

~~Re-do wrong Q values used~~

~~OK RT~~ OK RT

### SCOUR ANALYSIS AND REPORTING FORM

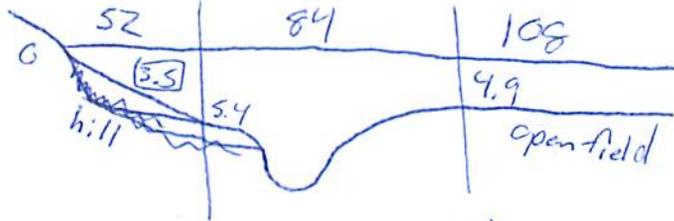
Bridge Structure No. 50232140 Date 6/19/12 Initials Pat Region (A B C D) C  
 Site \_\_\_\_\_ Location 2.2 mi E of Renner corner on 2585  
 $Q_{100} =$  3990 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 3990 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 108 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = 108 74 88 84  
 Avg. flow depth at bridge,  $y_2$  iteration = 8.5 10.2 9.4 9.6  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 84 ft\*  $q_2 = Q_2/W_2 =$  46.2 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.8 ft/s Final  $y_2 = q_2/V_2 =$  9.6 ft  $\Delta h =$  0.5 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  10.1 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2  
 Effective pier width =  $L \sin(a) + a \cos(a)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1.0 ft  
 Low Steel Elev. = 13.4 ft  
 n (Channel) = 0.033  
 n (LOB) = 0.030  
 n (ROB) = 0.030  
 Pier Width = 2.35 ft  
 Pier Length = 2.35 ft  
 # Piers for 100 yr = 2 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  84 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  52 ft Average left overbank flow depth,  $y_{lob} =$  3.5 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  108 ft Average right overbank flow depth,  $y_{rob} =$  4.9 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  6.38 From Figure 9  $W_2$  (effective) = 79.3 ft  $y_{cs} =$  7.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.27 Using pier width a on Figure 11,  $\xi =$  9.1 Pier scour  $y_{ps} =$  7.5 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.5 ft right abutment,  $y_{aRT} =$  4.9 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  12.4 and  $\psi_{RT} =$  14.8  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  12.4 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  14.8 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

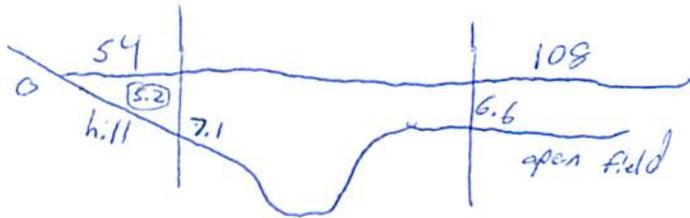
Bridge Structure No. 50232140 Date 6/19/12 Initials RAT Region (A B C D) C  
 Site \_\_\_\_\_ Location 2.2 mi E of Renner Corner on 256 St  
 $Q_{500} =$  5000 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = \_\_\_\_\_ (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 108 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = 108 91 94  
 Avg. flow depth at bridge,  $y_2$  iteration = 10.4 11.3 11.2  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 94 ft\*  $q_2 = Q_2/W_2 =$  62.6 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  5.6 ft/s Final  $y_2 = q_2/V_2 =$  11.2 ft  $\Delta h =$  0.6 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  11.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1.0 ft  
 Low Steel Elev. = 13.4 ft  
 $n$  (Channel) = 0.033  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.030  
 Pier Width = 2.35 ft  
 Pier Length = 2.35 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  94 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  54 ft Average left overbank flow depth,  $y_{lob} =$  5.2 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  108 ft Average right overbank flow depth,  $y_{rob} =$  6.6 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  8.58 From Figure 9  $W_2$  (effective) = 89.3 ft  $y_{cs} =$  9.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.29 Using pier width  $a$  on Figure 11,  $\xi =$  9.1 Pier scour  $y_{ps} =$  7.6 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.2 ft right abutment,  $y_{aRT} =$  6.6 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  15.4 and  $\psi_{RT} =$  17.9  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  15.4 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  ~~17.9~~ 17.9 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Handwritten text in the top left corner, possibly a header or reference number.

96.6762  
43.4953

Vertical handwritten text on the right side of the page, possibly a date or location.

96° 40' 3.432"  
43° 38' 43.081"

Red scribbled-out text or markings in the lower middle section.

Route 258 St Stream \_\_\_\_\_ MRM \_\_\_\_\_ Date 6/19/12 Initials RJT  
 Bridge Structure No. 50232-140 Location 2.2 mi E of Renner Corner on 258 St  
 GPS coordinates: N 43° 36' 44.8" W 96° 40' 13.3" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
N 36° 3.4' W 96° 40' 13.3" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_  
 Drainage area = 24.7 sq. mi. ~~24.7~~ *correct location*  
 The average bottom of the main channel was 17.4 ft below top of guardrail at a point 73 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>3880</u>			Q <sub>500</sub> = <u>5880</u>		
Estimated flow passing through bridge	<u>3880</u>			<u>5880</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

6/15  
 2 419  
 5 1030  
 10 1570  
 25 2400  
 50 3100  
 100 3880  
 500 5880

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know *minor contraction is all*  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

*wrong Q values*  
~~419~~  
~~1030~~  
~~1570~~  
~~2400~~  
~~3100~~  
~~3880~~  
~~5880~~

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA *raise quartz on upstream abutment*  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand  Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1). left ab
- 2). main channel
- 3). right ab
- 4). right abutment
- 5). left abutment
- 6). left abutment
- 7). right abutment
- 8). right abutment
- 9). left abutment
- 10). main channel

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>3880</u>	<u>5880</u>
Flow depth at left abutment (yaLT), in feet	<u>3.5</u>	<u>5.2</u>
Flow depth at right abutment (yaRT), in feet	<u>4.9</u>	<u>6.6</u>
Contraction scour depth (y <sub>c</sub> ), in feet	<u>7.1</u>	<u>9.5</u>
Pier scour depth (y <sub>p</sub> ), in feet	<u>7.5</u>	<u>7.6</u>
Left abutment scour depth (y <sub>a</sub> ), in feet	<u>12.5</u> <u>12.4</u>	<u>15.4</u>
Right abutment scour depth (y <sub>a</sub> ), in feet	<u>14.8</u>	<u>17.9</u>
IFlow angle of attack	<u>0</u>	<u>0</u>

See Comments/Diagram for justification where required