

OK TET

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 50199170 Date 6/20/12 Initials RAT Region (A B C D) C  
 Site \_\_\_\_\_ Location Silver CK + 60th St. N or SP38A  
 $Q_{100} =$  4320 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 4320 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

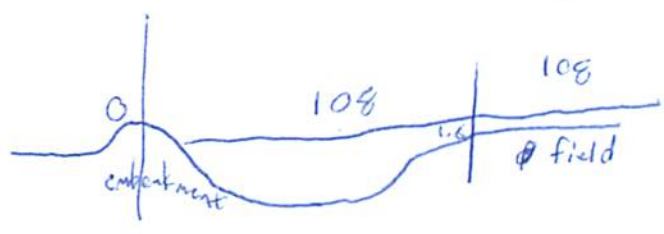
#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 99 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 99 ft\*  $q_2 = Q_2/W_2 =$  43.6 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.7 ft/s Final  $y_2 = q_2/V_2 =$  9.3 ft  $\Delta h =$  0.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9.8 ft

\*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-2.4 ft 15.6  
 Low Steel Elev. = 11.8 ft -3.8  
 $n$  (Channel) = 0.035 11.8  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.040  
 Pier Width = 6.65 ft  
 Pier Length = 1.65 ft  
 # Piers for 100 yr = 3 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  109 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  108 ft Average right overbank flow depth,  $y_{rob} =$  1.6 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  1.93 From Figure 9  $W_2$  (effective) = 94.1 ft  $y_{cs} =$  2.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1  
 Froude # at bridge = 0.27  
 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Using pier width  $a$  on Figure 11,  $\xi =$  6.9 Pier scour  $y_{ps} =$  5.7 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  1.6 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  6.6  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  6.6 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

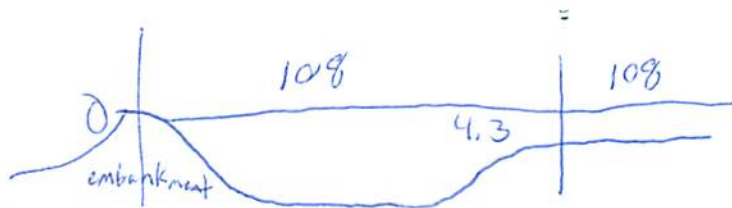
Bridge Structure No. 50199170 Date 6/20/12 Initials RLT Region ( A B C D ) D  
 Site \_\_\_\_\_ Location Silver Ck + 60th St N or SD38A  
 $Q_{500} =$  6927 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 6927 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 99 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 99 ft\*  $q_2 = Q_2/W_2 =$  70 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  5.9 ft/s Final  $y_2 = q_2/V_2 =$  11.9 ft  $\Delta h =$  0.7 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  12.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-6.1 ft  
 Low Steel Elev. = 11.9 ft  
 $n$  (Channel) = 0.035  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.040  
 Pier Width = 1.65 ft  
 Pier Length = 1.65 ft  
 # Piers for 500 yr = 3



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  109 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  109 ft Average right overbank flow depth,  $y_{rob} =$  4.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  3.98 From Figure 9  $W_2$  (effective) = 94.1 ft  $y_{cs} =$  4.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{cs0} = 0.0006 (q_2 / y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{cs0}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.3 Using pier width  $a$  on Figure 11,  $\xi =$  6.9 Pier scour  $y_{ps} =$  5.8 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  4.3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  13.8  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  13.8 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie:

PGRM: Abutment



43.60202

96.13987

167

43° 36' 7.272"

96° 43' 54.021"

SD384

Route 60th St N Stream Silver Ck MRM SM Date 6/29/12 Initials RAT  
 Bridge Structure No. 50199170 Location Silver Ck + 60th St N or SD384  
 GPS coordinates: N 43° 36' 7.4" taken from: USL abutment X centerline of ↑ MRM end X  
W 96° 43' 52.6" Datum of coordinates: WGS84 X NAD27 \_\_\_\_\_  
 Drainage area = 32.59 sq. mi.  
 The average bottom of the main channel was 15.6 ft below top of guardrail at a point 70 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio X regional regression equations.

32.59  
6118  
8/25

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>4320</u>			Q <sub>500</sub> = <u>6580</u>		
Estimated flow passing through bridge	<u>4320</u>			<u>6580</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<u>X</u>			<u>SM</u>	<u>X</u>
Chance of Pressure flow		<u>X</u>		<u>X</u>	<u>SM</u>	<u>X</u>
Armored appearance to channel		<u>X</u>			<u>X</u>	
Lateral instability of channel		<u>X</u>			<u>X</u>	

2 | 459  
5 |  
10 | 1130  
25 | 1730  
50 | 2650  
100 | 3450  
500 | 4320  
6580

Riprap at abutments? X Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal mostly on right hand side left abutment  
 Evidence of past Scour? X Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know marginal on left right  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med X Low lots of contraction, some abutment

Does scour countermeasure(s) appear to have been designed?  
 Riprap X Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA rose quartz along left abutment  
 Spur Dike \_\_\_\_\_ Yes X No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other X Yes X No \_\_\_\_\_ Don't know \_\_\_\_\_ NA -embankment built up along left abutment

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay X Sand X Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1) left CB
- 2) main channel
- 3) right CB
- 4) right abutment
- 5) piers
- 6) left abutments
- 7) left abutment
- 8) right abutment
- 9) right abutment - scour
- 10) main channel

Summary of Results

	Q <sub>100</sub>	Q <sub>500</sub>
Bridge flow evaluated	<u>4320</u>	<u>6580</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>1.6</u>	<u>4.3</u>
Contraction scour depth (yca), in feet	<u>2.5</u>	<u>4.6</u>
Pier scour depth (yca), in feet	<u>5.7</u>	<u>5.5</u>
Left abutment scour depth (yca), in feet	<u>0</u>	<u>0</u>
Right abutment scour depth (yca), in feet	<u>6.6</u>	<u>13.8</u>
IFlow angle of attack	<u>0</u>	<u>0</u>

See Comments/Diagram for justification where required