

OK RJ

### SCOUR ANALYSIS AND REPORTING FORM

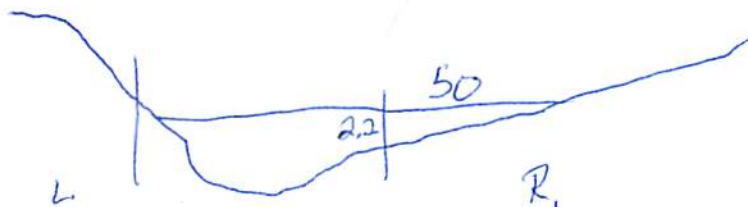
Bridge Structure No. 52310306 Date 9/24/10 Initials CW Region (A)BCD  
 Site \_\_\_\_\_ Location approx. 0.6 S Johnson, on Forest Rd near intersection with HWY 44  
 $Q_{100} =$  856 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 856 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 50 ft. Flow angle at bridge = 30 ° Abut. Skew = 30 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = 50 Vert. Abut  
 Avg. flow depth at bridge,  $y_2$  iteration = 3.4  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 50 ft\*  $q_2 = Q_2/W_2 =$  17.1 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  5 ft/s Final  $y_2 = q_2/V_2 =$  3.4 ft  $\Delta h =$  0.5 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  3.9 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above  $L_S$ , then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 7.4 ft  
 n (Channel) = 0.050  
 n (LOB) = 0.150  
 n (ROB) = 0.150  
 Pier Width = \_\_\_\_\_ ft  
 Pier Length = \_\_\_\_\_ ft  
 # Piers for 100 yr = 0 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  50 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  50 ft Average right overbank flow depth,  $y_{rob} =$  1.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  $Z = 0$

Estimated bed material  $D_{50} =$  0.30 ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  4.39 ft/s 2.19

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  9.38 ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  0.0256 ft

If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_

From Figure 10,  $y_{cs} =$  0.0 ft

#### PIER SCOUR CALCULATIONS

$L/a$  ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0.0 ft right abutment,  $y_{aRT} =$  1.1 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0.0 and  $\psi_{RT} =$  4.7  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  0.0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  8.5 ft  
7.0

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWSNEW

PGRM: Pier

PGRM: Abutment



**SCOUR ANALYSIS AND REPORTING FORM**

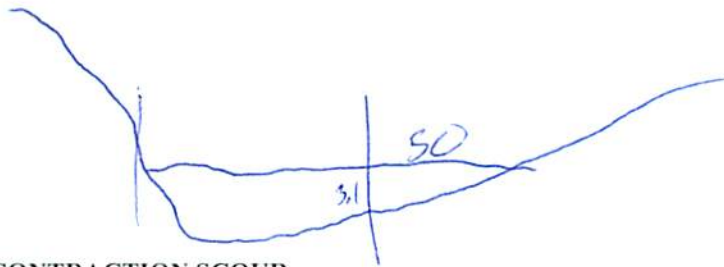
Bridge Structure No. 52310304 Date 9/24/10 Initials CW Region (AB C D)  
 Site \_\_\_\_\_ Location approx abt Johnson, on Forest Rd near intersection with HWY 44  
 $Q_{500} =$  1275 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 1275 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 50 ft. Flow angle at bridge = 30 ° Abut. Skew = 30 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = 50 Vert. Abut.  
 Avg. flow depth at bridge,  $y_2$  iteration = 4.2  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 50 ft\*  $q_2 = Q_2/W_2 =$  25.5 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  6.0 ft/s Final  $y_2 = q_2/V_2 =$  4.2 ft  $\Delta h =$  0.7 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  5.0 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = \_\_\_\_\_ ft  
 n (Channel) = 0.050  
 n (LOB) = 0.150  
 n (ROB) = 0.150  
 Pier Width = \_\_\_\_\_ ft  
 Pier Length = \_\_\_\_\_ ft  
 # Piers for 500 yr = \_\_\_\_\_ ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  50 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  50 ft Average right overbank flow depth,  $y_{rob} =$  1.55 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) 2=0

Estimated bed material  $D_{50} =$  0.3 ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  5.1 ft/s 2.55

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  9.78 ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  0.0356 ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0.0 ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at/bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  1.55 ft  
 Shape coefficient  $K_1 =$  1.80 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  6.4  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  11.7 ft  
9.6

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route Forest Rd Stream Rapid Creek MRM \_\_\_\_\_ Date 9/24/10 Initials Ch  
 Bridge Structure No. 52310306 Location on Forest Rd, near intersection with HWY 44, 0.65 Johnson  
 GPS coordinates: N 44° 04' 23.3" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 103° 25' 55.8" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_  
 Drainage area = 335.56 sq. mi.  
 The average bottom of the main channel was 12.0 ft below top of guardrail at a point 28 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal.  drainage area ratio \_\_\_ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>856</u>			Q <sub>500</sub> = <u>1275</u>		
Estimated flow passing through bridge	<u>856</u>			<u>1275</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour? \_\_\_ Yes  No \_\_\_ Don't know  
 Debris Potential?  High \_\_\_ Med \_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other Large wing walls  Yes \_\_\_ No \_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_ Sand \_\_\_ Gravel \_\_\_ Cobbles  Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

THICK Willows on overbank banks & overbanks  
 1244 - Bridge ID  
 45 - US from bridge  
 46 - US RB  
 47 - US LB  
 48 - US Face of bridge from XS  
 49 - R. Abut  
 50 - R. W.W.  
 51 - L. Abut  
 52 - L. WW  
 53 - Bed material

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>856</u>	<u>1275</u>
Flow depth at left abutment (yaLT), in feet	<u>0.0</u>	<u>0.0</u>
Flow depth at right abutment (yaRT), in feet	<u>1.0 1.1</u>	<u>1.55</u>
Contraction scour depth (yca), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (yps), in feet	<u><del>0.0</del> 0.0 NA</u>	<u><del>0.0</del> NA</u>
Left abutment scour depth (yas), in feet	<u><del>0.0</del> 0.0</u>	<u>0.0</u>
Right abutment scour depth (yas), in feet	<u><del>0.0</del> 7.0</u>	<u><del>11.7</del> 9.6</u>
Flow angle of attack	<u>0°</u>	<u>0°</u>

See Comments/Diagram for justification where required