

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

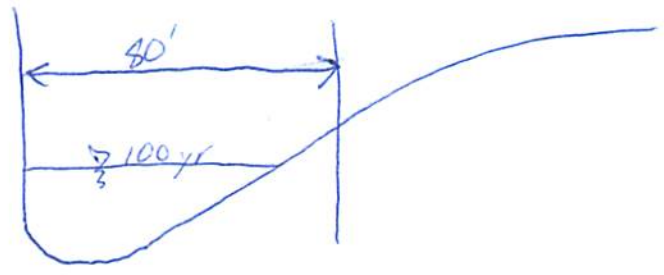
Bridge Structure No. 52318367 Date 10/21/10 Initials CW Region (A B C D)  
 Site \_\_\_\_\_ Location First bridge upstream from Balsar Gulch Rd  
 $Q_{100} =$  3010 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 3010 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 77 ft. Flow angle at bridge = 50 ° Abut. Skew = 25 ° Effective Skew = 25 °  
 Width ( $W_2$ ) iteration = 77 60 64  
 Avg. flow depth at bridge,  $y_2$  iteration = 5.7 6.5 6.3  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 54 ft\*  $q_2 = Q_2/W_2 =$  51.9 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.3 ft/s Final  $y_2 = q_2/V_2 =$  6.3 ft  $\Delta h =$  1.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = ~~11.5~~ ft  
 Low Steel Elev. = 11.5 ft  
 n (Channel) = 0.055  
 n (LOB) = 0.050  
 n (ROB) = 0.055  
 Pier Width = 2.0 ft  
 Pier Length = 2.0 ft  
 # Piers for 100 yr = 2



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  80 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0.0 ft Average left overbank flow depth,  $y_{lob} =$  0.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0.0 ft Average right overbank flow depth,  $y_{rob} =$  0.0 ft

#### Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

#### Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  0.50 ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  4.89 ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  12.46 ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  0.066 ft If  $D_{50} \geq D_{c50}$ ,  $\chi =$  0.0  
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0.0 ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.58 Using pier width a on Figure 11,  $\xi =$  8.0 Pier scour  $y_{ps} =$  7.4 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0.0 ft right abutment,  $y_{aRT} =$  0.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0.0 and  $\psi_{RT} =$  0.0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  0.0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  0.0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment



**SCOUR ANALYSIS AND REPORTING FORM**

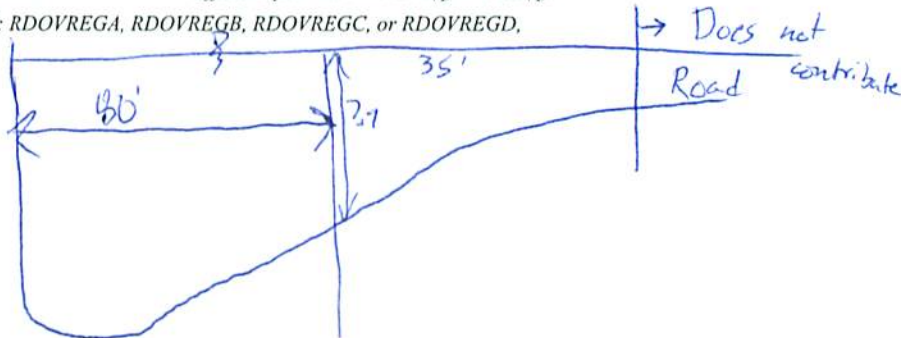
Bridge Structure No. 52318367 Date 10/21/10 Initials CW Region (A B C D)  
 Site \_\_\_\_\_ Location First bridge upstream from Balsar Gulch Rd  
 $Q_{500} =$  22400 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 10944 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 77 ft. Flow angle at bridge = 50° Abut. Skew = 25° Effective Skew = 25°  
 Width ( $W_2$ ) iteration = 77 RD overflow  $77 \cos 25^\circ = 69.79$   
 Avg. flow depth at bridge,  $y_2$  iteration = 17  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 69.79 ft\*  $q_2 = Q_2/W_2 = 157.4$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  13.7 ft/s Final  $y_2 = q_2/V_2 = 11.5$  ft  $\Delta h =$  3.9 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 15.4$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2  
 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = ~~11.5~~ ft  
 Low Steel Elev. = 11.5 ft  
 $n$  (Channel) = 0.055  
 $n$  (LOB) = 0.050  
 $n$  (ROB) = 0.055  
 Pier Width = 2.0 ft  
 Pier Length = 2.0 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  90 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0.0 ft Average left overbank flow depth,  $y_{lob} =$  0.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  35 ft Average right overbank flow depth,  $y_{rob} =$  4.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) 2=0  
 Estimated bed material  $D_{50} =$  0.5 ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  46.92 ft/s 6.2  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  13.94 ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  0.163 ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0.0 ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.71 Using pier width  $a$  on Figure 11,  $\xi =$  4.0 Pier scour  $y_{ps} =$  7.6 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0.0 ft right abutment,  $y_{aRT} =$  4.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0.0 and  $\psi_{RT} =$  13.3  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  0.0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  13.3 ft

