

OK RT

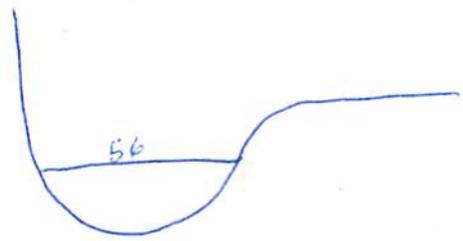
SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 52324266 Date 11/20/10 Initials CH Region (A B C D)
 Site _____ Location 0.5E intersection Nemo Rd + Pine Cone Ave
 $Q_{100} =$ 3480 by: drainage area ratio flood freq. anal. _____ regional regression eq. _____
 Bridge discharge (Q_2) = 3480 (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 110 ft. Flow angle at bridge = 45 ° Abut. Skew = 45 ° Effective Skew = 0 °
 Width (W_2) iteration = 110 57 65 ~~60~~ 66
 Avg. flow depth at bridge, y_2 iteration = 4.8 6.8 6.4 ~~6.3~~ 6.3
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 66 ft* $q_2 = Q_2/W_2 =$ 52.7 ft²/s
 Bridge Vel, $V_2 =$ 8.3 ft/s Final $y_2 = q_2/V_2 =$ 6.3 ft $\Delta h =$ 1.4 ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 7.7 ft
 *NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0 ft
 Low Steel Elev. = 11.9 ft
 n (Channel) = 0.036
 n (LOB) = 0.040 0.050
 n (ROB) = 0.040
 Pier Width = 0.83 ft
 Pier Length = 0.84 ft
 # Piers for 100 yr = 2



CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 110 ft (56?) ← Actual
 Width of left overbank flow at approach, $W_{lob} =$ 0 ft Average left overbank flow depth, $y_{lob} =$ 0 ft
 Width of right overbank flow at approach, $W_{rob} =$ 0 ft Average right overbank flow depth, $y_{rob} =$ 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ _____ From Figure 9 W_2 (effective) = _____ ft $y_{cs} =$ _____ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) z=0

Estimated bed material $D_{50} =$ 0.30 ft Average approach velocity, $V_1 = Q_{100}/(y_1 W_1) =$ 4.11 ft/s
 Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ 10.51 ft/s
 If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$ 0.0693 ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$
 Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ 0.0 ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1.0
 Froude # at bridge = 0.58 Using pier width a on Figure 11, $\xi =$ 4 Pier scour $y_{ps} =$ 3.7 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 0 ft right abutment, $y_{aRT} =$ 0 ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 0 and $\psi_{RT} =$ 0
 Left abutment scour, $y_{as} = \psi_{LT} (K_1/0.55) =$ 0 ft Right abutment scour $y_{as} = \psi_{RT} (K_1/0.55) =$ 0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

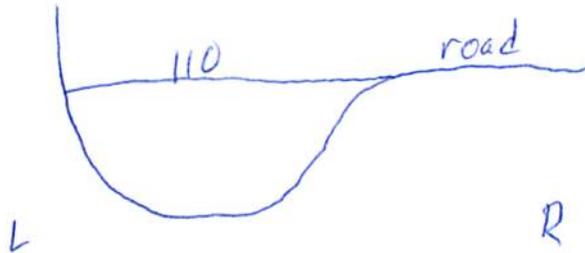
Bridge Structure No. 52324266 Date 11/20/10 Initials CW Region (AB C D)
 Site _____ Location 0.5 E intersection Nemo Rd + Pine Cone Ave
 $Q_{500} =$ 19200 by: drainage area ratio flood freq. anal. _____ regional regression eq. _____
 Bridge discharge (Q_2) = 18426 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 110 ft. Flow angle at bridge = 45 ° Abut. Skew = 45 ° Effective Skew = 0 °
 Width (W_2) iteration = 110
 Avg. flow depth at bridge, y_2 iteration = 12.2 → RDQ over flow
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 110 ft* $q_2 = Q_2/W_2 =$ 167.5 ft²/s
 Bridge Vel, $V_2 =$ 14.1 ft/s Final $y_2 = q_2/V_2 =$ 11.9 ft $\Delta h =$ 4.1 ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 16.0 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0 ft
 Low Steel Elev. = 11.9 ft
 n (Channel) = 0.036
 n (LOB) = 0.050
 n (ROB) = 0.040
 Pier Width = 0.93 ft
 Pier Length = 0.84 ft
 # Piers for 500 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ ~~110~~ ft 110
 Width of left overbank flow at approach, $W_{lob} =$ 0 ft Average left overbank flow depth, $y_{lob} =$ 0 ft
 Width of right overbank flow at approach, $W_{rob} =$ 0 ft Average right overbank flow depth, $y_{rob} =$ ~~0~~ 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ _____ From Figure 9 W_2 (effective) = _____ ft $y_{cs} =$ _____ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) z = 0

