

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 50201173 Date 6/19/12 Initials RLT Region (A B C D) C  
 Site \_\_\_\_\_ Location on N Minnesota Ave 0.3 mi S of 261 St  
 $Q_{100}$  = See notes by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 85120 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 298 ft. Flow angle at bridge = 25 ° Abut. Skew = 35 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 298 ft\*  $q_2 = Q_2/W_2 = 290$  ft<sup>2</sup>/s

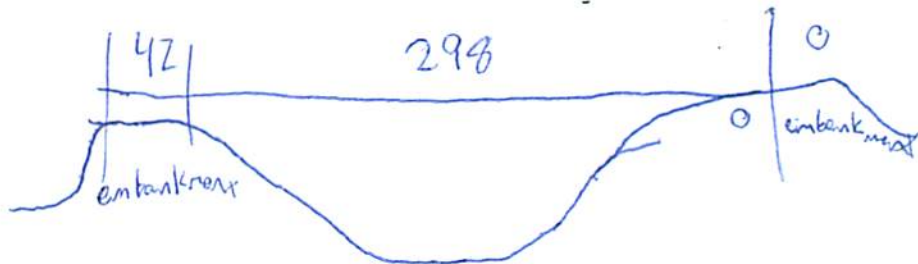
Bridge Vel,  $V_2 = 12.1$  ft/s Final  $y_2 = q_2/V_2 = 24$  ft  $\Delta h = 3$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 27$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(a) + a \cos(a)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 0-2.8 ft 31.4  
 Low Steel Elev. = 24.0 ft -7.4  
 $n$  (Channel) = 0.033  
 $n$  (LOB) = 0.020 - gravel  
 $n$  (ROB) = 0.030  
 Pier Width = 42 ft - rounded  
 Pier Length = 46 ft - constant  
 # Piers for 100 yr = 3 ft - face.



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 298$  ft

Width of left overbank flow at approach,  $W_{lob} = 42$  ft Average left overbank flow depth,  $y_{lob} = 1.4$  ft

Width of right overbank flow at approach,  $W_{rob} = 0$  ft Average right overbank flow depth,  $y_{rob} = 0$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 1.04$  From Figure 9  $W_2$  (effective) = 287.5 ft  $y_{cs} = 1.5$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 23

Correction factor for flow angle of attack (from Table 1),  $K_2 = 2$

Froude # at bridge = 0.44

Using pier width  $a$  on Figure 11,  $\xi = 8$  Pier scour  $y_{ps} = 14.1$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 0$  ft right abutment,  $y_{aRT} = 1.4$  ft

Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 0$  and  $\psi_{RT} = 5.9$

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 0$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 5.9$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment



**SCOUR ANALYSIS AND REPORTING FORM**

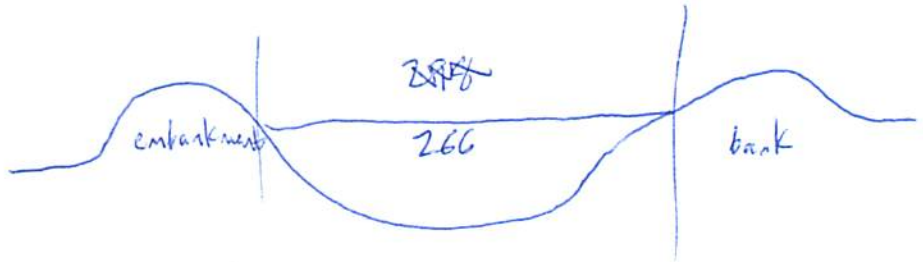
Bridge Structure No. 50201173 Date 8/19/12 Initials Lat Region (A B C D) C  
 Site \_\_\_\_\_ Location on N Minnesota Ave 0.3 mi S of 261 St  
 $Q_{500} =$  50,000 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 50,000 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 294 ft. <sup>233.47</sup> Flow angle at bridge = 25 ° Abut. Skew = 35 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = 264 260 270 265.9  
 Avg. flow depth at bridge,  $y_2$  iteration = 20.2 21.5 21.3  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 233.47 ft\*  $q_2 = Q_2/W_2 =$  189.4 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  93.97 ft/s Final  $y_2 = q_2/V_2 =$  19.3 ft  $\Delta h =$  1.9 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  21.3 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-2.9 ft  
 Low Steel Elev. = 24.0 ft  
 n (Channel) = 0.033  
 n (LOB) = 0.020  
 n (ROB) = 0.030  
 Pier Width = 2 ft  
 Pier Length = 46 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  266 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  0.33 From Figure 9  $W_2$  (effective) = 261.9 ft  $y_{cs} =$  0.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 23 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  2  
 Froude # at bridge = 0.39 Using pier width  $a$  on Figure 11,  $\xi =$  8 Pier scour  $y_{ps} =$  13.9 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

