

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 52320312 Date 9/24/16 Initials AW Region (A) B C D
 Site _____ Location on Thunderhead Falls Rd, near intersection with HWY44
 $Q_{100} =$ 860 by: drainage area ratio flood freq. anal. _____ regional regression eq. _____
 Bridge discharge (Q_2) = 860 (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 39 ft. Flow angle at bridge = 10 ° Abut. Skew = 15 ° Effective Skew = 5 °
 Width (W_2) iteration = _____

Avg. flow depth at bridge, y_2 iteration = _____
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 38.85 ft* $q_2 = Q_2/W_2 =$ 22.1 ft²/s

Bridge Vel, $V_2 =$ 5.6 ft/s Final $y_2 = q_2/V_2 =$ 3.9 ft $\Delta h =$ 0.6 ft

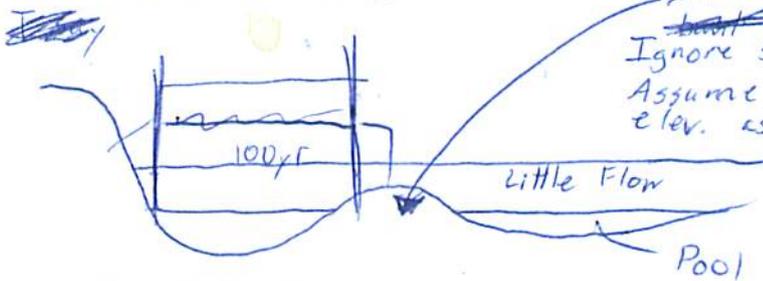
Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 4.6 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 2.3 ft
 Low Steel Elev. = _____ ft
 n (Channel) = 0.040
 n (LOB) = 0.035
 n (ROB) = 0.045
 Pier Width = _____ ft
 Pier Length = _____ ft
 # Piers for 100 yr = 0 ft

See Pics & Diagrams



~~Ignore small bank~~
 Ignore small ~~bank~~ bank
 Assume pool @ same elev. as channel

CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 45 ft
 Width of left overbank flow at approach, $W_{lob} =$ 0 ft Average left overbank flow depth, $y_{lob} =$ 0 ft
 Width of right overbank flow at approach, $W_{rob} =$ 39 ft Average right overbank flow depth, $y_{rob} =$ 4.6 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer) ~~2 = 0.93~~
 $x =$ _____ From Figure 9 W_2 (effective) = _____ ft $y_{cs} =$ 4.15 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) ~~2 = 0.93 0.648 0~~
 Estimated bed material $D_{50} =$ 0.20 ft Average approach velocity, $V_1 = Q_{100}/(y_1 W_1) =$ 4.15 ft/s 2.23

Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ 8.42 ft/s
 If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$ 0.0310 ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$
 Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ 0.0 ft

PIER SCOUR CALCULATIONS

L/a ratio = _____ Correction factor for flow angle of attack (from Table 1), $K_2 =$ _____
 Froude # at bridge = _____ Using pier width a on Figure 11, $\xi =$ _____ Pier scour $y_{ps} =$ _____ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 0 ft right abutment, $y_{aRT} =$ 4.6 ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 0.0 and $\psi_{RT} =$ 14.3
 Left abutment scour, $y_{as} = \psi_{LT} (K_1/0.55) =$ 0 ft Right abutment scour $y_{as} = \psi_{RT} (K_1/0.55) =$ 26 Ch / 21.3 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

neg?

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 52320312 Date 9/24/10 Initials Ch Region (A B C D)
 Site _____ Location on Thunderhead Falls Rd, near intersection with HWY 44
 $Q_{500} =$ 1280 by: drainage area ratio flood freq. anal. _____ regional regression eq. _____
 Bridge discharge (Q_2) = 1280 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

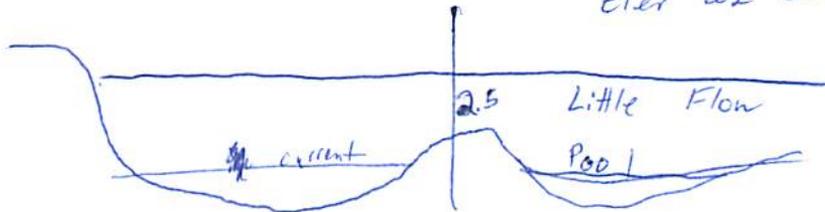
Bridge Width = 39 ft. Flow angle at bridge = 10 ° Abut. Skew = 15 ° Effective Skew = 5 °
 Width (W_2) iteration = _____
 Avg. flow depth at bridge, y_2 iteration = 30.85 ft
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 34.46 ft* $q_2 = Q_2/W_2 =$ 32.9 ft²/s
 Bridge Vel, $V_2 =$ 6.4 ft/s Final $y_2 = q_2/V_2 =$ 4.9 ft $\Delta h =$ 0.9 ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 5.8 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 2.3 ft
 Low Steel Elev. = _____ ft
 n (Channel) = 0.040
 n (LOB) = 0.0305
 n (ROB) = 0.045
 Pier Width = _____ ft
 Pier Length = _____ ft
 # Piers for 500 yr = 0

