

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 5021012 Date 6/19/12 Initials PAJ Region (A B C D) C
Site Location Cliff Ave & Big Sioux River
Q100 = 53300 by: drainage area ratio flood freq. anal. regional regression eq. Y
Bridge discharge (Q2) = 53300 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 303 ft. Flow angle at bridge = 10 degrees Abut. Skew = 15 degrees Effective Skew = 5 degrees
Width (W2) iteration = - see notes

Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 301.85 ft\* q2 = Q2/W2 = 176.6 ft^2/s

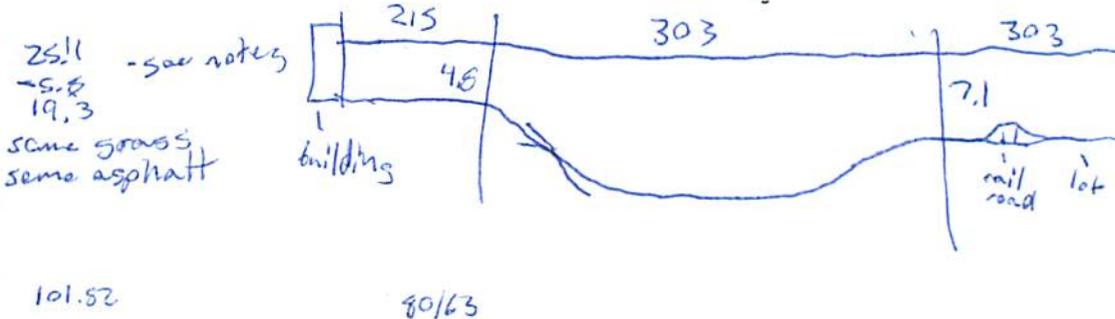
Bridge Vel, V2 = 9.4 ft/s Final y2 = q2/V2 = 18.7 ft Delta h = 1.8 ft

Average main channel depth at approach section, y1 = Delta h + y2 = 20.6 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(a) + a cos(a)

If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 07.6 ft
Low Steel Elev. = 19.3 ft
n (Channel) = 0.045
n (LOB) = 0.020
n (ROB) = 0.020
Pier Width = 1.2 ft
Pier Length = 19 ft
# Piers for 100 yr = 4



CONTRACTION SCOUR

Width of main channel at approach section W1 = 303 ft
Width of left overbank flow at approach, Wlob = 215 ft Average left overbank flow depth, ylob = 4.8 ft
Width of right overbank flow at approach, Wrob = 303 ft Average right overbank flow depth, yrob = 7.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 11.38 From Figure 9 W2 (effective) = 297.1 ft ycs = 12.4 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s

Critical approach velocity, Vc = 11.17 y1^(1/6) D50^(1/3) = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006 (q2/y1^(7/6))^3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122 y1 [q2 / (D50^(1/3) y1^(7/6))]^(6/7) - y1 = ft From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 57.5 Correction factor for flow angle of attack (from Table 1), K2 = 1.5
Froude # at bridge = 0.38 Using pier width a on Figure 11, xi = 5.5 Pier scour yps = 7.1 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 4.8 ft right abutment, yarT = 7.1 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 14.7 and psiRT = 18.8
Left abutment scour, yas = psiLT (K1/0.55) = 26.7 ft Right abutment scour yas = psiRT (K1/0.55) = 34.1 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

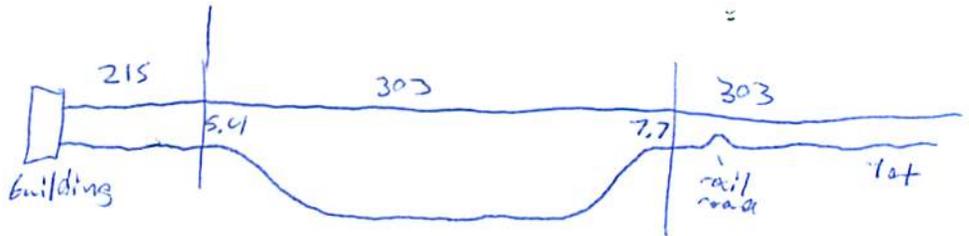
Bridge Structure No. 56210212 Date 6/19/12 Initials Rat Region (A B C D) C  
 Site \_\_\_\_\_ Location Cliff Arc + Big Sioux River  
 $Q_{500} =$  45000 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 56592 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 303 ft. Flow angle at bridge = 10 ° Abut. Skew = 15 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 301.85 ft\*  $q_2 = Q_2/W_2 =$  187.5 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  9.7 ft/s Final  $y_2 = q_2/V_2 =$  19.3 ft  $\Delta h =$  1.9 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  21.2 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1.6 ft  
 Low Steel Elev. = 19.3 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.020  
 $n$  (ROB) = 0.020  
 Pier Width = 1.2 ft  
 Pier Length = 69 ft  
 # Piers for 500 yr = 4



