

OK RJ

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 51200092 Date 8/18/10 Initials CW Region (A B C D)
Site 06480650 Location SE, 0.8 N from Flandreau
Q100 = 4870 by: drainage area flood frequency anal. regional regression eq.
Bridge discharge (Q2) = 4870 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 125 ft. Flow angle at bridge = 15 degrees Abut. Skew = 0 degrees Effective Skew = 15 degrees
Width (W2) iteration = 125
Avg. flow depth at bridge, y2 iteration = 9.0
Corrected channel width at bridge Section = W2 times cos of flow angle = 120.74 ft\* q2 = Q2/W2 = 40.3 ft2/s
Bridge Vel, V2 = 4.5 ft/s Final y2 = q2/V2 = 9 ft Delta h = 0.4 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 9.4 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = ft
Low Steel Elev. = 9.8 ft
n (Channel) = 0.037
n (LOB) = 0.037
n (ROB) = 0.070
Pier Width = 1.66 ft
Pier Length = 1.66 ft
# Piers for 100 yr = 3 ft

Vert. well @ 9.0

CONTRACTION SCOUR

Width of main channel at approach section W1 = 135 ft
Width of left overbank flow at approach, Wlob = 125 ft Average left overbank flow depth, ylob = 5.1 ft
Width of right overbank flow at approach, Wrob = 125 ft Average right overbank flow depth, yrob = 0.6 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 5.32 From Figure 9 W2 (effective) = 115.8 ft ycs = 6 ft
5.28

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s

Critical approach velocity, Vc = 11.52 y1 1/6 D50 1/3 = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006 (q2/y1 7/6) 3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122 y1 [q2 / (D50 1/3 y1 7/6)] 6/7 - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), K2 = 1.0
Froude # at bridge = 0.26 Using pier width a on Figure 11, xi = 6.9 Pier scour yps = 5.7 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalt = 5.1 ft right abutment, yarT = 0.6 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalt and yarT on figure 12, psLT = 15.2 and psRT = 2.7
Left abutment scour, yas = psLT (K1/0.55) = 22.1 ft Right abutment scour yas = psRT (K1/0.55) = 3.9 ft
15.2 2.7

0.80

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 51200092 Date 8/18/10 Initials CW Region (A B C D) D  
 Site 06480650 Location 5 E, 0.8 N from Flandreau  
 $Q_{500} =$  6740 by: drainage area  flood frequency anal.  regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 6030 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 125 ft. Flow angle at bridge = 15 ° Abut. Skew = 0 ° Effective Skew = 15 °  
 Width ( $W_2$ ) iteration = 125  
 Avg. flow depth at bridge,  $y_2$  iteration = 10.5  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 120.74 ft\*  $q_2 = Q_2/W_2 =$  49.9 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  5 ft/s Final  $y_2 = q_2/V_2 =$  10 ft  $\Delta h =$  0.5 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  10.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 9.8 ft  
 n (Channel) = 0.037  
 n (LOB) = 0.037  
 n (ROB) = 0.070  
 Pier Width = 1.66 ft  
 Pier Length = 1.66 ft  
 # Piers for 500 yr = 3 ft

$y_2 > LS \rightarrow$  RD overflow

**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  135 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  125 ft Average left overbank flow depth,  $y_{lob} =$  6.2 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  125 ft Average right overbank flow depth,  $y_{rob} =$  1.7 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  6.75 From Figure 9  $W_2$  (effective) = 115.8 ft  $y_{cs} =$  7.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.28 Using pier width a on Figure 11,  $\xi =$  6.9 Pier scour  $y_{ps} =$  5.7 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  6.2 ft right abutment,  $y_{aRT} =$  1.7 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  17.2 and  $\psi_{RT} =$  7  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  25 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  10.2 ft  
17.2 7.0

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 486<sup>th</sup> Ave Stream Flandreau Creek MRM \_\_\_\_\_ Date 8/18/10 Initials CW  
 Bridge Structure No. 51200092 Location SE, 0.8 N from Flandreau  
 GPS coordinates: N 44° 03' 45.0" taken from: USL abutment X centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 096° 29' 08.7" Datum of coordinates: WGS84 X NAD27 \_\_\_\_\_  
 Drainage area = 100.54 sq. mi.  
 The average bottom of the main channel was 13.3 ft below top of guardrail at a point 48 ft from left abutment.  
 Method used to determine flood flows:  Freq. Anal. \_\_\_\_\_ drainage area adjustment \_\_\_\_\_ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>4870</u>			Q <sub>500</sub> = <u>6740</u>		
Estimated flow passing through bridge	<u>4870</u>			<u>6030</u>		
Estimated road overflow & overtopping	<u>710</u>			<u>710</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<u>X</u>		<u>X</u>		
Chance of Pressure flow		<u>X</u>			<u>X</u>	
Armored appearance to channel		<u>X</u>			<u>X</u>	
Lateral instability of channel		<u>X</u>			<u>X</u>	

Riprap at abutments? \_\_\_\_\_ Yes \_\_\_\_\_ No X Marginal Mostly washed away  
 Evidence of past Scour? X Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med X Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap X Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know X NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know X NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)  
 Material Silt/Clay X Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1173- Bridge #  
 74- US from Bridge  
 75- US RB  
 76- US LB  
 77- ~~US~~ L. Abut  
 78- L. Abut  
 79- R. Abut  
 80- US face of bridge  
 81- US face of bridge

Summary of Results

	Q100		Q500	
Bridge flow evaluated	<u>4870</u>		<u>6030</u>	
Flow depth at left abutment (yaLT), in feet	<u>5.1</u>		<u>6.2</u>	
Flow depth at right abutment (yaRT), in feet	<u>0.6</u>		<u>1.7</u>	
Contraction scour depth (yca), in feet	<u>6.0</u>		<u>7.5</u>	
Pier scour depth (yps), in feet	<u>5.7</u>		<u>5.7</u>	
Left abutment scour depth (yas), in feet	<u>w-22.1</u>	<u>15.2</u>	<u>w-25</u>	<u>17.2</u>
Right abutment scour depth (yas), in feet	<u>w-3.9</u>	<u>2.7</u>	<u>w-10.2</u>	<u>7.0</u>
IFlow angle of attack	<u>15</u>		<u>15</u>	

See Comments/Diagram for justification where required