Ignore small ridge
 Assume pool @ same
 elev as channel



CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 45 ft
 Width of left overbank flow at approach, $W_{lob} =$ 0 ft Average left overbank flow depth, $y_{lob} =$ 0 ft
 Width of right overbank flow at approach, $W_{rob} =$ 39 ft Average right overbank flow depth, $y_{rob} =$ 5.8 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ _____ From Figure 9 W_2 (effective) = _____ ft $y_{cs} =$ _____ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ 0.20 ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ 4.9 ft/s 2.63

Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ 8.76 ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$ 0.043 ft 0.045 If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ 0.0 ft

PIER SCOUR CALCULATIONS

L/a ratio = _____ Correction factor for flow angle of attack (from Table 1), $K_2 =$ _____
 Froude # at bridge = _____ Using pier width a on Figure 11, $\xi =$ _____ Pier scour $y_{ps} =$ _____ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 0 ft right abutment, $y_{aRT} =$ 5.8 ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 8 and $\psi_{RT} =$ 16.5
 Left abutment scour, $y_{as} = \psi_{LT} (K_1/0.55) =$ 0 ft Right abutment scour $y_{as} = \psi_{RT} (K_1/0.55) =$ 29.9 ft
24.5

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

5.8
 2.3
 4.6
 2.5
 2.1

Route Thunderhead Falls Road Stream Rapid Creek MRM _____ Date 9/24/10 Initials CG
 Bridge Structure No. 52320312 Location on Thunderhead Falls Rd, near intersection with Hwy 44
 GPS coordinates: N 44° 03' 53.2" taken from: USL abutment centerline of \uparrow MRM end _____
W 103° 24' 45.4" Datum of coordinates: WGS84 NAD27 _____

Drainage area = 337.33 sq. mi.
 The average bottom of the main channel was 14.1 ft below top of guardrail at a point 10 ft from left abutment.
 Method used to determine flood flows: ___ Freq. Anal. drainage area ratio ___ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = <u>860</u>			Q ₅₀₀ = <u>1280</u>		
Estimated flow passing through bridge	<u>860</u>			<u>1280</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? ___ Yes No ___ Marginal
 Evidence of past Scour? Yes ___ No ___ Don't know scour US L. Abut
 Debris Potential? High ___ Med ___ Low

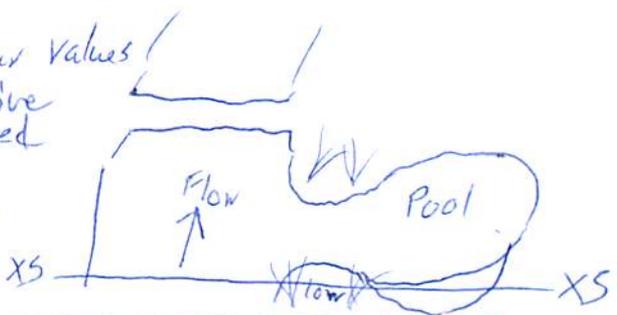
Does scour countermeasure(s) appear to have been designed?
 Riprap ___ Yes ___ No ___ Don't know NA
 Spur Dike ___ Yes ___ No ___ Don't know NA
 Other ___ Yes ___ No ___ Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay ___ Sand ___ Gravel ___ Cobbles Boulders ___
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1264- ID
- 65- US
- 66- RBUS
- 67- LBUS
- 68-70- Graffiti
- 71- R. Abut.
- 72- L. Abut
- Summary of Results
- 73- US face of bridge R. Abut Scour values!
- 74- Scour hole/pool very conservative b/c I ignored small bank
- 75- snake
- 76-77- pool
- 79- Bed Material
- 80- Pool



	Q100	Q500
Bridge flow evaluated	<u>860</u>	<u>1280</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0.0</u>
Flow depth at right abutment (yaRT), in feet	<u>4.6</u>	<u>5.4</u>
Contraction scour depth (yca), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (ypp), in feet	<u>0.0 NA</u>	<u>0.0 NA</u>
Left abutment scour depth (yab), in feet	<u>0.0</u>	<u>0.0</u>
Right abutment scour depth (yrb), in feet	<u>26 21.3</u>	<u>27.9 24.5</u>
Flow angle of attack	<u>5°</u>	<u>5°</u>

See Comments/Diagram for justification where required