

OK RT

SCOUR ANALYSIS AND REPORTING FORM

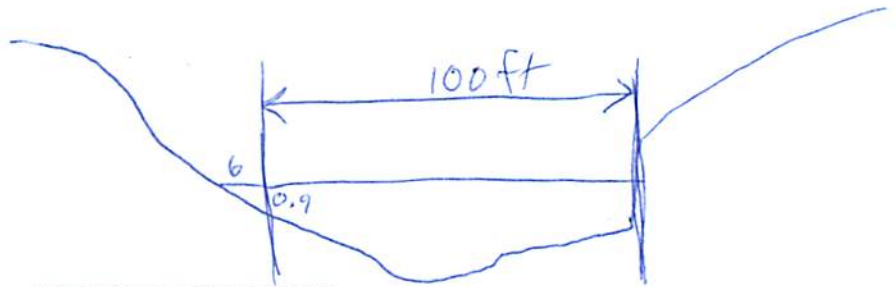
Bridge Structure No. 52314371 Date 10/22/10 Initials CW Region (A B C D)
Site Location First bridge downstream from Mountain Park Road
Q100 = 3010 by: drainage area ratio [checked] flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 3010 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 95 ft. Flow angle at bridge = 50 degrees Abut. Skew = 40 degrees Effective Skew = 10 degrees
Width (W2) iteration = 95 67 80 76
Avg. flow depth at bridge, y2 iteration = 4.8 5.8 5.3 5.4
Corrected channel width at bridge Section = W2 times cos of flow angle = 74.95 ft* q2 = Q2/W2 = 40.2 ft^2/s
Bridge Vel, V2 = 7.4 ft/s Final y2 = q2/V2 = 5.4 ft Delta h = 1.1 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 6.6 ft

* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = ft
Low Steel Elev. = 11.7 ft
n (Channel) = 0.045
n (LOB) = 0.040
n (ROB) = 0.050
Pier Width = 2.0 ft
Pier Length = 2.0 ft
Piers for 100 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section W1 = 100 ft
Width of left overbank flow at approach, Wlob = 6 ft Average left overbank flow depth, ylob = 0.45 ft
Width of right overbank flow at approach, Wrob = 0 ft Average right overbank flow depth, yrob = 0.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = From Figure 9 W2 (effective) = ft ycs = ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) 2=0

Estimated bed material D50 = 0.4 ft Average approach velocity, V1 = Q100/(y1 W1) = 4.8 ft/s

Critical approach velocity, Vc = 11.52 y1^(1/6) D50^(1/3) = 11.27 ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006 (q2/y1^(7/6))^3 = 0.0523 ft

If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122 y1 [q2 / (D50^(1/3) y1^(7/6))]^(6/7) - y1 = From Figure 10, ycs = 0.0 ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), K2 = 1.0
Froude # at bridge = 0.56 Using pier width a on Figure 11, xi = 8 Pier scour yps = 7.3 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 0.45 ft right abutment, yarT = 0.0 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 2.1 and psiRT = 0.0
Left abutment scour, yas = psiLT (K1/0.55) = 2.1 ft Right abutment scour yas = psiRT (K1/0.55) = 0.0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

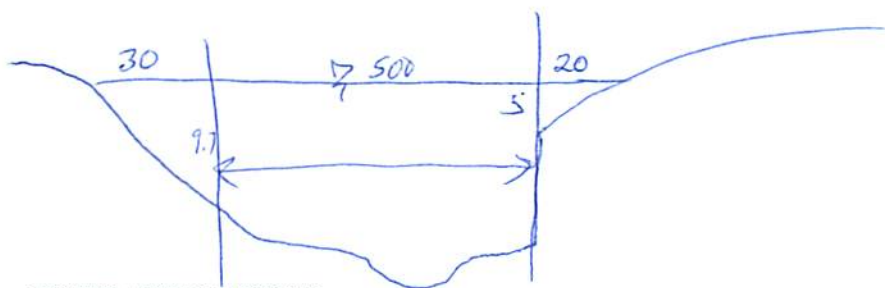
Bridge Structure No. 52314371 Date 10/22/10 Initials CH Region (A B C D)
 Site _____ Location First bridge downstream from Mountain Park Road
 $Q_{500} = \underline{22400}$ by: drainage area ratio flood freq. anal. _____ regional regression eq. _____
 Bridge discharge (Q_2) = 15195 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 95 ft. Flow angle at bridge = 50 ° Abut. Skew = 40 ° Effective Skew = 10 °
 Width (W_2) iteration = 95
 Avg. flow depth at bridge, y_2 iteration = 14.5 RDO over Flow $95 \cos 10^\circ = 93.56$
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 93.56 ft* $q_2 = Q_2/W_2 = \underline{162.7}$ ft²/s
 Bridge Vel, $V_2 = \underline{13.9}$ ft/s Final $y_2 = q_2/V_2 = \underline{11.7}$ ft $\Delta h = \underline{4.0}$ ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \underline{15.7}$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = _____ ft
 Low Steel Elev. = 11.7 ft
 n (Channel) = 0.045
 n (LOB) = 0.040
 n (ROB) = 0.050
 Pier Width = 2.0 ft
 Pier Length = 2.0 ft
 # Piers for 500 yr = 2



