	-	(L)
		OK by RFT
	SCOUR ANALYSIS AND REPORTING FORM	UNUYNI
	Bridge Structure No. $\underline{62311432}$ Date $\underline{91210}$ Initials $\underline{124}$ Region (\underline{ABCD})	
	Site Location $0.6 \text{ m}_{i} \text{ W of } \text{keystore on Old Hill Gty Re} Q_{100} = 125° by: drainage area ratio flood freq. anal regional regression eq. X$	<u></u>
	$Q_{100} = 125^{\circ}$ by: drainage area ratio flood freq. anal. regional regression eq. \times	
	Bridge discharge $(Q_2) = 1250$ (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)	
	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method	
nB",	Bridge Width = $\underline{47}$ ft. Flow angle at bridge = $\underline{50}$ ° Abut. Skew = $\underline{40}$ ° Effective Skew = \underline{40} ° Effective Skew = $\underline{40}$ ° Effective Skew = \underline{40} ° Effective Skew = 4	
:gion	Avg. flow depth at bridge, y_2 iteration =	
PGRM: "RegionA", "RegionB" 'RegionC", or "RegionD"	Corrected channel width at bridge Section = W, times cos of flow angle = $\frac{46.21}{16.21}$ ft*	Q ² /2
"Re	Corrected channel width at bridge Section = W_2 times cos of flow angle = $\frac{\mathcal{U}\mathcal{L}}{\mathcal{L}^2}$ ft* $q_2 = Q_2/W_2 = \frac{2.7}{\mathcal{L}^2}$ Bridge Vel, $V_2 = \frac{\mathcal{O}}{\mathcal{L}^2}$ ft/s Final $y_2 = q_2/V_2 = \frac{\mathcal{U}}{\mathcal{L}^2}$ ft $\Delta h = \frac{\mathcal{O}}{\mathcal{L}^2}$ ft	11/5
Regi	Bridge ver, $v_2 = \underbrace{v_1 + v_2}_{\text{III}}$ for $v_2 = \underbrace{v_1 + v_2}_{\text{IIII}}$ in $\underbrace{\Delta h} = \underbrace{v_1 + v_2}_{\text{IIIIIIIII}}$	
M: "I	Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 5.2$ ft * NOTE: repeat above calculations until y 2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)	
PGR	If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,	
	Water Surface Elev. = 0 ft Low Steel Elev. = $0.5.9$ ft n (Channel) = 0.035	
	Low Steel Elev. = $\frac{O^2 5.9}{Kack}$ ft 47 Kack wall	
	n (Channel) = 0.036 $n (LOB) = 0.036$	
	n(ROB) = 0	
	Pier Width =ft	
	Pier Length =ft	
	# Piers for 100 yr = $\underline{//}_{ft}$ ft	
	CONTRACTION SCOUR	
	Width of main channel at approach section $W_1 = \frac{47}{1000}$ ft	
act	Width of left overbank flow at approach, $W_{lob} = -\frac{1}{9}$ ft Average left overbank flow depth, $y_{lob} = -\frac{1}{9}$) ft
ontr		
M: C	Width of right overbank flow at approach, $W_{rob} = $ ft Average right overbank flow depth, $y_{rob} = $ ft	ft
PGRM: Contract	Live Bed Contraction Scour (use if bed material is small cobbles or finer)	
	$x = 0, 15$ From Figure 9 W_2 (effective) = 46, 3 ft $y_{cs} = 0, 2$ ft	
MB	Clear Water Contraction Scour (use if bed material is larger than small cobbles)	
SNI	Estimated bed material $D_{50} = $ ft Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = $ ft	's
PGRM: CWCSNEW	Critical approach velocity, $Vc = 11.17y_1^{1/6}D_{50}^{1/3} =ft/s$	
SM:	If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.	
PGI	$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =ft$ If $D_{50} >= D_{c50}, \chi = 0.0$	
	Otherwise, $\chi = 0.122 y_1 [\dot{q}_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = $ From Figure 10, $y_{cs} = $	ft
PGRM: Pier	PIER SCOUR CALCULATIONS	
RM:	L/a ratio = Correction factor for flow angle of attack (from Table 1), K2 =	
PG	Froude # at bridge = Using pier width a on Figure 11, ξ = Pier scour y _{ps} =	ft
	A DEPARTMENT COLD OUT ATTONIC	
PGRM: Abutment	Average flow depth blocked by: $y_{aLT} = \frac{1}{2} O$ ft right abutment, $y_{aRT} = 0$ ft	
Abutt	Shape coefficient $K_1 = 1_00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through	h -
M. 4	Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \frac{473}{2}$ and $\psi_{RT} = \frac{2}{2}$	
JR	Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 2.5$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) =ft$	