Estimated bed material $D_{50} =$ 0.3 ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ 10.47 ft/s

Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ 11.87 ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$ ~~0.0006~~ ft 0.1721

If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ 0.0 ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1.0
 Froude # at bridge = 0.72 Using pier width a on Figure 11, $\xi =$ 4 Pier scour $y_{ps} =$ 3.8 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 0 ft right abutment, $y_{aRT} =$ 0 ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 0 and $\psi_{RT} =$ 0
 Left abutment scour, $y_{as} = \psi_{LT} (K_1 / 0.55) =$ 0 ft Right abutment scour $y_{as} = \psi_{RT} (K_1 / 0.55) =$ 0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route Nemo Rd Stream Boxelder Creek MRM _____ Date 11/20/10 Initials Ch
 Bridge Structure No. 52324266 Location 0.5E intersection Nemo Rd + Pine cone Ave
 GPS coordinates: N 44° 07' 54.6" taken from: USL abutment centerline of ↑ MRM end _____
W 103° 24' 17.7" Datum of coordinates: WGS84 NAD27 _____
 Drainage area = 111.56 sq. mi.
 The average bottom of the main channel was 16.5 ft below top of guardrail at a point 35 ft from left abutment.
 Method used to determine flood flows: _____ Freq. Anal. drainage area ratio _____ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

| | | | | | | |
|---------------------------------------|--------------------------------|-------------------------------------|----------|-------------------------------------|-------------------------------------|-------------------------------------|
| Flows | Q ₁₀₀ = <u>3480</u> | | | Q ₅₀₀ = <u>19200</u> | | |
| Estimated flow passing through bridge | <u>3480</u> | | | <u>18426</u> | | |
| Estimated road overflow & overtopping | <u>←</u> | | | <u>774</u> | | |
| Consideration | Yes | No | Possibly | Yes | No | Possibly |
| Chance of overtopping | | <input checked="" type="checkbox"/> | | <input checked="" type="checkbox"/> | | |
| Chance of Pressure flow | | <input checked="" type="checkbox"/> | | <input checked="" type="checkbox"/> | | <input checked="" type="checkbox"/> |
| Armored appearance to channel | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | |
| Lateral instability of channel | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | |

Riprap at abutments? _____ Yes _____ No Marginal Gabian Baskets underneath
 Evidence of past Scour? _____ Yes No _____ Don't know
 Debris Potential? High _____ Med _____ Low

Does scour countermeasure(s) appear to have been designed?

Riprap Yes _____ No _____ Don't know _____ NA Gabian baskets
 Spur Dike _____ Yes _____ No _____ Don't know NA
 Other _____ Yes _____ No _____ Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay _____ Sand _____ Gravel _____ Cobbles Boulders _____
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

1193 - US from bridge 99 - Downstream
94 - RB US 100 - L. Abut,
95 - LB US 101 - R. Abut
98 - Bridge ID 102 - Bridge from
US

Summary of Results

| | Q100 | Q500 |
|--|-------------|--------------|
| Bridge flow evaluated | <u>3480</u> | <u>18426</u> |
| Flow depth at left abutment (yaLT), in feet | <u>0.0</u> | <u>0.0</u> |
| Flow depth at right abutment (yaRT), in feet | <u>0.0</u> | <u>0.0</u> |
| Contraction scour depth (yca), in feet | <u>0.0</u> | <u>0.0</u> |
| Pier scour depth (yps), in feet | <u>3.7</u> | <u>3.8</u> |
| Left abutment scour depth (yas), in feet | <u>0.0</u> | <u>0.0</u> |
| Right abutment scour depth (yas), in feet | <u>0.0</u> | <u>0.0</u> |
| Flow angle of attack | <u>0°</u> | <u>0°</u> |

See Comments/Diagram for justification where required