

Dup OK-Rat

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 51177030 Date 10-11-12 Initials RFT Region (A B O D)  
 Site \_\_\_\_\_ Location 3.7 mi W of Ward on 223<sup>rd</sup> St  
 $Q_{100} = \underline{3890}$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 3890 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

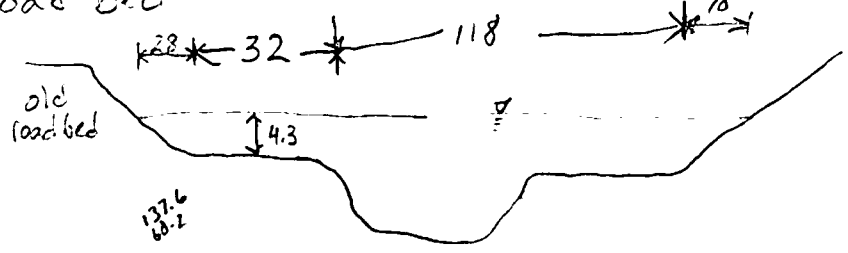
Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 118 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = 118 116  
 Avg. flow depth at bridge,  $y_2$  iteration = 8.2 8.2  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 114.24 ft\*  $q_2 = Q_2/W_2 = \underline{34.1}$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = \underline{4.1}$  ft/s Final  $y_2 = q_2/V_2 = \underline{8.2}$  ft  $\Delta h = \underline{0.3}$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{8.6}$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2  
 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

moved approach section further upstream to avoid old road bed

Water Surface Elev. = 1.0 ft  
 Low Steel Elev. = 14.4 ft  
 $n$  (Channel) = .035  
 $n$  (LOB) = .030  
 $n$  (ROB) = .030  
 Pier Width = 1.69 ft  
 Pier Length = 1.69 ft  
 # Piers for 100 yr = 4



CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = \underline{118}$  ft  
 Width of left overbank flow at approach,  $W_{lob} = \underline{60}$  ft Average left overbank flow depth,  $y_{lob} = \underline{3.3}$  ft  
 Width of right overbank flow at approach,  $W_{rob} = \underline{10}$  ft Average right overbank flow depth,  $y_{rob} = \underline{0.9}$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = \underline{2}$  From Figure 9  $W_2$  (effective) = 107.5 ft  $y_{cs} = \underline{2.5}$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} = \underline{\hspace{2cm}}$  ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) = \underline{\hspace{2cm}}$  ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} = \underline{\hspace{2cm}}$  ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 = \underline{\hspace{2cm}}$  ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\hspace{2cm}}$  From Figure 10,  $y_{cs} = \underline{\hspace{2cm}}$  ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1}$   
 Froude # at bridge = 0.25 Using pier width  $a$  on Figure 11,  $\xi = \underline{7}$  Pier scour  $y_{ps} = \underline{5.7}$  ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{3.3}$  ft right abutment,  $y_{aRT} = \underline{0.9}$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{12}$  and  $\psi_{RT} = \underline{39}$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = \underline{12}$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = \underline{3.9}$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PGRM: Contract  
 PGRM: CWCSNEW  
 PGRM: Pier  
 PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 51177030 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D) C

Site \_\_\_\_\_ Location \_\_\_\_\_

$Q_{500} =$  5990 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X

Bridge discharge ( $Q_2$ ) = 5990 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 118 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °

Width ( $W_2$ ) iteration = 118

Avg. flow depth at bridge,  $y_2$  iteration = 10.1

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 116.21 ft\*  $q_2 = Q_2/W_2 =$  51.5 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  5.1 ft/s Final  $y_2 = q_2/V_2 =$  10.1 ft  $\Delta h =$  0.5 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  10.7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2

Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

*assume overbank beyond roadbed is ineffective flow*

Water Surface Elev. = 1.0 ft

Low Steel Elev. = 14.4 ft

n (Channel) = .035

n (LOB) = .030

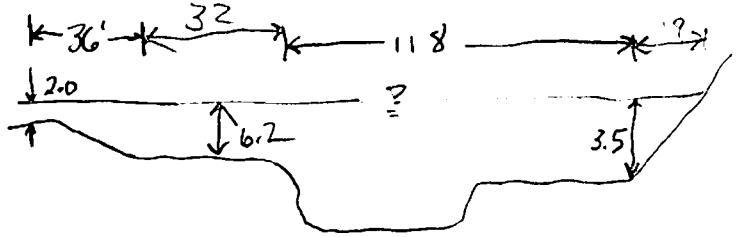
n (ROB) = .030

Pier Width = 1.69 ft

Pier Length = 1.69 ft

# Piers for 500 yr = 4 ft

*198.4  
147.6*



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  118 ft

Width of left overbank flow at approach,  $W_{lob} =$  68 ft

Average left overbank flow depth,  $y_{lob} =$  5.1 ft

Width of right overbank flow at approach,  $W_{rob} =$  19 ft

Average right overbank flow depth,  $y_{rob} =$  1.75 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)

$x =$  3.2 From Figure 9  $W_2$  (effective) = 109.5 ft  $y_{cs} =$  3.8 ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1

Froude # at bridge = 0.28

Using pier width a on Figure 11,  $\xi =$  7 Pier scour  $y_{ps} =$  5.8 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.1 ft right abutment,  $y_{aRT} =$  1.75 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  15.2 and  $\psi_{RT} =$  7.2

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  15.2 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  7.2 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pic

PGRM: Abutment

Route 223 St Stream Spring Creek MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 5117703 Location 3.7 mi W of Ward on 223<sup>rd</sup> St  
 GPS coordinates: N 44° 9.286' taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 96° 32.181' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 36.09 sq. mi.

The average bottom of the main channel was 18.3 ft below top of guardrail at a point 39 ft from left abutment.

Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>3890</u>			Q <sub>500</sub> = <u>5990</u>		
Estimated flow passing through bridge	<u>3890</u>			<u>5990</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know about, contraction, pier  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Str. no.  
 approach from bridge  
 LOB and old roadbed  
 ROB  
 Bridge from approach

there is a trashline of grass on a barb wire fence that indicates a flow between Q<sub>100</sub> and Q<sub>500</sub> has recently (this spring or summer) occurred at this site.

left abut. from ditch  
 rt. abut. from under bridge

old roadbed may help <sup>guide</sup> LOB flow toward bridge opening

**Summary of Results**

	Q <sub>100</sub>	Q <sub>500</sub>
Bridge flow evaluated	<u>3890</u>	<u>5990</u>
Flow depth at left abutment (yaLT), in feet	<u>3.3</u>	<u>5.1</u>
Flow depth at right abutment (yaRT), in feet	<u>0.9</u>	<u>1.75</u>
Contraction scour depth (yca), in feet	<u>2.5</u>	<u>3.8</u>
Pier scour depth (yp), in feet	<u>5.7</u>	<u>5.8</u>
Left abutment scour depth (yala), in feet	<u>12</u>	<u>15.2</u>
Right abutment scour depth (yara), in feet	<u>3.9</u>	<u>7.2</u>
Flow angle of attack	<u>10°</u>	<u>10°</u>

See Comments/Diagram for justification where required