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  303 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  215 ft Average left overbank flow depth,  $y_{lob} =$  5.4 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  303 ft Average right overbank flow depth,  $y_{rob} =$  7.7 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  12.95 From Figure 9  $W_2$  (effective) = 297.1 ft  $y_{cs} =$  13.9 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 57.5 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.5  
 Froude # at bridge = 0.39 Using pier width a on Figure 11,  $\xi =$  5.5 Pier scour  $y_{ps} =$  7.1 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.4 ft right abutment,  $y_{aRT} =$  7.7 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  15.7 and  $\psi_{RT} =$  19.5  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  28.6 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  35.5 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

68215'21  
1211L'26

Route Cliff Ave Stream Big Sioux River MRM \_\_\_\_\_ Date 6/19/12 Initials RAT  
 Bridge Structure No. 50210212 Location Cliff Ave & Big Sioux River  
 GPS coordinates: N 43° 32' 31.3" taken from: USL abutment > centerline of ↑ MRM end \_\_\_\_\_  
W 96° 42' 40.3" Datum of coordinates: WGS84 x NAD27 \_\_\_\_\_

Drainage area = 3770.94 sq. mi.  
 The average bottom of the main channel was 825.1 ft below top of guardrail at a point 198 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio X regional regression equations.

3770.94  
 6/13  
 2 5540  
 5 3300  
 10 20400  
 25 31700  
 50 41900  
 100 53300  
 500 85000

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>53300</u>			Q <sub>500</sub> = <u>85000</u>		
Estimated flow passing through bridge	<u>53300</u>			<u>56582</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>28418</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping	<u>X</u>		<u>W</u>	<u>X</u>		
Chance of Pressure flow	<u>X</u>		<u>W</u>	<u>X</u>		
Armored appearance to channel		<u>X</u>			<u>X</u>	
Lateral instability of channel		<u>X</u>			<u>X</u>	

Riprap at abutments? X Yes \_\_\_ No X Marginal *- all on right abutment*  
 Evidence of past Scour? \_\_\_ Yes X No \_\_\_ Don't know *very little pier/contraction*  
 Debris Potential? \_\_\_ High \_\_\_ Med X Low

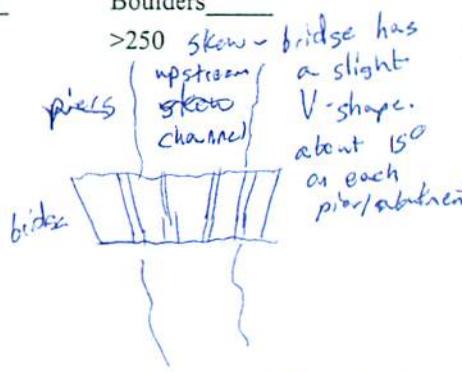
Does scour countermeasure(s) appear to have been designed?  
 Riprap X Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA *eye quartz on right abutment*  
 Spur Dike \_\_\_ Yes X No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes X No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay X Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1) left ab
  - 2) main channel
  - 3) right ab
  - 4-5) piers - metal cover, V-face
  - 6-7) left abutment
  - 8-9) right abutment
- k). main channel*



Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>53300</u>	<u>56582</u>
Flow depth at left abutment (yaLT), in feet	<u>4.8</u>	<u>5.4</u>
Flow depth at right abutment (yaRT), in feet	<u>7.1</u>	<u>7.7</u>
Contraction scour depth (yca), in feet	<u>12.4</u>	<u>13.9</u>
Pier scour depth (ypp), in feet	<u>7.1</u>	<u>7.1</u>
Left abutment scour depth (yaa), in feet	<u>26.7</u>	<u>29.6</u>
Right abutment scour depth (yaa), in feet	<u>34.1</u>	<u>35.5</u>
Flow angle of attack	<u>5</u>	<u>5</u>

low steel  
 - took low steel from mean channel depth location. Bridge crests like a hill.

See Comments/Diagram for justification where required