

# Split Rock Creek

## SCOUR ANALYSIS AND REPORTING FORM

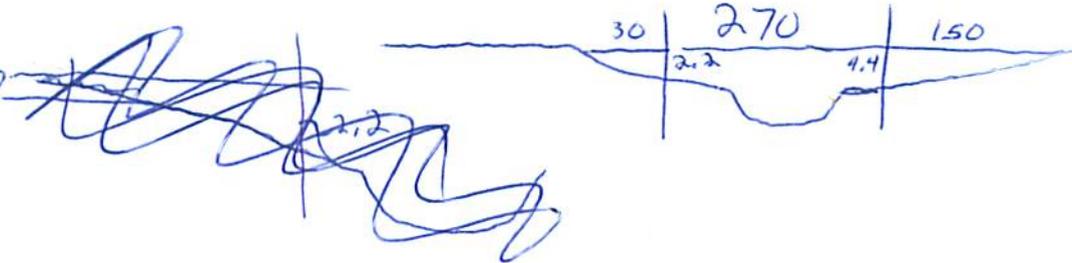
Bridge Structure No. 50290129 Date 10/9/11 Initials Ch Region (A B C D) C  
 Site \_\_\_\_\_ Location 3 mi. N + 1 mi. E of Carson on 257 St  
 $Q_{100} = 16700$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 16700 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 262 ft. Flow angle at bridge = 25 ° Abut. Skew = 30 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 262 244 247  
 Avg. flow depth at bridge,  $y_2$  iteration = 11.3 11.7 11.6  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 246.06 ft\*  $q_2 = Q_2/W_2 = 67.9$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 5.8$  ft/s Final  $y_2 = q_2/V_2 = 11.6$  ft  $\Delta h = 0.7$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 12.3$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2  
 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 14.8 ft  
 $n$  (Channel) = ~~0.04~~ 0.050  
 $n$  (LOB) = 0.040  
 $n$  (ROB) = 0.040  
 Pier Width = 3.0 ft  
 Pier Length = 3.0 ft  
 # Piers for 100 yr = 3 ft



### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 270$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 30$  ft Average left overbank flow depth,  $y_{lob} = 1.1$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 150$  ft Average right overbank flow depth,  $y_{rob} = 2.2$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} = 0.4$  ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) = 3.02$  ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} = 12.5$  ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 = 0.029$  ft

If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = 0.0$

From Figure 10,  $y_{cs} = 0.0$  ft

### PIER SCOUR CALCULATIONS

L/a ratio = 1.0

Correction factor for flow angle of attack (from Table 1),  $K_2 = 1.0$

Froude # at bridge = ~~0.29~~  
0.30

Using pier width  $a$  on Figure 11,  $\xi = 10.7$  Pier scour  $y_{ps} = 8.9$  ft

### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{alT} = 1.1$  ft right abutment,  $y_{arT} = 2.2$  ft

Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{alT}$  and  $y_{arT}$  on figure 12,  $\psi_{LT} = 4.7$  and  $\psi_{RT} = 9.0$

Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = 4.7$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = 9.0$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

