

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 50313088 Date 10-8-10 Initials RRL Region (A B C D)

Site Location N end Garretson

Q100 = 24000 by: drainage area ratio [checked] flood freq. anal. regional regression eq.

Bridge discharge (Q2) = 24000 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 243 ft. Flow angle at bridge = 17 degrees Abut. Skew = 0 degrees Effective Skew = 17 degrees

Width (W2) iteration = 156 140 142

Avg. flow depth at bridge, y2 iteration = 17.9 18.9 18.7

Corrected channel width at bridge Section = W2 times cos of flow angle = 135.8 ft\* q2 = Q2/W2 = 176.7 ft^2/s

Bridge Vel, V2 = 9.4 ft/s Final y2 = q2/V2 = 18.7 ft Delta h = 1.8 ft

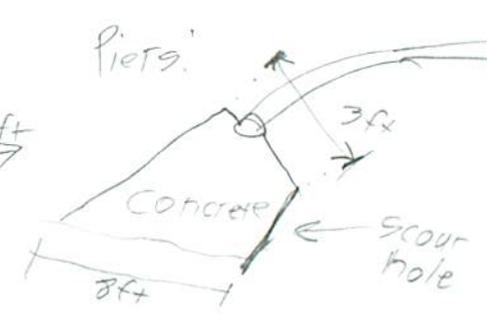
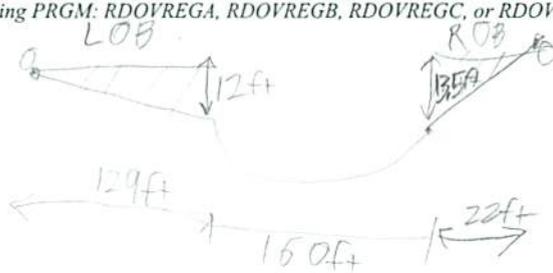
Average main channel depth at approach section, y1 = Delta h + y2 = 20.6 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2

Effective pier width = L sin(q) + a cos(q)

If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

- Water Surface Elev. = 2.3 ft
Low Steel Elev. = 29.6 ft
n (Channel) = 0.03
n (LOB) = 0.035
n (ROB) = 0.04
Pier Width = 37 ft
Pier Length = 3 ft
# Piers for 100 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section W1 = 160 ft

Width of left overbank flow at approach, Wlob = 129 ft

Average left overbank flow depth, ylob = 6 ft

Width of right overbank flow at approach, Wrob = 22 ft

Average right overbank flow depth, yrob = 6.75 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 7.45 From Figure 9 W2 (effective) = 129.8 ft ycs = 8.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = Average approach velocity, V1 = Q100/(y1W1) = ft/s

Critical approach velocity, Vc = 11.52y1^1/6 D50^1/3 = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006(q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 3.1 CW Correction factor for flow angle of attack (from Table 1), K2 = 1
Froude # at bridge = 0.38 Using pier width a on Figure 11, xi = 10.7 Pier scour yps = 9.3 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 6 ft right abutment, yarT = 6.75 ft

Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for yalT and yarT on figure 12, psiLT = 16.8 and psiRT = 18.1

Left abutment scour, yas = psiLT(K1/0.55) = 16.8 ft Right abutment scour yas = psiRT(K1/0.55) = 18.1 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 50313088 Date 10-8-10 Initials RRL Region (A B C D)

Site \_\_\_\_\_ Location N end Garretson

$Q_{500} =$ 42700 $$ by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_

Bridge discharge ( $Q_2$ ) = 42700 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 243 ft. Flow angle at bridge = 17 ° Abut. Skew = 0 ° Effective Skew = 17 °

Width ( $W_2$ ) iteration = 156 170 158 158

Avg. flow depth at bridge,  $y_2$  iteration = 23.8 22.8 23.7 23.7

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 151.1 ft\*  $q_2 = Q_2/W_2 =$ 282.6 ft<sup>2</sup>/s

