

OK T21

SCOUR ANALYSIS AND REPORTING FORM

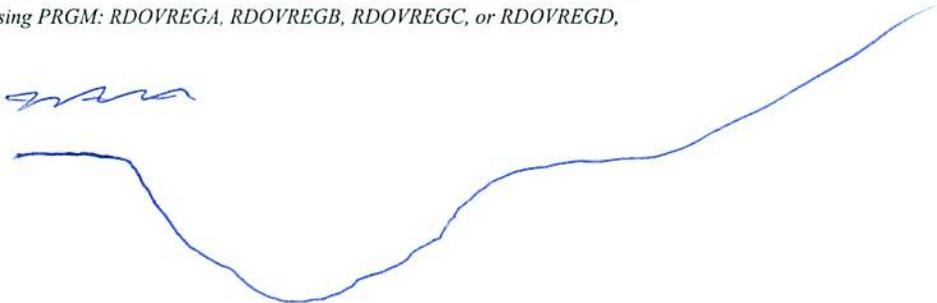
Bridge Structure No. 52322365 Date 10/21/10 Initials AW Region (A B C D)
 Site _____ Location First bridge downstream from Balsar Gulch Rd.
 $Q_{100} =$ 3020 by: drainage area ratio flood freq. anal. _____ regional regression eq. _____
 Bridge discharge (Q_2) = 3020 (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 96 ft. Flow angle at bridge = 50 ° Abut. Skew = 45 ° Effective Skew = 5 °
 Width (W_2) iteration = 96 60 63
 Avg. flow depth at bridge, y_2 iteration = 4.4 6.2 6.0
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 62.76 ft* $q_2 = Q_2/W_2 =$ 48.1 ft²/s
 Bridge Vel, $V_2 =$ 4.0 ft/s Final $y_2 = q_2/V_2 =$ 6.0 ft $\Delta h =$ 1.3 ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 7.3 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = _____ ft
 Low Steel Elev. = 11.0 ft
 n (Channel) = 0.050
 n (LOB) = 0.045
 n (ROB) = 0.045
 Pier Width = 2.0 ft
 Pier Length = 2.0 ft
 # Piers for 100 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 100 ft
 Width of left overbank flow at approach, $W_{lob} =$ 0.0 ft Average left overbank flow depth, $y_{lob} =$ 0.0 ft
 Width of right overbank flow at approach, $W_{rob} =$ ~~7.0~~ 0 ft Average right overbank flow depth, $y_{rob} =$ 0.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ _____ From Figure 9 W_2 (effective) = _____ ft $y_{cs} =$ _____ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) 2=0

Estimated bed material $D_{50} =$ 0.4 ft Average approach velocity, $V_1 = Q_{100}/(y_1 W_1) =$ 4.14 ft/s

Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ 11.46 ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water scour equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$ 0.0635 ft

If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____

From Figure 10, $y_{cs} =$ 0.0 ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0
 Froude # at bridge = 0.58

Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1.0
 Using pier width a on Figure 11, $\xi =$ 8 Pier scour $y_{ps} =$ 7.3 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 0.0 ft right abutment, $y_{aRT} =$ 0.0 ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 0.0 and $\psi_{RT} =$ 0.0
 Left abutment scour, $y_{as} = \psi_{LT} (K_1 / 0.55) =$ 0.0 ft Right abutment scour $y_{as} = \psi_{RT} (K_1 / 0.55) =$ 0.0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 52322365 Date 10/21/10 Initials GW Region (A B C D)
 Site _____ Location First Bridge downstream from Balsar Gulch Rd
 $Q_{500} = \underline{22500}$ by: drainage area ratio flood freq. anal. _____ regional regression eq. _____
 Bridge discharge (Q_2) = ~~13787~~ 13978 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

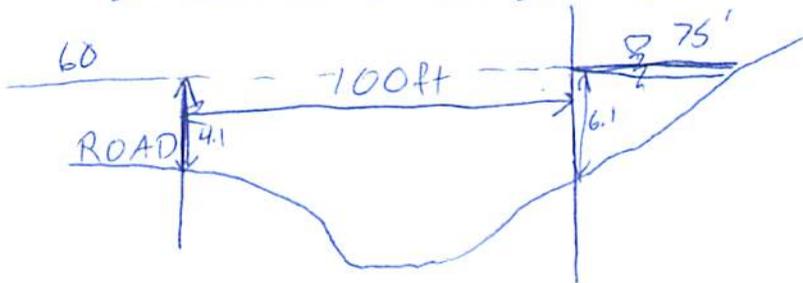
Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 96 ft. Flow angle at bridge = 50 ° Abut. Skew = 45 ° Effective Skew = 5 °
 Width (W_2) iteration = 96 RD overflow mass = 95.63 $96 \cos 5^\circ = 95.63'$
 Avg. flow depth at bridge, y_2 iteration = _____
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 95.63 ft* $q_2 = Q_2/W_2 = \underline{145.1}$ ft²/s
 Bridge Vel, $V_2 = \underline{13.2}$ ft/s Final $y_2 = q_2/V_2 = \underline{11.0}$ ft $\Delta h = \underline{3.6}$ ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \underline{14.6}$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

But LOB Flow won't contribute b/c on road.