*Handwritten calculations:*  
 $14.8 + 2.2 = 17.0$   
 $17.0 - 0.8 = 16.2$

**SCOUR ANALYSIS AND REPORTING FORM**

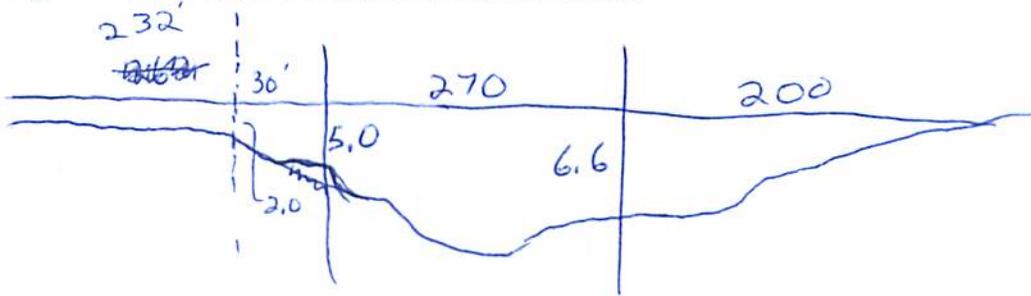
Bridge Structure No. 50290129 Date 10/9/11 Initials CL Region (A B C D) D  
 Site \_\_\_\_\_ Location 3 mi. N + 1 mi E of Carson on 257 St  
 $Q_{500} =$  26000 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 26,000 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 262 ft. Flow angle at bridge = 25 ° Abut. Skew = 30 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 262  
 Avg. flow depth at bridge,  $y_2$  iteration = 14.1 → Vert Wall  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 261 ft\*  $q_2 = Q_2/W_2 =$  99.6 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  7.1 ft/s Final  $y_2 = q_2/V_2 =$  14.1 ft  $\Delta h =$  1.0 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  15.1 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2  
 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 14.9 ft  
 $n$  (Channel) = 0.050  
 $n$  (LOB) = 0.040  
 $n$  (ROB) = 0.040  
 Pier Width = 3.0 ft  
 Pier Length = 3.0 ft  
 # Piers for 500 yr = 3 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  270 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  262 ft Average left overbank flow depth,  $y_{lob} =$  5.0 ft <sup>2.9</sup>  
 Width of right overbank flow at approach,  $W_{rob} =$  200 ft Average right overbank flow depth,  $y_{rob} =$  3.3 ft  
732

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $\chi =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  0.4 ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  2.35 ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  12.94 ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  0.044 ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  0.0 From Figure 10,  $y_{cs} =$  0.0 ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.33 Using pier width  $a$  on Figure 11,  $\xi =$  10.7 Pier scour  $y_{ps} =$  9.1 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  2.9 ft right abutment,  $y_{aRT} =$  3.3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  11.3 and  $\psi_{RT} =$  12.0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  11.3 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  12.0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"  
PGRM: Contract  
PGRM: CWCNEW  
PGRM: Pier  
PGRM: Abutment

12.3  
12.0  
0.5  
2.2

Route 257 St Stream Split Rock CK MRM \_\_\_\_\_ Date 10/19/11 Initials CM  
 Bridge Structure No. 50290129 Location 3mi N + 1mi E of Corson on 257 St  
 GPS coordinates: N 43° 39' 39.1" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 96° 33' 03.9" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 377.05 sq. mi.  
 The average bottom of the main channel was 22.0 ft below top of guardrail at a point 55 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>16700</u>			Q <sub>500</sub> = <u>26000</u>		
Estimated flow passing through bridge	<u>16700</u>			<u>26000</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal \_\_\_\_\_  
 Evidence of past Scour? \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_  
 Debris Potential? \_\_\_\_\_ High  Med \_\_\_\_\_ Low \_\_\_\_\_

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_\_\_ Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles  Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

10/4/11  
 2 1790  
 5 4320  
 10 6590  
 25 10100  
 50 13200  
 100 16700  
 500 26,000  
 2049 - ~~1000~~ ID  
 2050 - ~~45~~ RB  
 2051 - ~~45~~ RB  
 2052 - ~~45~~ LB  
 53 - L. Abut  
 56 - ~~45~~ Face  
 57 - R. Abut

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>16,700</u>	<u>26,000</u>
Flow depth at left abutment (yaLT), in feet	<u>1.1</u>	<u>2.9</u>
Flow depth at right abutment (yaRT), in feet	<u>2.2</u>	<u>3.3</u>
Contraction scour depth (yca), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (yps), in feet	<u>3.9</u>	<u>9.1</u>
Left abutment scour depth (yas), in feet	<u>4.7</u>	<u>11.3</u>
Right abutment scour depth (yas), in feet	<u>9.0</u>	<u>12.0</u>
Flow angle of attack	<u>5°</u>	<u>5°</u>

See Comments/Diagram for justification where required