

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 51129200 Date 7/26/12 Initials RAJ Region (A B C D) D

Site \_\_\_\_\_ Location 1 mi E of Trent on 240 St

Q<sub>100</sub> = Q<sub>10</sub> 1310 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X

Bridge discharge (Q<sub>2</sub>) = 1310 (should be Q<sub>100</sub> unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 41 ft. Flow angle at bridge = 20 ° Abut. Skew = 0 ° Effective Skew = 20 °

Width (W<sub>2</sub>) iteration = \_\_\_\_\_

Avg. flow depth at bridge, y<sub>2</sub> iteration = \_\_\_\_\_

Corrected channel width at bridge Section = W<sub>2</sub> times cos of flow angle = 38.53 ft\* q<sub>2</sub> = Q<sub>2</sub>/W<sub>2</sub> = 34 ft<sup>2</sup>/s

Bridge Vel, V<sub>2</sub> = 4.1 ft/s Final y<sub>2</sub> = q<sub>2</sub>/V<sub>2</sub> = 8.2 ft Δh = 0.3 ft

Average main channel depth at approach section, y<sub>1</sub> = Δh + y<sub>2</sub> = 8.6 ft

\* NOTE: repeat above calculations until y<sub>2</sub> changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)

If y<sub>2</sub> is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

10  
11.4  
0.6  
2.0  
2.0  
2.2

Water Surface Elev. = 2.0 ft  
Low Steel Elev. = 8.6 ft  
n (Channel) = 0.045  
n (LOB) = 0.030  
n (ROB) = 0.035 0.010  
Pier Width = 0 ft  
Pier Length = 0 ft  
# Piers for 100 yr = 0 ft



CONTRACTION SCOUR

Width of main channel at approach section W<sub>1</sub> = 41 ft

Width of left overbank flow at approach, W<sub>lob</sub> = 0 ft Average left overbank flow depth, y<sub>lob</sub> = 0 ft

Width of right overbank flow at approach, W<sub>rob</sub> = 41 ft Average right overbank flow depth, y<sub>rob</sub> = 2.2 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 1.61 From Figure 9 W<sub>2</sub> (effective) = 38.5 ft y<sub>cs</sub> = 2.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D<sub>50</sub> = \_\_\_\_\_ ft Average approach velocity, V<sub>1</sub> = Q<sub>100</sub>/(y<sub>1</sub>W<sub>1</sub>) = \_\_\_\_\_ ft/s

Critical approach velocity, V<sub>c</sub> = 11.17y<sub>1</sub><sup>1/6</sup>D<sub>50</sub><sup>1/3</sup> = \_\_\_\_\_ ft/s

If V<sub>1</sub> < V<sub>c</sub> and D<sub>50</sub> >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

D<sub>c50</sub> = 0.0006(q<sub>2</sub>/y<sub>1</sub><sup>7/6</sup>)<sup>3</sup> = \_\_\_\_\_ ft If D<sub>50</sub> >= D<sub>c50</sub>, χ = 0.0

Otherwise, χ = 0.122y<sub>1</sub>[q<sub>2</sub>/(D<sub>50</sub><sup>1/3</sup>y<sub>1</sub><sup>7/6</sup>)]<sup>6/7</sup> - y<sub>1</sub> = \_\_\_\_\_ From Figure 10, y<sub>cs</sub> = \_\_\_\_\_ ft

PIER SCOUR CALCULATIONS

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1), K<sub>2</sub> = \_\_\_\_\_

Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11, ξ = \_\_\_\_\_ Pier scour y<sub>ps</sub> = \_\_\_\_\_ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, y<sub>aLT</sub> = 0 ft right abutment, y<sub>aRT</sub> = 2.2 ft

Shape coefficient K<sub>1</sub> = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for y<sub>aLT</sub> and y<sub>aRT</sub> on figure 12, ψ<sub>LT</sub> = 0 and ψ<sub>RT</sub> = 9

Left abutment scour, y<sub>as</sub> = ψ<sub>LT</sub>(K<sub>1</sub>/0.55) = 0 ft Right abutment scour y<sub>as</sub> = ψ<sub>RT</sub>(K<sub>1</sub>/0.55) = 16.4 ft

16.4

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 51129200 Date 7/26/12 Initials RAT Region (A B C D)

Site \_\_\_\_\_ Location 1 mi E of Trent on 240 St

$Q_{500} = Q_{25}$  7020 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X

Bridge discharge ( $Q_2$ ) = 1431 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 41 ft. Flow angle at bridge = 20 ° Abut. Skew = 0 ° Effective Skew = 20 °

Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 38.53 ft\*  $q_2 = Q_2/W_2 =$  37.1 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  4.3 ft/s Final  $y_2 = q_2/V_2 =$  8.6 ft  $\Delta h =$  0.4 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 2.0 ft  
 Low Steel Elev. = 6.6 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = ~~0.030~~ 0.040  
 Pier Width = 0 ft  
 Pier Length = 0 ft  
 # Piers for 500 yr = 0 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  41 ft

Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft

Width of right overbank flow at approach,  $W_{rob} =$  41 ft Average right overbank flow depth,  $y_{rob} =$  ~~0~~ 2.6 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  1.94 From Figure 9  $W_2$  (effective) = 38.5 ft  $y_{cs} =$  2.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_

Froude # at bridge = \_\_\_\_\_ Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  2.6 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  10.6

Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  19.3 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

43.906  
96.62783

43 54 21.11  
96 37 40.188

Project A

Route 240 St Stream Brookfield Ck MRM \_\_\_\_\_ Date 7/24/12 Initials RAT  
 Bridge Structure No. 51129200 Location 1 mi E of Trent on 240 St  
 GPS coordinates: N 43° 54' 21.71" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 96° 37' 40.01" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 22.6 sq. mi.  
 The average bottom of the main channel was 14.1 ft below top of guardrail at a point 30 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

6/29  
8/25

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>Q<sub>100</sub></u> 1310			Q <sub>500</sub> = <u>Q<sub>25</sub></u> 2020		
Estimated flow passing through bridge	1310			1431		
Estimated road overflow & overtopping	0			589		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow			<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

2 342  
5 854  
10 1310  
25 2020  
50 2640  
100 3300  
500 5030

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal *- corr husky on abutment areas, exposed outside abutment.*  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *some abutment. Underwater.*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Notes overbank profile taken 7ft from left abutment

Comments, Diagrams & orientation of digital photos  
 1) left CP  
 2) main channel  
 3) right CP  
 4) right abutment  
 5) left abutment  
 6) main channel

Summary of Results

	Q <sub>100</sub> Q <sub>10</sub>	Q <sub>500</sub> Q <sub>25</sub>
Bridge flow evaluated	1310	1431
Flow depth at left abutment (yaLT), in feet	0	0
Flow depth at right abutment (yaRT), in feet	2.2	2.6
Contraction scour depth (y <sub>cs</sub> ), in feet	2.1	2.5
Pier scour depth (y <sub>ps</sub> ), in feet	N/A	N/A
Left abutment scour depth (y <sub>as</sub> ), in feet	0	0
Right abutment scour depth (y <sub>as</sub> ), in feet	18.4	19.3
Flow angle of attack	20	20

See Comments/Diagram for justification where required