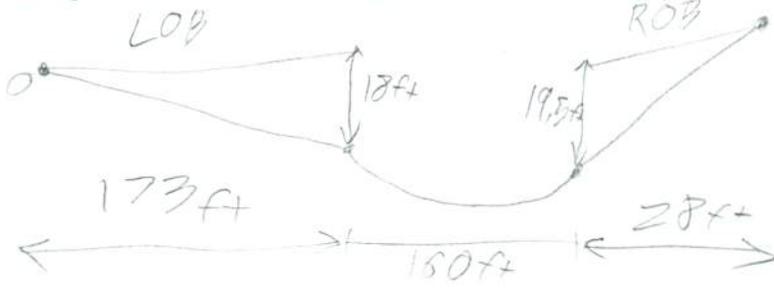
Bridge Vel,  $V_2 =$ 11.9 ft/s Final  $y_2 = q_2/V_2 =$ 23.7 ft  $\Delta h =$ 2.9 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$ 26.6 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 2.3 ft  
 Low Steel Elev. = 29.6 ft  
 $n$  (Channel) = 0.03  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.04  
 Pier Width = 3 ft  
 Pier Length = 3 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$ 160 ft

Width of left overbank flow at approach,  $W_{lob} =$ 173 ft Average left overbank flow depth,  $y_{lob} =$ 9 ft

Width of right overbank flow at approach,  $W_{rob} =$ 28 ft Average right overbank flow depth,  $y_{rob} =$ 9.75 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ 7.92 From Figure 9  $W_2$  (effective) = 145.1 ft  $y_{cs} =$ 8.8 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$ \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$ \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$ \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ \_\_\_\_\_ From Figure 10,  $y_{cs} =$ \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 31 CV  
 Froude # at bridge = 0.43

Correction factor for flow angle of attack (from Table 1),  $K_2 =$ 1  
 Using pier width  $a$  on Figure 11,  $\xi =$ 10.7 Pier scour  $y_{ps} =$ 9.4 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$ 9 ft right abutment,  $y_{aRT} =$ 9.75 ft

Shape coefficient  $K_i = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$ 20.6 and  $\psi_{RT} =$ 21.1

Left abutment scour,  $y_{as} = \psi_{LT}(K_i/0.55) =$ 20.6 ft Right abutment scour  $y_{as} = \psi_{RT}(K_i/0.55) =$ 21.1 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 5th St Stream Split Rock Creek MRM Date 10-7-10 Initials RRL

Bridge Structure No. 50313088 Location N end Garretson

GPS coordinates: N 47° 43.179' taken from: USL abutment  centerline of  MRM end   
W 096° 30.249' Datum of coordinates: WGS84  NAD27

Drainage area = 366.07 sq. mi.

The average bottom of the main channel was 71.8 ft below top of guardrail at a point 78 ft from left abutment.

Method used to determine flood flows:  Freq. Anal.  drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>24000</u>			Q <sub>500</sub> = <u>42700</u>		
Estimated flow passing through bridge	<u>24000</u>			<u>42700</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments?  Yes  No  Marginal  
 Evidence of past Scour?  Yes  No  Don't know  
 Debris Potential?  High  Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes  No  Don't know  NA  
 Spur Dike  Yes  No  Don't know  NA  
 Other  Yes  No  Don't know  NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand  Gravel  Cobbles  Boulders   
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

**Comments, Diagrams & orientation of digital photos**

1- Upstream Obstruction  
 2- Bridge Deck  
 3- Looking Upstream  
 4- Looking Downstream  
 5- Left Overbank  
 6- Right Overbank  
 7- Left Abutment  
 8- Right Abutment  
 9- Pier 2  
 Notes: Upstream Dam structure, Piers built into bedrock, non-uniform arch design.

**Summary of Results**

	Q100	Q500
Bridge flow evaluated	<u>24000</u>	<u>42700</u>
Flow depth at left abutment (yaLT), in feet	<u>6</u>	<u>9</u>
Flow depth at right abutment (yaRT), in feet	<u>6.75</u>	<u>9.75</u>
Contraction scour depth (yca), in feet	<u>8.3</u>	<u>8.8</u>
Pier scour depth (ypp), in feet	<u>9.3</u>	<u>9.4</u>
Left abutment scour depth (yas), in feet	<u>16.8</u>	<u>20.6</u>
Right abutment scour depth (yas), in feet	<u>18.1</u>	<u>21.1</u>
Flow angle of attack	<u>17</u>	<u>17</u>

See Comments/Diagram for justification where required