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = \underline{100}$ ft
 Width of left overbank flow at approach, $W_{lob} = \underline{30}$ ft Average left overbank flow depth, $y_{lob} = \underline{4.85}$ ft
 Width of right overbank flow at approach, $W_{rob} = \underline{20}$ ft Average right overbank flow depth, $y_{rob} = \underline{2.5}$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
 $x =$ _____ From Figure 9 W_2 (effective) = _____ ft $y_{cs} =$ _____ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) 2=0
 Estimated bed material $D_{50} = \underline{0.4}$ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) = \underline{7.68}$ ft/s 6.45
 Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} = \underline{13.02}$ ft/s
 If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 = \underline{0.164}$ ft If $D_{50} >= D_{c50}$, $\chi = \underline{0.0}$
 Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} = \underline{0.0}$ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), $K_2 = \underline{1.0}$
 Froude # at bridge = 0.72 Using pier width a on Figure 11, $\xi = \underline{8}$ Pier scour $y_{ps} = \underline{7.6}$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = \underline{4.85}$ ft right abutment, $y_{aRT} = \underline{2.5}$ ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \underline{14.8}$ and $\psi_{RT} = \underline{10.2}$
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = \underline{14.8}$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = \underline{10.2}$ ft

4.5
3.5
4.5

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route Sheridan Lk Road Stream Spring Creek MRM _____ Date 10/22/10 Initials ew
 Bridge Structure No. 52314371 Location First bridge downstream from Mountain Park Road
 GPS coordinates: N43°58'56.7" taken from: USL abutment centerline of \uparrow MRM end _____
W103°25'57.7" Datum of coordinates: WGS84 NAD27 _____

Drainage area = 150.84 sq. mi.

The average bottom of the main channel was 15.8 ft below top of guardrail at a point 31 ft from left abutment.

Method used to determine flood flows: _____ Freq. Anal. drainage area ratio _____ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = <u>3010</u>			Q ₅₀₀ = <u>22400</u>		
Estimated flow passing through bridge	<u>3010</u>			<u>15195</u>		
Estimated road overflow & overtopping	<u>7205</u>					
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? _____ Yes _____ No Marginal
 Evidence of past Scour? _____ Yes No _____ Don't know
 Debris Potential? High _____ Med _____ Low

Does scour countermeasure(s) appear to have been designed?

Riprap _____ Yes No _____ Don't know _____ NA
 Spur Dike _____ Yes _____ No _____ Don't know NA
 Other _____ Yes _____ No _____ Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay _____ Sand _____ Gravel _____ Cobbles Boulders _____
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Prescribed burn in area
 1392- 1D
 93- 4S
 94- 4SRB
 95- 4S LB
 96 - L. Abut.
 97 - R. Abut.
 98 - Burn
 99 - Burn

1400 - App. XS R. Bank
01 - App XS L. Bank
02 - 4S Face Dam

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>3010</u>	<u>15195</u>
Flow depth at left abutment (yaLT), in feet	<u>0.45</u>	<u>4.85</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>2.5</u>
Contraction scour depth (yca), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (yps), in feet	<u>7.3</u>	<u>7.6</u>
Left abutment scour depth (yas), in feet	<u>2.1</u>	<u>14.8</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<u>10.2</u>
IFlow angle of attack	<u>10°</u>	<u>10°</u>

See Comments/Diagram for justification where required