43.597

96.72867



Route N Minnesota Ave Stream Big Sioux Diversion MRM Date 1/19/12 Initials RAJ  
 Bridge Structure No. 50201173 Location N Minnesota Ave 0.3 mi S of 261st  
 GPS coordinates: N 43° 35' 49.20" taken from: USL abutment X centerline of ↑ MRM end \_\_\_\_\_  
W 96° 43' 43.61" Datum of coordinates: WGS84 X NAD27 \_\_\_\_\_

Drainage area = ? sq. mi.  
 The average bottom of the main channel was 31.4 ft below top of guardrail at a point 92 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio \_\_\_ regional regression equations.

Road width  
 crown  
 6.07  
 615

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>85120</u>			Q <sub>500</sub> = <u>50000</u>		
Estimated flow passing through bridge	<u>85120</u>			<u>50000</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping			<u>X</u>		<u>X</u>	
Chance of Pressure flow	<u>X</u>				<u>X</u>	
Armored appearance to channel		<u>X</u>			<u>X</u>	
Lateral instability of channel		<u>X</u>			<u>X</u>	

2	19.6
5	49.6
10	75.5
25	114
50	144
100	176
500	252

Riprap at abutments? X Yes \_\_\_ No \_\_\_ Marginal primarily on right abutment  
 Evidence of past Scour? \_\_\_ Yes X No \_\_\_ Don't know  
 Debris Potential? \_\_\_ High \_\_\_ Med X Low

32.66

2	460
5	1130
10	1730
25	2660
50	3150
100	4320
500	6520

Does scour countermeasure(s) appear to have been designed?  
 Riprap X Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA rose quartz up and down  
 Spur Dike \_\_\_ Yes X No \_\_\_ Don't know \_\_\_ NA both banks/abutments  
 Other X Yes X No \_\_\_ Don't know \_\_\_ NA man made banks @ road the height

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material	Silt/Clay <u>X</u>	Sand ___	Gravel ___	Cobbles ___	Boulders ___
Size range, in mm	<0.062	0.062-2.00	2.00-64	64-250	>250

Comments, Diagrams & orientation of digital photos

- 1). left ab
- 2). main channel
- 3). right ab
- 4). piers
- 5). right abutment
- 6). left abutment
- 7). left abutment
- 8-9). right abutment
- 10). main channel

Notes: Used low Steel as estimate as streambanks does not reflect the flow, also calculated @ Q<sub>500</sub> as that's similar to Q<sub>100</sub> for Sioux river

Summary of Results

	Q <sub>100</sub>	Q <sub>500</sub>
Bridge flow evaluated	<u>85120</u>	<u>50000</u>
Flow depth at left abutment (yaLT), in feet	<u>1.4</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>0</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>1.5</u>	<u>0.6</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>14.1</u>	<u>13.9</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>0</u>	<u>0</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>5.9</u>	<u>0</u>
Flow angle of attack	<u>10</u>	<u>10</u>

See Comments/Diagram for justification where required