YesNoMarginal									
Evidence of past Scour? Yes No Don't know									
Debris Potential?									
Does scour countermeasure(s) appear to have been designed?									
Riprap Yes No Don't know NA									
Spur Dike Y	es × N	loDor	't know	NA					
Other YesNoNA									
Bed Material Classification Based on Median Particle Size (D ₅₀)									
	Gravel			Cobbles		Boulders			
NAME OF THE PARTY				64-250		>250	-		
Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250									
Comments, Diagrams & orientation of digital photos									
1 hard pack									
7- I pot ing upstream 10-1 ow Road Section, I Flow would g									
7- Looking upstream 3- Looking Downstream 4- Left Overbank 5- Right Overbank 6- Left Abutment 6- Left Abutment									
4-Left Overbank North through ditch, over road, and pack through									
5-Right Overbant ather ditch Road is gravel,									
6-Left Abutment									
7-Right Abut ment Previous Bridge Parts Still Present.									
8-11-12									
Summary of Results									
	Q100			Q500					
Bridge flow evaluated	21,298			21,298					
Flow depth at left abutment (yaLT), in feet	21			3					
Flow depth at right abutment (yaRT), in feet	7 5								
Contraction scour depth (ycs), in feet Pier scour depth (yps), in feet	2,5 PP			Z, 5					
Left abutment scour depth (yas), in feet	8.8			8 6					
Right abutment scour depth (yas), in feet	11,5			11,5					
1Flow angle of attack	3				3				