

OK

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 50202018 Date 6/26/12 Initials RAT Region (A B C D) D  
 Site \_\_\_\_\_ Location W 3<sup>rd</sup> St in Dell Rapids just w of Hwy 115  
 $Q_{100} =$  610 872 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 872 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 47 ft. Flow angle at bridge = 85.5° Abut. Skew = 40° Effective Skew = 5°  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

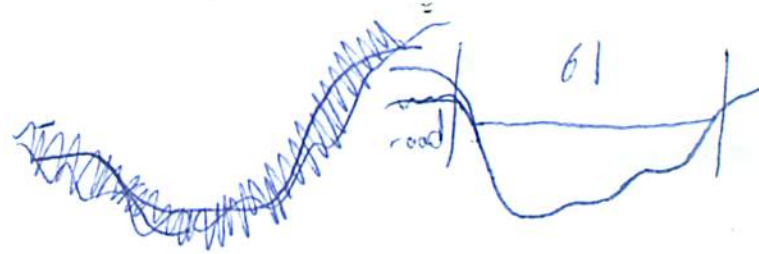
Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 46.82 ft\*  $q_2 = Q_2/W_2 =$  18.6 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  3.1 ft/s Final  $y_2 = q_2/V_2 =$  6.1 ft  $\Delta h =$  0.2 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  6.3 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 0-0.2 ft  
 Low Steel Elev. = 7.4 ft  
 $n$  (Channel) = 0.040 - smooth & uniform rock cut.  
 $n$  (LOB) = 0.016 asphalt  
 $n$  (ROB) = 0.030  
 Pier Width = 0 ft  
 Pier Length = 0 ft  
 # Piers for 100 yr = 0 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  61 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  1.91 From Figure 9  $W_2$  (effective) = 46.8 ft  $y_{cs} =$  2.4 ft - see notes

#### Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  0  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

$5.233 / 5.35$   
 $12^\circ$

**SCOUR ANALYSIS AND REPORTING FORM**

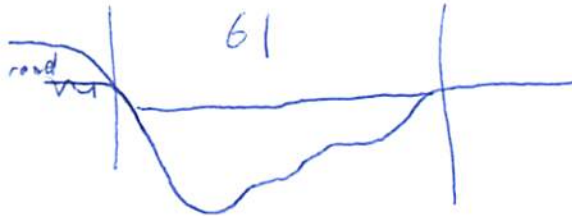
Bridge Structure No. 50202018 Date 4/26/12 Initials pat Region (A B C D) D  
 Site \_\_\_\_\_ Location W 3rd St in Dell Rapids just W of Hwy 115  
 $Q_{500} =$  Q<sub>25</sub> 1340 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1287 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 47 ft. Flow angle at bridge = 30.45° Abut. Skew = 40° Effective Skew = 5°  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 46.82 ft\*  $q_2 = Q_2/W_2 =$  29.6 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  3.8 ft/s Final  $y_2 = q_2/V_2 =$  7.6 ft  $\Delta h =$  0.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.9 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-0.2 ft  
 Low Steel Elev. = 7.4 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.016  
 $n$  (ROB) = 0.030  
 Pier Width = 0 ft  
 Pier Length = 0 ft  
 # Piers for 500 yr = 0 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  61 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  2.36 From Figure 9  $W_2$  (effective) = 46.8 ft  $y_{cs} =$  2.9 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment



96.71932  
43.52268

96.43, 9.55211  
43.49, 21.64811

Route W 3<sup>rd</sup> St Stream \_\_\_\_\_ MRM \_\_\_\_\_ Date 6/26/12 Initials RAJ  
 Bridge Structure No. 50202018 Location W 3<sup>rd</sup> St. in Dell Rapids just W of Hwy 115  
 GPS coordinates: N 42° 49' 22.1'' taken from: USL abutment  centerline of  MRM end \_\_\_\_\_  
W 96° 43' 9.6'' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 10.12 sq. mi.  
 The average bottom of the main channel was 13 ft below top of guardrail at a point 35 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = Q <sub>10</sub> <u>872</u>			Q <sub>500</sub> = Q <sub>25</sub> <u>1340</u>		
Estimated flow passing through bridge	<u>872</u>			<u>1287</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>63</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

10.12  
619  
8725  
2 226  
5 567  
10 872  
25 1340  
50 1740  
100 2170  
500 3290

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal mostly gravel sized rose quartz on right abutment  
 Evidence of past Scour? \_\_\_ Yes  No  Don't know - doesn't appear anything can be easily eroded  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_ Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

see picture 9 - bed is ~~essentially~~ basically one slight slab of rose quartz (bedrock)

- Comments, Diagrams & orientation of digital photos
- 1). right ab
  - 2). main
  - 3). left ab.
  - 4). right abutment scour
  - 5-6). right abutment
  - 7-8). left abutment
  - 9). bed material
  - 10). main channel

Notes: Bridge bed was ~~essentially~~ a single flat sheet of rose quartz with little other material. erosion would likely be less.

Summary of Results

	Q <sub>100</sub> Q <sub>10</sub>	Q <sub>500</sub> Q <sub>25</sub>
Bridge flow evaluated	<u>872</u>	<u>1287</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>0</u>
Contraction scour depth (y <sub>c</sub> s), in feet	<u>2.4</u>	<u>2.9</u>
Pier scour depth (y <sub>p</sub> s), in feet	<u>N/A</u>	<u>N/A</u>
Left abutment scour depth (y <sub>a</sub> s), in feet	<u>0</u>	<u>0</u>
Right abutment scour depth (y <sub>a</sub> s), in feet	<u>0</u>	<u>0</u>
Flow angle of attack	<u>5</u>	<u>5</u>

Note: abutment walls are sloped  
120

See Comments/Diagram for justification where required