

OK RT

SCOUR ANALYSIS AND REPORTING FORM

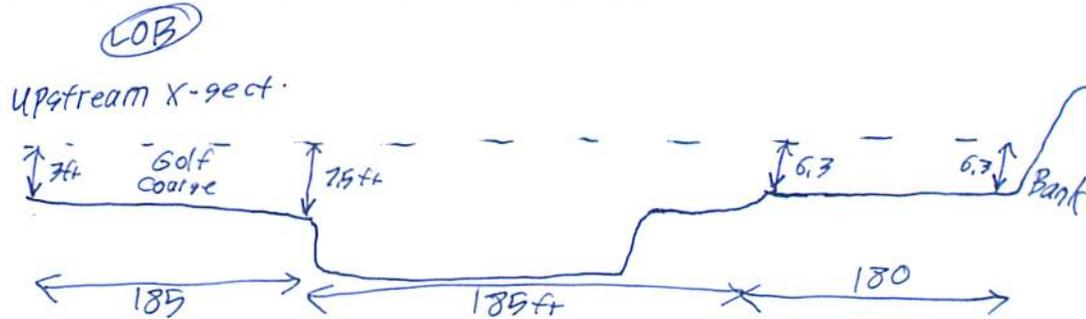
Bridge Structure No. 50286180 Date 9-19-10 Initials KAL Region (A B O D)
Site Location From I-90 Exit 406, 1.49 0.6E
Q100 = 27,900 by: drainage area ratio [checked] flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 27,900 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 218 ft Flow angle at bridge = 25 degrees Abut. Skew = 0 Effective Skew = 25 degrees
Width (W2) iteration = 200 204
Avg. flow depth at bridge, y2 iteration = 17.5 17.3
Corrected channel width at bridge Section = W2 times cos of flow angle = 184.89 ft\* q2 = Q2/W2 = 150.9 ft^2/s
Bridge Vel, V2 = 8.7 ft/s Final y2 = q2/V2 = 17.3 ft Delta h = 1.6 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 18.9 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 3.9 ft
Low Steel Elev. = 21.6 ft
n (Channel) = 0.073
n (LOB) = 0.025
n (ROB) = 0.045
Pier Width = 3 ft
Pier Length = 3 ft
# Piers for 100 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section W1 = 185 ft
Width of left overbank flow at approach, Wlob = 185 ft Average left overbank flow depth, ylob = 5.625 ft
Width of right overbank flow at approach, Wrob = 180 ft Average right overbank flow depth, yrob = 6.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 6.3 From Figure 9 W2 (effective) = 178.9 ft ycs = 7.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s
Critical approach velocity, Vc = 11.52 y1^(1/6) D50^(1/3) = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^(7/6))^3 = ft If D50 >= Dc50, zeta = 0.0
Otherwise, zeta = 0.122 y1 [q2 / (D50^(1/3) y1^(7/6))]^(6/7) - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), K2 = 1
Froude # at bridge = 0.37 Using pier width a on Figure 11, zeta = 10.7 Pier scour yps = 9.2 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 5.625 ft right abutment, yarT = 6.3 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 16.1 and psiRT = 17.3
Left abutment scour, yas = psiLT (K1/0.55) = 16.1 ft Right abutment scour yas = psiRT (K1/0.55) = 17.3 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

