

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 50203205 Date 6/25/12 Initials RAT Region (A B C D) C
Site Location 6th St & Big Sioux River in SF
Q100 = Q25 31700 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = 31700 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 232 ft. Flow angle at bridge = 19 degrees Abut. Skew = 10 degrees Effective Skew = 5 degrees
Width (W2) iteration = Pier skew 100

Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 231.12 ft\* q2 = Q2/W2 = 137.2 ft^2/s

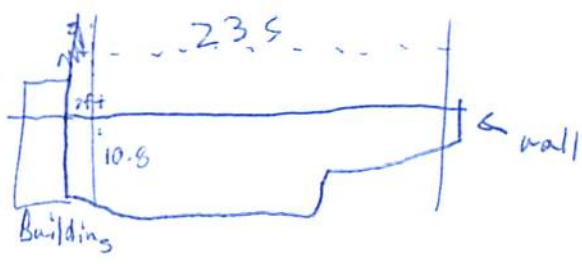
Bridge Vel, V2 = 8.3 ft/s Final y2 = q2/V2 = 16.5 ft Delta h = 1.4 ft

Average main channel depth at approach section, y1 = Delta h + y2 = 17.9 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-4.4 ft
Low Steel Elev. = 17.0 ft
n (Channel) = 0.025
n (LOB) = 0.030
n (ROB) = 0.020
Pier Width = 1.55 ft
Pier Length = 59.59 ft
# Piers for 100 yr = 3

1.75 + 0.6 = 2.35
23.9
6.9
17.0
16.4
-6.
9.9
V-face w/
Steel protector.



CONTRACTION SCOUR

Width of main channel at approach section W1 = 232 ft
Width of left overbank flow at approach, Wlob = 67 ft Average left overbank flow depth, ylob = 10.8 ft
Width of right overbank flow at approach, Wrob = 70 ft Average right overbank flow depth, yrob = 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 0.64 From Figure 9 W2 (effective) = 226.5 ft ycs = 1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = Average approach velocity, V1 = Q100/(y1 W1) =
Critical approach velocity, Vc = 11.17 y1^(1/6) D50^(1/3) =
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^(7/6))^3 = If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [(q2/(D50^(1/3) y1^(7/6)))^(6/7) - y1 = From Figure 10, ycs =

PIER SCOUR CALCULATIONS

L/a ratio = 38 Correction factor for flow angle of attack (from Table 1), K2 = 1.5
Froude # at bridge = 0.36 Using pier width a on Figure 11, xi = 6.6 Pier scour yps = 8.5 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 10.8 ft right abutment, yarT = 0 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 22 and psiRT = 0
Left abutment scour, yas = psiLT (K1/0.55) = 40 ft Right abutment scour yas = psiRT (K1/0.55) = 0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment



**SCOUR ANALYSIS AND REPORTING FORM**

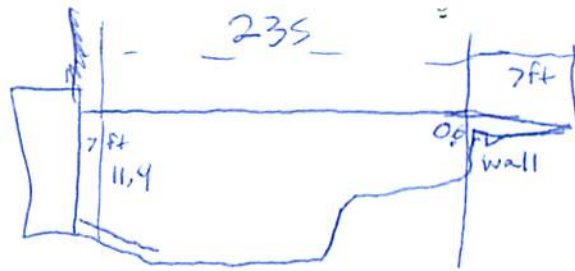
Bridge Structure No. 50203205 Date 6/29/12 Initials Rat Region (A B C D)  
 Site \_\_\_\_\_ Location 6<sup>th</sup> St + Big Sioux River in SF  
 $Q_{500} = Q_{50}$  41900 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 33601 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 232 ft. Flow angle at bridge = 15 ° Abut. Skew = 10 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 231.12 ft\*  $q_2 = Q_2/W_2 =$  145.4 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  6.6 ft/s Final  $y_2 = q_2/V_2 =$  17 ft  $\Delta h =$  1.5 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  18.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-4.4 ft  
 Low Steel Elev. = 17.0 ft  
 n (Channel) = 0.025  
 n (LOB) = 0.030  
 n (ROB) = 0.020  
 Pier Width = 1.55 ft  
 Pier Length = 59 ft  
 # Piers for 500 yr = 3 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  232 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  7 ft Average left overbank flow depth,  $y_{lob} =$  11.4 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  7 ft Average right overbank flow depth,  $y_{rob} =$  0.6 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)  
 $x =$  0.67 From Figure 9  $W_2$  (effective) = 226.5 ft  $y_{cs} =$  1.1 ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 38 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.5  
 Froude # at bridge = 0.37 Using pier width a on Figure 11,  $\xi =$  6.6 Pier scour  $y_{ps} =$  8.5 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  11.4 ft  $K_2 =$  1.5 right abutment,  $y_{aRT} =$  0.6 ft  $K_2 =$  0.55  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  22.5 and  $\psi_{RT} =$  2.7  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  40.9 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  2.7 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

