

OK RTT

SCOUR ANALYSIS AND REPORTING FORM

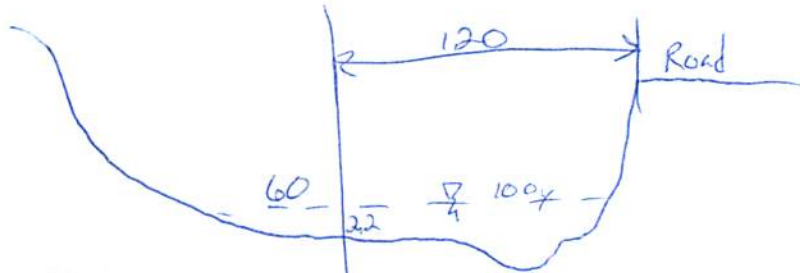
Bridge Structure No. 52323365 Date 10/15/10 Initials CW Region (A B C D)
Site Location Second bridge downstream from Balsar Gulch Rd
Q100 = 3030 by: drainage area ratio flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 3030 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 99 ft. Flow angle at bridge = 70 degrees Abut. Skew = 65 degrees Effective Skew = 5 degrees
Width (W2) iteration = 99 54 87 80 80
Avg. flow depth at bridge, y2 iteration = 4.7 6.5 6.2 5.3 5.3
Corrected channel width at bridge Section = W2 times cos of flow angle = 86.67 ft q2 = Q2/W2 = 35 ft^2/s
Bridge Vel, V2 = 6.4 ft/s 7.2 Final y2 = q2/V2 = 5 ft 5.3 Delta h = 1.0 ft 1.1
Average main channel depth at approach section, y1 = Delta h + y2 = 6.6 6.3 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = - ft
Low Steel Elev. = 10.4 ft
n (Channel) = 0.04
n (LOB) = 0.045
n (ROB) = 0.045
Pier Width = 1.7 ft
Pier Length = 1.7 ft
# Piers for 100 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section W1 = 120 ft
Width of left overbank flow at approach, Wlob = 60 ft Average left overbank flow depth, ylob = 1.1 ft
Width of right overbank flow at approach, Wrob = 0.0 ft Average right overbank flow depth, yrob = 0.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = From Figure 9 W2 (effective) = ft ycs = ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) z=0

Estimated bed material D50 = 0.3 ft Average approach velocity, V1 = Q100/(y1 W1) = 4.21 ft/s 2.67

Critical approach velocity, Vc = 11.52 y1^(1/6) D50^(1/3) = 10.08 ft/s 10.16

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006 (q2/y1^(7/6))^3 = 0.0446 ft 0.0525 If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122 y1 [(q2/(D50^(1/3) y1^(7/6)))^(6/7) - y1 = From Figure 10, ycs = 0.0 ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), K2 = 1.0
Froude # at bridge = 0.54 0.55 Using pier width a on Figure 11, xi = 2.0 Pier scour yps = 6.4 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 1.1 ft right abutment, yarT = 0.0 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 4.7 and psiRT = 0.0
Left abutment scour, yas = psiLT (K1/0.55) = 4.7 ft Right abutment scour yas = psiRT (K1/0.55) = 0.0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment



**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 52323365 Date 10/15/10 Initials Ch Region (AB C D)  
 Site \_\_\_\_\_ Location Second Bridge downstream from Balsar Gulch Rd  
 $Q_{500} =$  22600 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 12839 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

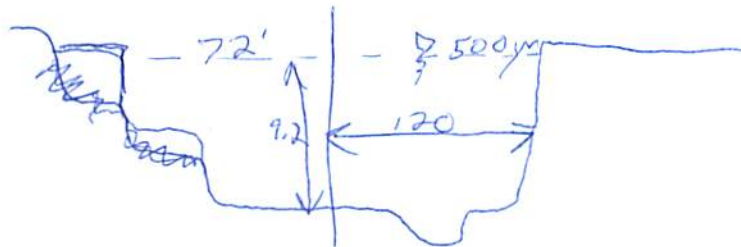
**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 99 ft. Flow angle at bridge = 70 ° Abut. Skew = 65 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 99  
 Avg. flow depth at bridge,  $y_2$  iteration = 19.6 RD Over Flow width =  $99 - \cos 5^\circ = 98 \text{ ft}$   
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 98.62 ft\*  $q_2 = Q_2/W_2 =$  130.2 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  12.6 ft/s Final  $y_2 = q_2/V_2 =$  10.4 ft  $\Delta h =$  3.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  13.6 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = - ft  
 Low Steel Elev. = 10.4 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.045  
 $n$  (ROB) = 0.045  
 Pier Width = 1.7 ft  
 Pier Length = 1.7 ft  
 # Piers for 500 yr = 2

*Q thru bridge = 12839*



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  120 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  72 ft Average left overbank flow depth,  $y_{lob} =$  4.6 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0-0 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)

$x =$  -0.87 From Figure 9  $W_2$  (effective) = 116.6 ft  $y_{cs} =$  7.15 ft *Not sure what's going on. Not live Bed.*

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  0.3 ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  120 ft/s 2=0 4.92

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  11.55 ft/s *went into 2nd routine*

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  0.143 ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0.0 ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.69 Using pier width  $a$  on Figure 11,  $\xi =$  7.0 Pier scour  $y_{ps} =$  6.7 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  4.6 ft right abutment,  $y_{aRT} =$  0.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  14.3 and  $\psi_{RT} =$  0.0  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  14.3 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  0.0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route Sheridan Lake Rd Stream Spring Creek MRM \_\_\_\_\_ Date 10/15/10 Initials CU  
 Bridge Structure No. 52323365 Location Second bridge downstream from Balsar Gulch Rd.  
 GPS coordinates: N 43° 59' 18.6" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 103° 24' 52.5" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 152.69 sq. mi.

The average bottom of the main channel was 14.5 ft below top of guardrail at a point 27 ft from left abutment.

Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio \_\_\_\_\_ regional regression equations.

### MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>3030</u>			Q <sub>500</sub> = <u>22600</u>		
Estimated flow passing through bridge	<u>3030</u>			<u>12839</u>		
Estimated road overflow & overtopping	<u>—</u>			<u>9761</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_\_\_ Yes  No \_\_\_\_\_ Marginal  
 Evidence of past Scour? \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know  
 Debris Potential?  High \_\_\_\_\_ Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

### Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_\_\_ Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles  Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

1338 - ID  
 39 - US  
 40 - USRB  
 41 - USLB  
 42 - US Face of bridge  
 43 - ~~US~~ Looking toward R. overbank  
 44 - again  
 45 - L. overbank  
 46 - R. Abut  
 47 - same  
 48 - L. Abut

### Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>3030</u>	<u>12839</u>
Flow depth at left abutment (yaLT), in feet	<u>1.1</u>	<u>4.6</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>0.0</u>
Contraction scour depth (yca), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (yps), in feet	<u>6.4</u>	<u>6.7</u>
Left abutment scour depth (yas), in feet	<u>4.7</u>	<u>14.3</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<u>0.0</u>
IFlow angle of attack	<u>5°</u>	<u>5°</u>

See Comments/Diagram for justification where required