3.95  
2/17.9  
6.1

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

Route Sheridan Lake Rd Stream Spring Creek MRM \_\_\_\_\_ Date 10/21/10 Initials CW  
 Bridge Structure No. 52318367 Location First bridge upstream from Balsam Gulch Rd  
 GPS coordinates: N 43° 59' 06.7" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 103° 25' 27.9" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 151.23 sq. mi.  
 The average bottom of the main channel was 15.5 ft below top of guardrail at a point 24 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio \_\_\_\_\_ regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

|                                       |                                |                                     |          |                                     |                                     |                                     |
|---------------------------------------|--------------------------------|-------------------------------------|----------|-------------------------------------|-------------------------------------|-------------------------------------|
| Flows                                 | Q <sub>100</sub> = <u>3010</u> |                                     |          | Q <sub>500</sub> = <u>22400</u>     |                                     |                                     |
| Estimated flow passing through bridge | <u>3010</u>                    |                                     |          | <u>10984</u>                        |                                     |                                     |
| Estimated road overflow & overtopping |                                |                                     |          | <u>11416</u>                        |                                     |                                     |
| Consideration                         | Yes                            | No                                  | Possibly | Yes                                 | No                                  | Possibly                            |
| Chance of overtopping                 |                                | <input checked="" type="checkbox"/> |          | <input checked="" type="checkbox"/> |                                     |                                     |
| Chance of Pressure flow               |                                | <input checked="" type="checkbox"/> |          |                                     |                                     | <input checked="" type="checkbox"/> |
| Armored appearance to channel         |                                | <input checked="" type="checkbox"/> |          |                                     | <input checked="" type="checkbox"/> |                                     |
| Lateral instability of channel        |                                | <input checked="" type="checkbox"/> |          |                                     | <input checked="" type="checkbox"/> |                                     |

Riprap at abutments?  Yes  No  Marginal Rock dumped from construction  
 Evidence of past Scour?  Yes  No  Don't know  
 Debris Potential?  High  Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes  No  Don't know  NA  
 Spur Dike  Yes  No  Don't know  NA  
 Other \_\_\_\_\_  Yes  No  Don't know  NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

|                   |                 |            |              |   |                |
|-------------------|-----------------|------------|--------------|---|----------------|
| Material          | Silt/Clay _____ | Sand _____ | Gravel _____ | Cobbles <input checked="" type="checkbox"/> | Boulders _____ |
| Size range, in mm | <0.062          | 0.062-2.00 | 2.00-64      | 64-250                                      | >250           |

Comments, Diagrams & orientation of digital photos  
 1379 - Bridge ID  
 45 - R. Abut  
 46 - App. XS to Left  
 47 - App. XS to Right  
 48 - "  
 49 - US Face Bridge  
 90 - "  
 11 - Cliff on Left Bank

**Summary of Results**

|  |             |              |
|--|-------------|--------------|
|  | Q100        | Q500         |
| Bridge flow evaluated                        | <u>3010</u> | <u>10984</u> |
| Flow depth at left abutment (yaLT), in feet  | <u>0.0</u>  | <u>0.0</u>   |
| Flow depth at right abutment (yaRT), in feet | <u>0.0</u>  | <u>4.0</u>   |
| Contraction scour depth (yca), in feet       | <u>0.0</u>  | <u>0.0</u>   |
| Pier scour depth (yps), in feet              | <u>7.4</u>  | <u>7.6</u>   |
| Left abutment scour depth (yas), in feet     | <u>0.0</u>  | <u>0.0</u>   |
| Right abutment scour depth (yas), in feet    | <u>0.0</u>  | <u>13.3</u>  |
| Flow angle of attack                         | <u>25°</u>  | <u>25°</u>   |

See Comments/Diagram for justification where required