43,55123

96.72363



Route 6th St Stream Big Sioux River MRM \_\_\_\_\_ Date 6/29/12 Initials Rat  
 Bridge Structure No. 50203205 Location 6th St on Big Sioux River in SF  
 GPS coordinates: N 43° 33' 4.31" taken from: USL abutment X centerline of ↑ MRM end \_\_\_\_\_  
W 96° 43' 29.21" Datum of coordinates: WGS84 X NAD27 \_\_\_\_\_

Drainage area = 3772.76 sq. mi.  
 The average bottom of the main channel was 23.9 ft below top of guardrail at a point 45 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio X regional regression equations.

3772.76  
 6/13  
 2 | 5540  
 5 | 13300  
 10 | 20400  
 25 | 31700  
 50 | 41900  
 100 | 53300  
 500 | 85100

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = Q <sub>25</sub> = 31700			Q <sub>500</sub> = Q <sub>50</sub> 41900		
Estimated flow passing through bridge	31700			33601		
Estimated road overflow & overtopping	0			8299		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<del>Yes</del>	X	X		
Chance of Pressure flow	X			X		
Armored appearance to channel		X			X	
Lateral instability of channel		X			X	

Riprap at abutments? \_\_\_ Yes X No \_\_\_ Marginal  
 Evidence of past Scour? \_\_\_ Yes \_\_\_ No X Don't know *likely some pier contraction, unable to look @ left abutment*  
 Debris Potential? \_\_\_ High \_\_\_ Med X Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes X No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes X No \_\_\_ Don't know \_\_\_ NA  
 Other X Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA

*-Bike trail on right abutment prevents overbank flow, cement filled abutment under bridge.*

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material	Silt/Clay <u>X</u>	Sand ___	Gravel ___	Cobbles ___	Boulders ___
Size range, in mm	<0.062	0.062-2.00	2.00-64	64-250	>250

Comments, Diagrams & orientation of digital photos

- 1). left ab
- 2). main channel
- 3). right ab
- 4). pier
- 5-6). right abutment
- 7-8). left abutment
- 9). main channel

*Notes made to reach left abutment due to contract construction and steep wall downstream of bridge. However there is about 7ft of exposed abutment & very susceptible to scour.*

Summary of Results

	Q <sub>100</sub> Q <sub>25</sub>	Q <sub>500</sub> Q <sub>50</sub>
Bridge flow evaluated	31700	33601
Flow depth at left abutment (yaLT), in feet	10.8	11.4
Flow depth at right abutment (yaRT), in feet	0	0.6
Contraction scour depth (y <sub>cs</sub> ), in feet	1	1.1
Pier scour depth (y <sub>ps</sub> ), in feet	8.5	6.5
Left abutment scour depth (y <sub>as</sub> ), in feet	10.40	4.09
Right abutment scour depth (y <sub>as</sub> ), in feet	0	2.7
Flow angle of attack	5	5

See Comments/Diagram for justification where required