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"	SCOUR ANALYSIS AND REPORTING FORM Bridge Structure No. $523 [1432]$ Date 4124 Initials 1244 Region 60 B C D) Site Location to get the structure No. $523 [1432]$ Date $4124 [143]$ D
PGRM: Contract	CONTRACTION SCOUR Width of main channel at approach section $W_1 = \underbrace{\begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \end{array}{c} \end{array}{c} \end{array}{c} \end{array}{c} \end{array}{c} ft Average left overbank flow depth, y_{lob} = \underbrace{\begin{array}{c} \begin{array}{c} \end{array}{c} \end{array}{c} \end{array}{c} } \underbrace{\begin{array}{c} \begin{array}{c} \begin{array}{c} \end{array}{c} \end{array}{c} \end{array}{c} } ft Width of left overbank flow at approach, W_{lob} = \underbrace{\begin{array}{c} \end{array}{c} \end{array}{c} } \underbrace{\begin{array}{c} \begin{array}{c} \end{array}{c} \end{array}{c} } ft Average left overbank flow depth, y_{lob} = \underbrace{\begin{array}{c} \end{array}{c} } \underbrace{\begin{array}{c} \begin{array}{c} \end{array}{c} } 1.9 \\ $
ď	$x = \underbrace{\bigcirc, 4}_{\text{From Figure 9}} \text{ W}_2 \text{ (effective)} = \underbrace{46, 3}_{\text{ft}} \text{ ft} y_{es} = \underbrace{\bigcirc, 7}_{\text{ft}} \text{ ft}$
PGRM: CWCSNEW	$ \begin{array}{c} \underline{\text{Clear Water Contraction Scour}} \text{ (use if bed material is larger than small cobbles)} \\ \hline \text{Estimated bed material D}_{50} = \underline{\qquad} & \text{ft} \\ \hline \text{Critical approach velocity, Vc} = 11.17 y_1^{1/6} \overline{D}_{50}^{1/3} = \underline{\qquad} & \text{ft/s} \\ \hline \text{If V}_1 < V_c \text{ and } D_{50} >= 0.2 \text{ ft, use clear water equation below, otherwise use live bed scour equation above.} \\ \hline D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 = \underline{\qquad} & \text{ft} \\ \hline \text{Otherwise, } \chi = 0.122 y_1 [q_2/(D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\qquad} & \text{From Figure 10, } y_{cs} = \underline{\qquad} & \text{ft} \\ \hline \end{array} $
Pic	L/a ratio = PIER SCOUR CALCULATIONS Froude # at bridge = Correction factor for flow angle of attack (from Table 1), K2 = Using pier width a on Figure 11, ξ = Pier scour y _{ps} =ft
PGRM: Abutment	Average flow depth blocked by: left abutment, $y_{aLT} = 1.9$ ft right abutment, $y_{aRT} =ft$ Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =7$ and $\psi_{RT} =1$ Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) =1^{1/2}$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) =ft$

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PGRM: Contract

PGRM: CWCSNEW

PGRM: Abutment PGRM: Pier

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Route <u>Old Hill Gh Rd</u> Stream <u>Battle Cl</u> Bridge Structure No. <u>52311432</u> Loc GPS coordinates: <u>NU43° 55' 40.71'</u> <u>WI63° 26' (2.3')</u> Drainage area = <u>13.37</u> sq. mi. The average bottom of the main channel was <u>10</u> Method used to determine flood flows: <u>Freq.</u> MIS	tation <u>0,6</u> taken from: Datum of co <u>0</u> ft below Anal.	W; W c USL abutmen ordinates: We v top of guardr drainage area r	sf Keyste t X GS84 X ail at a poin ratio 1	NAD27_ t7 regional regr	OU HI f îl MRM e ft from let ression equ	t abutment. ations.	7	3				
	$Q_{100} = 750$			$Q_{500} = \frac{7860}{2156}$			Z	41,2				
Estimated flow passing through bridge		IZSC			5	132						
Estimated road overflow & overtopping		:0	D		1	10	252					
Consideration	Yes	No	Possibly	Yes	No	Possibly	25	505				
Chance of overtopping		<u> </u>		<u> </u>			So	1819				
Chance of Pressure flow		×		×		X	ice					
Armored appearance to channel			\times		~	~	500	2880				
Lateral instability of channel		X			X		J	1				
Riprap at abutments? Yes No Marginal Evidence of past Scour? Yes No Don't know Same tright Debris Potential? High Med Low Does scour countermeasure(s) appear to have been designed? Riprap Yes No Don't know NA Spur Dike Yes No Don't know NA Other Yes No Don't know NA Bed Material Classification Based on Median Particle Size (D ₅₀) Boulders Boulders Material Silt/Clay Sand Gravel Cobbles Boulders Size range, in mm <0.062												
Summary of Results		1			N. Contraction		1					
	Q100			Q500								
Bridge flow evaluated	1250			2156								
Flow depth at left abutment (yaLT), in feet	1.0											
Flow depth at right abutment (yaRT), in feet	0			6.7								
Contraction scour depth (ycs), in feet	0, 2											
Pier scour depth (yps), in feet	<u>×</u>											
Left abutment scour depth (yas), in feet	7.9			1								
Right abutment scour depth (yas), in feet 0 1Flow angle of attack 10												
1Flow angle of attack	10											

See Comments/Diagram for justification where required

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