

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 52316317 Date 9/30/10 Initials CW Region (A B C D)
Site Location on Thunderhead Falls Rd, 0.2 upstream from Placer Ln
Q100 = 863 by: drainage area ratio [checked] flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 463 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 46 ft. Flow angle at bridge = 60 degrees Abut. Skew = 45 degrees Effective Skew = 15 degrees
Width (W2) iteration = Vert. Abut.

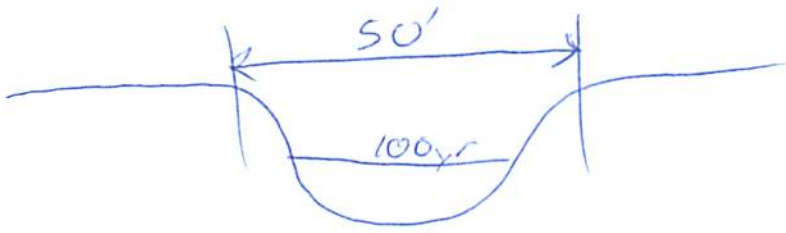
Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 44.43 ft\* q2 = Q2/W2 = 19.4 ft^2/s

Bridge Vel, V2 = 5.3 ft/s Final y2 = q2/V2 = 3.7 ft Delta h = 0.6 ft

Average main channel depth at approach section, y1 = Delta h + y2 = 4.2 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = ft
Low Steel Elev. = ft
n (Channel) = 0.050
n (LOB) = 0.060
n (ROB) = 0.045
Pier Width = ft
Pier Length = ft
# Piers for 100 yr = 0



CONTRACTION SCOUR

Width of main channel at approach section W1 = 50 ft
Width of left overbank flow at approach, Wlob = 0 ft Average left overbank flow depth, ylob = 0 ft
Width of right overbank flow at approach, Wrob = 0 ft Average right overbank flow depth, yrob = 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = From Figure 9 W2 (effective) = ft ycs = ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) 2=0

Estimated bed material D50 = 0.30 ft Average approach velocity, V1 = Q100/(y1W1) = 4.11 ft/s

Critical approach velocity, Vc = 11.52y1^1/6 D50^1/3 = 9.5 ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006(q2/y1^7/6)^3 = 0.0285 ft If D50 >= Dc50 chi = 0.0

Otherwise, chi = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = 0.0 ft

PIER SCOUR CALCULATIONS

L/a ratio = Correction factor for flow angle of attack (from Table 1), K2 =
Froude # at bridge = Using pier width a on Figure 11, xi = Pier scour yps = ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 0 ft right abutment, yaRT = 0 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = and psiRT =
Left abutment scour, yas = psiLT(K1/0.55) = 0 ft Right abutment scour yas = psiRT(K1/0.55) = 0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 52316317 Date 9/30/10 Initials CW Region (AB C D)  
 Site \_\_\_\_\_ Location on Thunderhead Falls Rd, 0.2 Upstream from Placer Ln  
 $Q_{500} =$  1280 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 1280 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

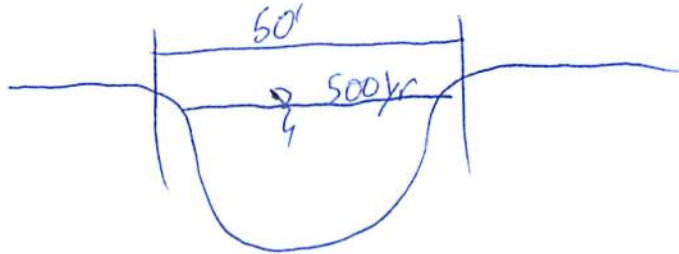
**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 46 ft. Flow angle at bridge = 60 ° Abut. Skew = 45 ° Effective Skew = 15 °  
 Width ( $W_2$ ) iteration = Vert. Abut  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 44.43 ft\*  $q_2 = Q_2/W_2 =$  28.8 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  6.4 ft/s Final  $y_2 = q_2/V_2 =$  4.5 ft  $\Delta h =$  0.8 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  5.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2  
 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = \_\_\_\_\_ ft  
 $n$  (Channel) = 0.050  
 $n$  (LOB) = 0.060  
 $n$  (ROB) = 0.045  
 Pier Width = \_\_\_\_\_ ft  
 Pier Length = \_\_\_\_\_ ft  
 # Piers for 500 yr = 0 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  50 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

PRGM: Contract

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) 2=0

Estimated bed material  $D_{50} =$  0.30 ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  4.74 ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  7.9 ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  0.03917 ft If  $D_{50} \geq D_{c50}$ ,  $\chi =$  0.0

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0.0 ft

PRGM: CWCNEW

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

PRGM: Pie

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  \_\_\_\_\_ and  $\psi_{RT} =$  \_\_\_\_\_  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  0 ft

PRGM: Abutment



Thunderhead

Route Falls Rd Stream Rapid Creek MRM \_\_\_\_\_ Date 9/30/10 Initials ch  
 Bridge Structure No. 52316317 Location On Thunderhead Falls Rd, Upstream from Placer Ln  
 GPS coordinates: N 44° 03' 24.3" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 103° 25' 08.1" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 339.10 sq. mi.

The average bottom of the main channel was 13.3 ft below top of guardrail at a point 15 ft from left abutment.

Method used to determine flood flows: \_\_\_ Freq. Anal.  drainage area ratio \_\_\_ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>863</u>			Q <sub>500</sub> = <u>1280</u>		
Estimated flow passing through bridge	<u>863</u>			<u>1280</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour? \_\_\_ Yes  No \_\_\_ Don't know  
 Debris Potential?  High \_\_\_ Med \_\_\_ Low

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other Lo Wing Wall  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA  
Extra long

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_ Sand \_\_\_ Gravel \_\_\_ Cobbles  Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

1302-1D 08- US Face of Bridge  
 03- US 09- Flowers  
 04- LB US 10- US Face of Bridge  
 05- RB US  
 06- R, Abut.  
 07- L, Abut.

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>863</u>	<u>1280</u>
Flow depth at left abutment (yaLT), in feet	<u>0.0</u>	<u>0.0</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>0.0</u>
Contraction scour depth (yca), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (yps), in feet	<u>0.0 NA</u>	<u>0.0 NA</u>
Left abutment scour depth (yas), in feet	<u>0.0</u>	<u>0.0</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<u>0.0</u>
IFlow angle of attack	<u>15°</u>	<u>15°</u>

See Comments/Diagram for justification where required