

OK RT

check

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 50198140 Date 6/19/12 Initials Rat Region (A B C D) C  
 Site \_\_\_\_\_ Location 0.8 mi W of Renner on 2546 St  
 $Q_{100} =$  See notes, low steel by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 2579 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 62 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

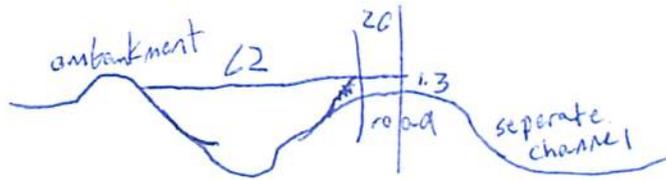
Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 62 ft\*  $q_2 = Q_2/W_2 =$  41.6 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  4.6 ft/s Final  $y_2 = q_2/V_2 =$  9.1 ft  $\Delta h =$  0.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = 0-1.0 ft  
 Low Steel Elev. = 9.1 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.026  
 $n$  (ROB) = 0.020 - gravel  
 Pier Width = 1.7 ft  
 Pier Length = 1.65 ft  
 # Piers for 100 yr = 2



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  62 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  20 ft Average right overbank flow depth,  $y_{rob} =$  1.3 ft

PGRM: Contract

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  0.79 From Figure 9  $W_2$  (effective) = 58.6 ft  $y_{cs} =$  1.2 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{cs50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{cs50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

PGRM: CWCSNEW

#### PIER SCOUR CALCULATIONS

L/a ratio = ~1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.27 Using pier width  $a$  on Figure 11,  $\xi =$  7 Pier scour  $y_{ps} =$  5.8 ft

PGRM: Pier

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  1.3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  5.5  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  5.5 ft

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 50198140 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D)

Site \_\_\_\_\_ Location 0.8 mi W of Renner on 258 St

$Q_{500}$  = \_\_\_\_\_ by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_

Bridge discharge ( $Q_2$ ) = \_\_\_\_\_ (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = \_\_\_\_\_ ft. Flow angle at bridge = \_\_\_\_\_ ° Abut. Skew = \_\_\_\_\_ ° Effective Skew = \_\_\_\_\_ °

Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = \_\_\_\_\_ ft\*  $q_2 = Q_2/W_2 =$  \_\_\_\_\_ ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  \_\_\_\_\_ ft/s Final  $y_2 = q_2/V_2 =$  \_\_\_\_\_ ft  $\Delta h =$  \_\_\_\_\_ ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  \_\_\_\_\_ ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft

Low Steel Elev. = \_\_\_\_\_ ft

n (Channel) = \_\_\_\_\_

n (LOB) = \_\_\_\_\_

n (ROB) = \_\_\_\_\_

Pier Width = \_\_\_\_\_ ft

Pier Length = \_\_\_\_\_ ft

# Piers for 500 yr = \_\_\_\_\_ ft

**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  \_\_\_\_\_ ft

Width of left overbank flow at approach,  $W_{lob} =$  \_\_\_\_\_ ft Average left overbank flow depth,  $y_{lob} =$  \_\_\_\_\_ ft

Width of right overbank flow at approach,  $W_{rob} =$  \_\_\_\_\_ ft Average right overbank flow depth,  $y_{rob} =$  \_\_\_\_\_ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_

Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  \_\_\_\_\_ ft right abutment,  $y_{aRT} =$  \_\_\_\_\_ ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  \_\_\_\_\_ and  $\psi_{RT} =$  \_\_\_\_\_

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  \_\_\_\_\_ ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  \_\_\_\_\_ ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie:

PRGM: Abutment

96.73653  
43.64538

960 44' 11.2294"  
430 38' 43.368"

2 11.1  
5 15.3  
10 23.3  
25 34.1  
50 45.2  
100 55.7  
500 81.6

Route 258 St Stream Dimension Ditch MRM \_\_\_\_\_ Date 6/19/12 Initials ReT  
 Bridge Structure No. 50198140 Location 0.8 mi W of Renner on 258 St  
 GPS coordinates: N 43 38' 43.711 taken from: USL abutment  centerline of  MRM end \_\_\_\_\_  
W 96 49' 11.411 Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 0.03 sq. mi.  
 The average bottom of the main channel was 12.7 ft below top of guardrail at a point 16 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

|                                       |  |                                     |                                     |                          |    |          |
|---------------------------------------|--|-------------------------------------|-------------------------------------|--------------------------|----|----------|
| Flows                                 | Q <sub>100</sub> = <del>2578</del> <u>2578</u> |                                     |                                     | Q <sub>500</sub> = _____ |    |          |
| Estimated flow passing through bridge | <u>2578</u>                                    |                                     |                                     |                          |    |          |
| Estimated road overflow & overtopping | <u>0</u>                                       |                                     |                                     |                          |    |          |
| Consideration                         | Yes  | No                                  | Possibly                            | Yes                      | No | Possibly |
| Chance of overtopping                 |  |                                     | <input checked="" type="checkbox"/> |                          |    |          |
| Chance of Pressure flow               |  |                                     | <input checked="" type="checkbox"/> |                          |    |          |
| Armored appearance to channel         |  | <input checked="" type="checkbox"/> |                                     |                          |    |          |
| Lateral instability of channel        |  | <input checked="" type="checkbox"/> |                                     |                          |    |          |

mid  
 Da 0.003  
 6/15  

|     |      |
|-----|------|
| 2   | 12.7 |
| 5   | 32.2 |
| 10  | 49   |
| 25  | 73.6 |
| 50  | 93   |
| 100 | 113  |
| 500 | 161  |

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal \_\_\_\_\_  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ *slight pier/contraction heavy abutment especially along left abutment (see picture).*  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Da 0.11  

|     |      |
|-----|------|
| 2   | 24.5 |
| 5   | 22.4 |
| 10  | 19.5 |
| 25  | 14.1 |
| 50  | 19.2 |
| 100 | 22.3 |
| 500 | 32.0 |

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA *rose quartz*  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

0.73 left  

|     |      |
|-----|------|
| 2   | 65.4 |
| 5   | 164  |
| 10  | 247  |
| 25  | 377  |
| 50  | 454  |
| 100 | 597  |
| 500 | 575  |

Comments, Diagrams & orientation of digital photos

- 1). left ab
- 2). main channel
- 3). right ab
- 4-5). right abutment
- 6-7). left abutment
- 8). pier

9-10). left abutment  
 11). main channel

Note stream stats  
 values are very low and  
 do no leave channel  
 evaluated ~~flow~~ flow  
 @ low steel. Highest water  
 mark ~ 3ft which is > Q<sub>500</sub>.

Summary of Results

|  |                       |      |
|--|-----------------------|------|
|  | Q100 <i>low steel</i> | Q500 |
| Bridge flow evaluated                        | <u>2578</u>           |      |
| Flow depth at left abutment (yaLT), in feet  | <u>0</u>              |      |
| Flow depth at right abutment (yaRT), in feet | <u>1.3</u>            |      |
| Contraction scour depth (yca), in feet       | <u>1.2</u>            |      |
| Pier scour depth (yca), in feet              | <u>5.8</u>            |      |
| Left abutment scour depth (yca), in feet     | <u>0</u>              |      |
| Right abutment scour depth (yca), in feet    | <u>5.5</u>            |      |
| IFlow angle of attack                        | <u>0</u>              |      |

See Comments/Diagram for justification where required