

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 50335090 Date 6/24/12 Initials Pat Region (A B C D) D  
 Site \_\_\_\_\_ Location 1.5 mi E of Garretson on 253 St  
 $Q_{100} = Q_5$  941 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 941 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 56 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 49.5 ft\*  $q_2 = Q_2/W_2 =$  19.4 ft<sup>2</sup>/s

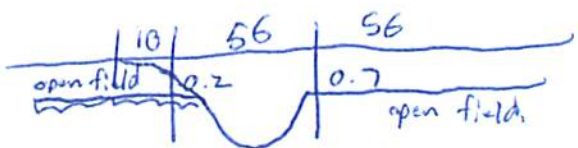
Bridge Vel,  $V_2 =$  3.1 ft/s Final  $y_2 = q_2/V_2 =$  6.2 ft  $\Delta h =$  0.2 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  6.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = 671.0 ft  
 Low Steel Elev. = 665 ft  
 n (Channel) = 0.030  
 n (LOB) = 0.030  
 n (ROB) = 0.030  
 Pier Width = 2.85 ft  
 Pier Length = 78 ft  
 # Piers for 100 yr = 3 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  56 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  65 ft Average left overbank flow depth,  $y_{lob} =$  0.7 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  10 ft Average right overbank flow depth,  $y_{rob} =$  0.2 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  2.8 From Figure 9  $W_2$  (effective) = 40 ft  $y_{cs} =$  3.4 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

PRGM: Contract

PRGM: CWCNEW

#### PIER SCOUR CALCULATIONS

L/a ratio = 27.37 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  3.5  
 Froude # at bridge = 0.22 Using pier width a on Figure 11,  $\xi =$  10.4 Pier scour  $y_{ps} =$  28.9 ft

PRGM: Pier

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0.7 ft right abutment,  $y_{aRT} =$  0.2 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  3.1 and  $\psi_{RT} =$  1  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  5.6 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  1.7 ft

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

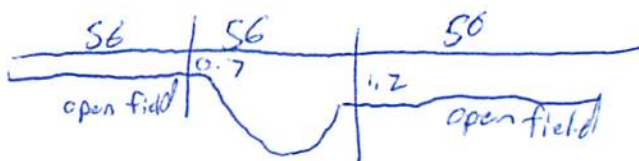
Bridge Structure No. 50335090 Date 6/25/12 Initials kal Region (A B C D) D  
 Site \_\_\_\_\_ Location 1.5 mi E of Garretson on 253 St  
 $Q_{500} = Q_p$  1430 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1142 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 56 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 48.5 ft\*  $q_2 = Q_2/W_2 =$  23.5 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  3.4 ft/s Final  $y_2 = q_2/V_2 =$  6.9 ft  $\Delta h =$  0.2 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.1 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0+1.0 ft  
 Low Steel Elev. = 6.85 ft  
 n (Channel) = 0.030  
 n (LOB) = 0.030  
 n (ROB) = 0.030  
 Pier Width = 28.5 ft  
 Pier Length = 78 ft  
 # Piers for 500 yr = 3



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  56 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  56 ft Average left overbank flow depth,  $y_{lob} =$  1.2 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  56 ft Average right overbank flow depth,  $y_{rob} =$  0.7 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)  
 $x =$  3.58 From Figure 9  $W_2$  (effective) = 40 ft  $y_{cs} =$  4.2 ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 27.37 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  3.5  
 Froude # at bridge = 0.23 Using pier width a on Figure 11,  $\xi =$  10.4 Pier scour  $y_{ps} =$  29 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  1.2 ft right abutment,  $y_{aRT} =$  0.7 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  5.1 and  $\psi_{RT} =$  3.1  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  9.2 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  5.6 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

43.71617  
96.46089

96.27.39.165  
43.43.542

Route 253 St Stream \_\_\_\_\_ MRM \_\_\_\_\_ Date 6/25/12 Initials RAF  
 Bridge Structure No. 50335090 Location 1.5 mi E of Garretson on 253 St  
 GPS coordinates: N 43° 43' 53" W 96° 27' 40.3" taken from: USL abutment  centerline of  MRM end \_\_\_\_\_  
 Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 17.29 sq. mi.  
 The average bottom of the main channel was 8.9 ft below top of guardrail at a point 15 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>500</sub> <sup>5</sup> = <u>941</u>			Q <sub>500</sub> <sup>10</sup> = <u>1430</u>		
Estimated flow passing through bridge	<u>941</u>			<u>1142</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>288</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

8/25 6/16  
 2 388  
 5 941  
 10 1430  
 25 2170  
 50 2800  
 100 3480  
 500 5230

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour? \_\_\_ Yes \_\_\_ No  Don't know *very minor if any*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_\_\_ \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1). left ab *of main channel*  
 2). main channel  
 3). right ab.  
 4). left abutment  
 5). right abutment

Summary of Results

	Q <sub>100</sub> <sup>5</sup>	Q <sub>500</sub> <sup>10</sup>
Bridge flow evaluated	<u>941</u>	<u>1142</u>
Flow depth at left abutment (yaLT), in feet	<u>0.7</u>	<u>1.2</u>
Flow depth at right abutment (yaRT), in feet	<u>0.2</u>	<u>0.7</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<del>3.5</del> <u>3.4</u>	<u>4.2</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>28.9</u>	<u>29</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<del>5.6</del> <u>5.6</u>	<del>9.2</del> <u>9.2</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<del>1.7</del> <u>1.7</u>	<del>5.6</del> <u>5.6</u>
Flow angle of attack	<u>30</u>	<u>30</u>

See Comments/Diagram for justification where required