

OK RJ

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 50330183 Date 10-9-10 Initials RRL Region (A B C D) CD  
 Site 06048 2745 Location 1W 0.25 from SD/MN line @ Valley Springs  
 $Q_{100} =$  5770 by: drainage area ratio \_\_\_\_\_ flood freq. anal.  regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 5770 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

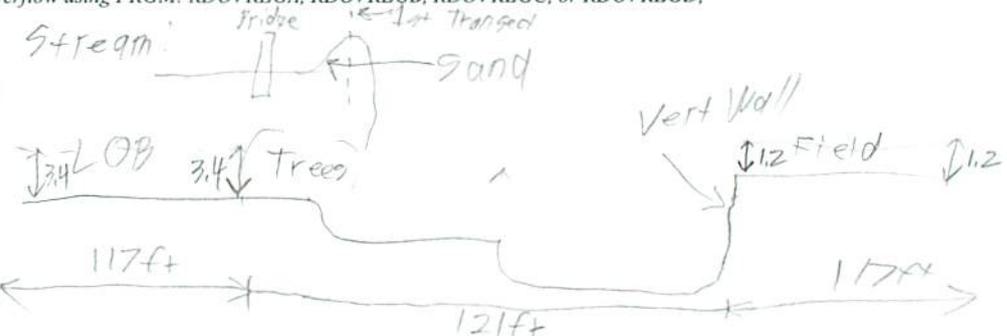
#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 117 ft. Flow angle at bridge = 0° Abut. Skew = 0° Effective Skew = 0°  
 Width ( $W_2$ ) iteration = 100 103  
 Avg. flow depth at bridge,  $y_2$  iteration = 10.7 10.6  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 103 ft\*  $q_2 = Q_2/W_2 =$  56 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  5.3 ft/s Final  $y_2 = q_2/V_2 =$  10.6 ft  $\Delta h =$  0.6 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  11.1 ft

\* - Low Flow is winding. High Flow is straight.

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 0 ft  
 Low Steel Elev. = 15.6 ft  
 $n$  (Channel) = 0.035  
 $n$  (LOB) = 0.05  
 $n$  (ROB) = 0.045  
 Pier Width = 3 ft  
 Pier Length = 3 ft  
 # Piers for 100 yr = 2 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  121 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  117 ft Average left overbank flow depth,  $y_{lob} =$  3.4 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  117 ft Average right overbank flow depth,  $y_{rob} =$  1.2 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  4.31 From Figure 9  $W_2$  (effective) = 97 ft  $y_{cs} =$  5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.29 Using pier width  $a$  on Figure 11,  $\xi =$  10.7 Pier scour  $y_{ps} =$  8.9 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.4 ft right abutment,  $y_{aRT} =$  1.2 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  12.2 and  $\psi_{RT} =$  5.1  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  12.2 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  5.1 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

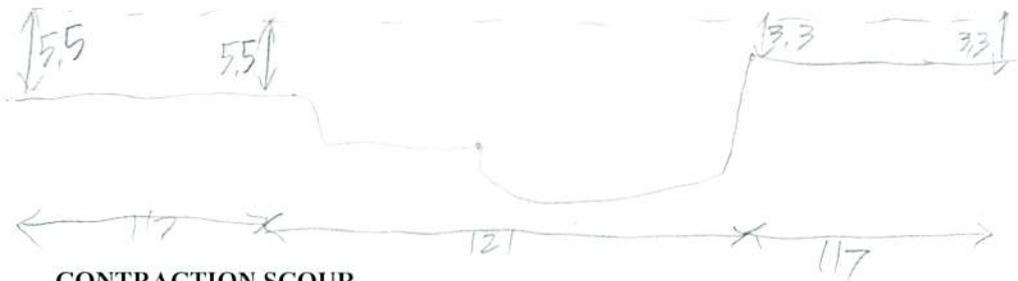
Bridge Structure No. 50330183 Date 10-9-10 Initials RRL Region (A B C D) D  
 Site 06482745 Location 1W 0.25 from SD/MN line @ Valley Springs  
 $Q_{500} =$  9110 by: drainage area ratio \_\_\_\_\_ flood freq. anal.  regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 9110 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 117 ft. Flow angle at bridge = 0° Abut. Skew = 0° Effective Skew = 0° *Note: Low Flow Winding, High Flow  $\alpha > 0$*   
 Width ( $W_2$ ) iteration = 117  
 Avg. flow depth at bridge,  $y_2$  iteration = 12.4  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 117 ft\*  $q_2 = Q_2/W_2 =$  77.9 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  6.3 ft/s Final  $y_2 = q_2/V_2 =$  12.4 ft  $\Delta h =$  0.8 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  13.2 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0 ft  
 Low Steel Elev. = 15.6 ft  
 $n$  (Channel) = 0.035  
 $n$  (LOB) = 0.09  
 $n$  (ROB) = 0.045  
 Pier Width = 3 ft  
 Pier Length = 3 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  121 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  117 ft Average left overbank flow depth,  $y_{lob} =$  5.5 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  117 ft Average right overbank flow depth,  $y_{rob} =$  3.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  4.53 From Figure 9  $W_2$  (effective) = 111 ft  $y_{cs} =$  5.2 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.32 Using pier width  $a$  on Figure 11,  $\xi =$  10.7 Pier scour  $y_{ps} =$  9 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.5 ft right abutment,  $y_{aRT} =$  3.3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  15.9 and  $\psi_{RT} =$  12  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  15.9 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  12 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route 487 Ave Stream Beaver Creek MRM \_\_\_\_\_ Date 10-9-10 Initials RRL  
 Bridge Structure No. 50330183 Location 1W, 0.2S from SD/MN line @ Valley Springs  
 GPS coordinates: N 43° 35.165' taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 096° 28.335' Datum of coordinates: WGS84 \_\_\_\_\_ NAD27 \_\_\_\_\_

Drainage area = 104 sq. mi.  
 The average bottom of the main channel was 19.6 ft below top of guardrail at a point 38 ft from left abutment.  
 Method used to determine flood flows:  Freq. Anal. \_\_\_\_\_ drainage area ratio \_\_\_\_\_ regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>5770</u>			Q <sub>500</sub> = <u>9110</u>		
Estimated flow passing through bridge	<u>5770</u>			<u>9110</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>

Riprap at abutments? \_\_\_\_\_ Yes \_\_\_\_\_ No  Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  
 Debris Potential?  High \_\_\_\_\_ Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
1 - Bridge Deck 6 - Left Abutment  
2 - Looking Upstream 7 - Right Abutment  
3 - Looking Downstream  
4 - Left Overbank  
5 - Right Overbank

**Summary of Results**

	Q100	Q500
Bridge flow evaluated	<u>5770</u>	<u>9110</u>
Flow depth at left abutment (yaLT), in feet	<u>3.4</u>	<u>5.5</u>
Flow depth at right abutment (yaRT), in feet	<u>1.2</u>	<u>3.3</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>5</u>	<u>5.2</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>8.9</u>	<u>9</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>12.2</u>	<u>15.9</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>5.1</u>	<u>12</u>
Flow angle of attack	<u>0</u>	<u>0</u>

See Comments/Diagram for justification where required