Water Surface Elev. = _____ ft
 Low Steel Elev. = 11.0 ft
 n (Channel) = 0.050
 n (LOB) = 0.045
 n (ROB) = 0.045
 Pier Width = 2.0 ft
 Pier Length = 2.0 ft
 # Piers for 500 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = \underline{100}$ ft
 Width of left overbank flow at approach, $W_{lob} = \underline{60}$ ft Average left overbank flow depth, $y_{lob} = \underline{4.10}$ ft
 Width of right overbank flow at approach, $W_{rob} = \underline{75}$ ft Average right overbank flow depth, $y_{rob} = \underline{3.1}$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ _____ From Figure 9 W_2 (effective) = _____ ft $y_{cs} =$ _____ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) $z = 0$

Estimated bed material $D_{50} = \underline{0.4}$ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) = \underline{9.51}$ ft/s 5.43

Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} = \underline{12.47}$ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} = \underline{0.154}$ ft If $D_{50} \geq D_{c50}$, $\chi = \underline{0.0}$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{-0}$ From Figure 10, $y_{cs} = \underline{0.0}$ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), $K_2 = \underline{1.0}$
 Froude # at bridge = 0.7 Using pier width a on Figure 11, $\xi = \underline{8}$ Pier scour $y_{ps} = \underline{7.6}$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = \underline{0.0}$ ft right abutment, $y_{aRT} = \underline{3.1}$ ft
 Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \underline{0.0}$ and $\psi_{RT} = \underline{11.7}$
 Left abutment scour, $y_{as} = \psi_{LT} (K_1/0.55) = \underline{0.0}$ ft Right abutment scour $y_{as} = \psi_{RT} (K_1/0.55) = \underline{11.7}$ ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

Route Sheridan Lake Road Stream Spring Creek MRM _____ Date 10/21/10 Initials CW
 Bridge Structure No. 52322365 Location First bridge downstream from Balsar Gulch Rd
 GPS coordinates: N43°59'19.2" taken from: USL abutment X centerline of \uparrow MRM end _____
W103°25'03.6" Datum of coordinates: WGS84 X NAD27 _____

Drainage area = 151.51 sq. mi.
 The average bottom of the main channel was 15.1 ft below top of guardrail at a point 50 ft from left abutment.
 Method used to determine flood flows: _____ Freq. Anal. _____ drainage area ratio _____ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = <u>3020</u>			Q ₅₀₀ = <u>22500</u>		
Estimated flow passing through bridge	<u>3020</u>			<u>13478</u>		
Estimated road overflow & overtopping	<u>3020</u>			<u>4622</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<u>X</u>		<u>X</u>		
Chance of Pressure flow		<u>X</u>				<u>X</u>
Armored appearance to channel		<u>X</u>			<u>X</u>	
Lateral instability of channel		<u>X</u>			<u>X</u>	

Riprap at abutments? _____ Yes _____ No X Marginal Looks like rock was just dumped
 Evidence of past Scour? _____ Yes X No _____ Don't know
 Debris Potential? X High _____ Med _____ Low

Does scour countermeasure(s) appear to have been designed?
 Riprap _____ Yes X No _____ Don't know _____ NA
 Spur Dike _____ Yes _____ No _____ Don't know X NA
 Other _____ Yes _____ No _____ Don't know X NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material	Silt/Clay _____	Sand _____	Gravel _____	Cobbles <u>X</u>	Boulders _____
Size range, in mm	<0.062	0.062-2.00	2.00-64	64-250	>250

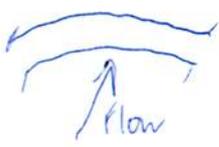
Comments, Diagrams & orientation of digital photos

Prescribed burns in area
US Face bridge is curved

For 500 yr event 20rB
Flow won't contribute
b/c on road already

- 1370-ID
- 71-US
- 72-RBUs
- 73-LBUs
- 74-R. Abut
- 75-App. XS to Right

- 76-App. XS to Left
- 77-L. Abut
- 78-US Face Bridge



Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>3020</u>	<u>13478</u>
Flow depth at left abutment (yaLT), in feet	<u>0.0</u>	<u>0.0</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>3.1</u>
Contraction scour depth (yca), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (yps), in feet	<u>7.3</u>	<u>7.6</u>
Left abutment scour depth (yas), in feet	<u>0.0</u>	<u>0.0</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<u>11.7</u>
Flow angle of attack	<u>5°</u>	<u>5°</u>

See Comments/Diagram for justification where required