	SCOUR ANALYSIS AND REPORTING FORM
	Bridge Structure No. 50277150 Date 10-8-10 Initials FH Region (ABCD)
	Site Location From I-90 Exit 406, 1.5 N 0.5 W
	O ₁₀₀ = 27600 by: drainage area ratio flood freq. anal. regional regression eq
	Bridge discharge $(Q_2) = 27600$ (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)
	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method
	Bridge Width = $\frac{238}{100}$ ft. Flow angle at bridge = $\frac{35}{100}$ Abut. Skew = $\frac{25}{100}$ Effective Skew = $\frac{100}{100}$
gionl)"	Width (W ₂) iteration = $\frac{238}{228}$ $\frac{228}{226}$
	Avg. flow depth at bridge, y_2 iteration = 19.79 15.6 15.7 15.6 15.7
	Corrected channel width at bridge Section = W_2 times cos of flow angle = $\frac{272.6}{1}$ ft* $q_2 = Q_2/W_2 = \frac{124}{1}$ ft²/s
	Bridge Vel, $V_2 = 7$ ft/s Final $y_2 = q_2/V_2 = 15$ ft $\Delta h = 13$ ft
	Average main channel depth at approach section, $y_1 = \Delta h + y_2 = ft$
	* NOTE: repeat above calculations until y 2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q) If y 2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,
	Water Surface Elev. = 3 ft Bridge Section, 725
	Low Steel Elev. = Average 17 ft
	$n \text{ (Channel)} = \frac{0.028}{0.028}$
	$ \frac{n \text{ (LOB)} = 0.03}{n \text{ (ROB)} = 0.03} \text{(Jert Wall)} $
	Pier Width = 2,5 ft upgft such, Vert, Wall Fields
	Pier Length = 35 ft
	# Piers for $100 \text{ yr} = ft$
	CONTRACTION SCOUR 226'
	Width of main channel at approach section $W_1 = 226$ ft
act	Width of left overbank flow at approach $W_{t,t} = 0$ ft Average left overbank flow depth, $y_{lob} = 0$
ontr	Width of right overbank flow at approach, $W_{rob} = 130$ ft Average right overbank flow depth, $y_{rob} = 4.75$ ft
PGRM: Contract	Width of fight overbank now at approach, Wrob
PGR	Live Bed Contraction Scour (use if bed material is small cobbles or finer)
	$x = 1.57$ From Figure 9 W_2 (effective) = 220 ft $y_{es} = 21$ ft
PGRM: CWCSNEW	Clear Water Contraction Scour (use if bed material is larger than small cobbles) Estimated bed material $D_{50} = $ ft Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = $ ft/s
VCS	Critical approach velocity, $Vc = 11.52y_1^{1/6}D_{50}^{-1/3} = $ ft/s
I: CV	If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
BRM	$P_{1} = 0.0006(a_{1}/v_{0}^{7/6})^{3} = 0.0006(a_{2}/v_{0}^{7/6})^{3} = 0.0006(a_{2}/v_{0}^{$
P	$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =ft If D_{50} >= D_{c50}, \chi = 0.0$ Otherwise, $\chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 =ft$
	Otherwise, $\chi = 0.12291[42/(D_{30} - y_1 - y_1)]$
icr	PIER SCOUR CALCULATIONS
GRM: Pier	L/a ratio = Correction factor for flow angle of attack (from Table 1), $K2 = \frac{1}{16\pi^2}$
PGR	Froude # at bridge = $\frac{9}{2.3}$ PIER SCOUR CALCULATIONS Correction factor for flow angle of attack (from Table 1), K2 = $\frac{2}{2.5}$ Using pier width a on Figure 11, $\xi = \frac{9}{2.5}$ Pier scour $y_{ps} = \frac{16}{2.5}$ ft
	ABUTMENT SCOUR CALCULATIONS
ent	$g = 1$ th Marked how Left shutment $y = 0$ ft right abutment $y_{nx} = 0$ ft
butn	Shape coefficient K ₂ = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
PGRM: Abutment	Shape coefficient K_1 = 1.00 for vertical-wall, Using values for y_{aLT} and y_{aRT} on figure 12, ψ_{LT} = 0.82 for vertical-wall with wingwalls, and ψ_{RT} = 1.00 for spill-through with wingwalls, ψ_{LT} = 1.00 for vertical-wall wi
PGR	Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = $ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = $ ft

PGRM: "RegionA", "RegionB".