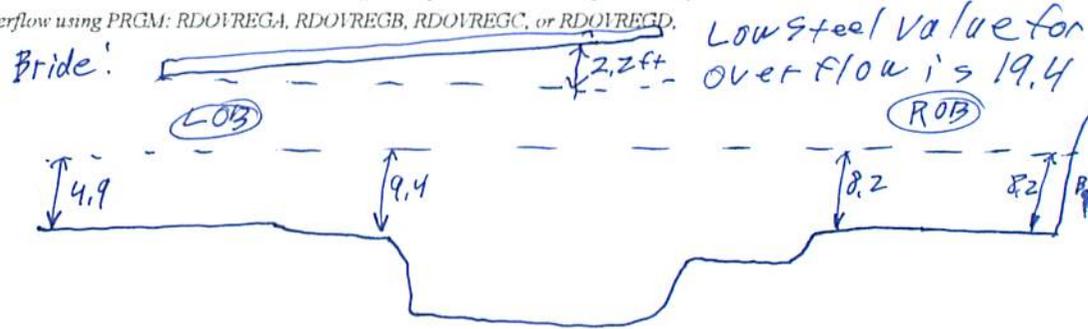
Bridge Structure No. 50286180 Date 9-19-10 Initials KAL Region (A B O D)       
 Site      Location From I-90 Exit 406, 1.45, 0.6E  
 $Q_{500} =$  49,600 by: drainage area ratio  flood freq. anal.      regional regression eq.       
 Bridge discharge ( $Q_2$ ) = 37,421 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 218 ft. Flow angle at bridge = 25° Abut. Skew = 0 Effective Skew = 25°  
 Width ( $W_2$ ) iteration = 218  
 Avg. flow depth at bridge,  $y_2$  iteration = 19.4  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 197.58 ft\*  $q_2 = Q_2/W_2 =$  189.4 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  9.8 ft/s Final  $y_2 = q_2/V_2 =$  19.4 ft  $\Delta h =$  2 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  21.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\theta) + a \cos(\theta)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 3.9 ft  
 Low Steel Elev. = 21.6 ft  
 $n$  (Channel) = 0.033  
 $n$  (LOB) = 0.025  
 $n$  (ROB) = 0.045  
 Pier Width = 3 ft  
 Pier Length = 3 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  185 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  185 ft Average left overbank flow depth,  $y_{lob} =$  7.525 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  180 ft Average right overbank flow depth,  $y_{rob} =$  8.2 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)  
 $x =$  7.02 From Figure 9  $W_2$  (effective) = 191.6 ft  $y_{cs} =$  7.8 ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$       ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$       ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$       ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{cs} = 0.0006 (q_2 / y_1^{7/6})^3 =$       ft If  $D_{50} >= D_{cs}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$       From Figure 10,  $y_{cs} =$       ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.39 Using pier width  $a$  on Figure 11,  $\xi =$  10.7 Pier scour  $y_{ps} =$  9.3 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{alT} =$  7.525 ft right abutment,  $y_{arT} =$  8.2 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{alT}$  and  $y_{arT}$  on figure 12,  $\psi_{LT} =$  19.4 and  $\psi_{RT} =$  19.9  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  19.4 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  19.9 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Abutment

Route old 9264 Stream Split Rock Creek MRM Date 9-19-10 Initials RAZ  
 Bridge Structure No. 50286180 Location From I-90 Exit 406, 1.49, 0.6 E  
 GPS coordinates: N43° 35.238' taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W96° 33.662' Datum of coordinates: WGS84 \_\_\_\_\_ NAD27 \_\_\_\_\_  
 Drainage area = 486.32 sq. mi.

The average bottom of the main channel was 29.1 ft below top of guardrail at a point 51 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio \_\_\_\_\_ regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>27900</u>			Q <sub>500</sub> = <u>49600</u>		
Estimated flow passing through bridge	<u>27900</u>			<u>37,421</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>12,179</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal \_\_\_\_\_  
 Evidence of past Scour? \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know  
 Debris Potential? \_\_\_\_\_ High  Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know \_\_\_\_\_ NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

**Comments, Diagrams & orientation of digital photos**

- 1- Bridge Deck
- 2- Looking upstream
- 3- Looking downstream
- 4- Left overbank
- 5- Right overbank
- 6- Left Abutment
- 7- Right Abutment
- 8- Piers
- 9-

**Summary of Results**

	Q100	Q500
Bridge flow evaluated	<u>27,900</u>	<u>37,421</u>
Flow depth at left abutment (yaLT), in feet	<u>5.625</u>	<u>7.525</u>
Flow depth at right abutment (yaRT), in feet	<u>6.3</u>	<u>8.2</u>
Contraction scour depth (yca), in feet	<u>7.1</u>	<u>7.8</u>
Pier scour depth (yps), in feet	<u>9.2</u>	<u>9.3</u>
Left abutment scour depth (yas), in feet	<u>16.1</u>	<u>19.4</u>
Right abutment scour depth (yas), in feet	<u>17.3</u>	<u>19.9</u>
Flow angle of attack	<u>25</u>	<u>25</u>

See Comments/Diagram for justification where required