PGRM: Contract

	SCOUR ANALYSIS AND REPORTING FORM					
	Bridge Structure No. 50277150 Date 10-0-10 Initials Region (A BCD)					
	by: drainage area ratio flood freq. anal. regional regression eq					
	Bridge discharge $(Q_2) = 34076$ (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)					
PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method Bridge Width = $\frac{1}{2}$ $\frac{1}{2}$ ft. Flow angle at bridge = $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ Abut. Skew = $\frac{1}{2}$					
	CONTRACTION SCOUR					
_	Width of main channel at approach section $W_1 = \frac{235}{0}$ ft A verage left overbank flow depth, $y_{tob} = 0$ ft					
ntraci	Width of left overbank flow at approach, W _{lob} = it					
1: Co	Width of right overbank flow at approach, $W_{rob} = \frac{120}{100}$ ft Average right overbank flow depth, $y_{rob} = \frac{120}{100}$ ft					
PGRM: Contract	Live Bed Contraction Scour (use if bed material is small cobbles or finer)					
Δ.	Live Bed Contraction Scour (use if bed material is small coobles of filler) $x = \frac{1}{2} \frac{2}{3} \text{From Figure 9} \qquad W_2 \text{ (effective)} = \frac{2}{3} \frac{9}{9} \text{ft} \qquad y_{cs} = \frac{1}{3} \frac{9}{9} \text{ft}$					
	Grant Control of Security Secu					
PGRM: CWCSNEW	Estimated bed material D_{50} = ft Average approach velocity, $V_1 = Q_{500}/(y_1W_1) = \underline{\qquad}$ It/S					
WCS	Gaiting Lamproach velocity $V_C = 11.52 \text{ y.}^{10} D_{50}^{10} = 10.5$					
M: C	$16V < V$ and $D_{xx} >= 0.2$ ft use clear water equation below, otherwise use live bed scour equation above.					
PGR	$\begin{array}{lll} D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = & & \text{If } D_{50} >= D_{c50}, \chi = 0.0 \\ \text{Otherwise, } \chi = 0.122y_1[q_2/(D_{50}^{-1/3}y_1^{7/6})]^{6/7} - y_1 = & & \text{From Figure 10, } y_{cs} = & & \text{ft} \end{array}$					
	Otherwise, $\chi = 0.122 y_1 [q_2/(D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = $ From Figure 10, $y_{cs} = $ If					
PGRM: Pier	PIER SCOUR CALCULATIONS Correction factor for flow angle of attack (from Table 1), $K2 = 2$ Using pier width a on Figure 11, $\xi = 9$ Pier scour $y_{ps} = 6$, $y_{gs} = 6$					
PGRM: Abutment	ABUTMENT SCOUR CALCULATIONS Average flow depth blocked by: left abutment, $y_{aLT} = 0$ ft right abutment, $y_{aRT} = 5$ ft Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = 0$ and $\psi_{RT} = 5$ ft Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 0$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 0$ ft					

Route 259 St Stream Solit Rock	Creek	MRM	Dat	e	Ini	tials				
Bridge Structure No. 50277150 L	ocation From	T-90 F	= xi+ 406	1.5 1	1 0	5W				
Bridge Structure No. 50277150 Location From I 90 Exit 406, 1.5 N 0.5 W GPS coordinates: 143° 37.870′ taken from: USL abutment centerline of ft MRM end Datum of coordinates: WGS84 NAD27										
Drainage area = $\frac{476.78}{}$ sq. m				_						
The average bottom of the main channel was	55 ft below	top of guard	rail at a point	54	ft from le	ft abutment.				
Method used to determine flood flows:Free	a Anal	drainage area	ratio r	egional regr	ession equ	ations				
Method used to determine flood flows.	q. Anai. V	aramage area	Tatto	egionai regi	ession equ					
MISCELLANEOUS CONSIDERATIONS										
Flows		27600		$Q_{500} = 49100$						
Estimated flow passing through bridge		27600		34076						
Estimated road overflow & overtopping		0		15024						
Consideration	Yes	No	Possibly	Yes	No	Possibly				
Chance of overtopping		\prec				\times				
Chance of Pressure flow		\times		\times						
Armored appearance to channel		\times			X					
Lateral instability of channel			\times			\times				
Riprap at abutments? Yes No Marginal Evidence of past Scour? Pes No Don't know Debris Potential? High Med Low Does scour countermeasure(s) appear to have been designed? Riprap Yes No Don't know NA Spur Dike Yes No Don't know NA Other Yes No Don't know NA Bed Material Classification Based on Median Particle Size (D ₅₀) Material Silt/Clay Sand Gravel Cobbles Boulders Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250 Comments, Diagrams & orientation of digital photos										
	Q100 Q500									
Bridge flow evaluated		2 76 00			34076					
Flow depth at left abutment (yaLT), in feet		0			0					
Flow depth at right abutment (yaRT), in feet		4.75			5.05					
Contraction scour depth (ycs), in feet		21/			1,8					
Pier scour depth (yps), in feet		16,3			18,4					
Left abutment scour depth (yas), in feet										
Right abutment scour depth (yas), in feet										
1Flow angle of attack		10			10					