

OK 25

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 52327321 Date 10/14/2010 Initials CW Region (A B C D)  
 Site \_\_\_\_\_ Location downstream 0.1 mile from int. Hisega Lane + Triangle Trail  
 $Q_{100} =$  867 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 867 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 50 ft. Flow angle at bridge = 45 ° Abut. Skew = 20 ° Effective Skew = 25 °  
 Width ( $W_2$ ) iteration = vert Abut  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 45.32 ft\*  $q_2 = Q_2/W_2 =$  19.1 ft<sup>2</sup>/s

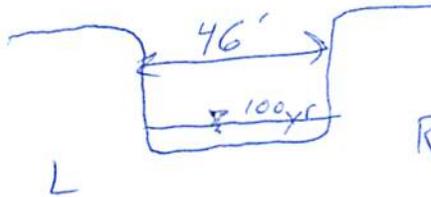
Bridge Vel,  $V_2 =$  5.3 ft/s Final  $y_2 = q_2/V_2 =$  3.6 ft  $\Delta h =$  0.6 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  4.2 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = \_\_\_\_\_ ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.040  
 Pier Width = \_\_\_\_\_ ft  
 Pier Length = \_\_\_\_\_ ft  
 # Piers for 100 yr = 0 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  50 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  0.16 From Figure 9  $W_2$  (effective) = 45.3 ft  $y_{cs} =$  0.1 ft

See comments

Clear Water Contraction Scour (use if bed material is larger than small cobbles) 2=0 2=0.567 2=0.499 2=0

Estimated bed material  $D_{50} =$  0.2 ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  4.49 ft/s 4.13

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  8.3 ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  0.0276 ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0.0 ft

#### PIER SCOUR CALCULATIONS

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0.0 ft right abutment,  $y_{aRT} =$  0.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0.0 and  $\psi_{RT} =$  0.0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  0.0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  0.0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

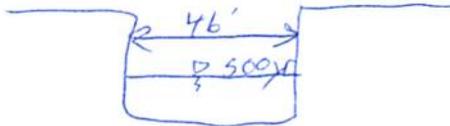
Bridge Structure No. 52327321 Date 10/14/2010 Initials ew Region (A B C D)  
 Site \_\_\_\_\_ Location downstream 0.1 mile from int. Hisega Ln and Triangle Tr.  
 $Q_{500} =$  1290 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 1290 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 50 ft. Flow angle at bridge = 45 ° Abut. Skew = 20 ° Effective Skew = 25 °  
 Width ( $W_2$ ) iteration = Vert Abut  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 45.32 ft\*  $q_2 = Q_2/W_2 =$  28.5 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  6.3 ft/s Final  $y_2 = q_2/V_2 =$  4.5 ft  $\Delta h =$  0.8 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  5.3 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = \_\_\_\_\_ ft  
 n (Channel) = 0.040  
 n (LOB) = 0.035  
 n (ROB) = 0.040  
 Pier Width = \_\_\_\_\_ ft  
 Pier Length = \_\_\_\_\_ ft  
 # Piers for 500 yr = 0 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  46.50 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0.0 ft Average left overbank flow depth,  $y_{lob} =$  0.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0.0 ft Average right overbank flow depth,  $y_{rob} =$  0.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  0.55 From Figure 9  $W_2$  (effective) = 45.3 ft  $y_{cs} =$  0.9 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  ~~$z = 0.86$~~   ~~$z = 0.119$~~   $z = 0$

Estimated bed material  $D_{50} =$  0.2 ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  5.27 ft/s 4.87

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  4.63 ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  0.0405 ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0.0 ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0.0 ft right abutment,  $y_{aRT} =$  0.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0.0 and  $\psi_{RT} =$  0.0  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  0.0 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  0.0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route Hisega Ln Stream Rapid Creek MRM \_\_\_\_\_ Date 10/14/10 Initials CW  
 Bridge Structure No. 52327321 Location downstream 0.1 mi from int. Hisega Ln and Triangle Tr.  
 GPS coordinates: N 44° 03' 06.3" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 103° 24' 02.3" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 341.38 sq. mi.

The average bottom of the main channel was 9 ft below top of guardrail at a point 15.3 ft from left abutment.

Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio \_\_\_\_\_ regional regression equations.

### MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>867</u>			Q <sub>500</sub> = <u>1290</u>		
Estimated flow passing through bridge	<u>867</u>			<u>1290</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_\_\_ Yes  No \_\_\_\_\_ Marginal  
 Evidence of past Scour? \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know  
 Debris Potential?  High \_\_\_\_\_ Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other large wing wall  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

### Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_\_\_ Sand \_\_\_\_\_ Gravel  Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

D<sub>50</sub> is probably smaller than 0.2 ft → Bed material ~~is~~ large gravel & small cobbles  
 I do not suspect much erosion. But ran live bed just to see. Both say basically 0.  
 Photos 13-1D 16- R. Wing Wall 19- R. overbank at approach XS  
 13- US 17- L. Wing Wall 20- R. Wing Wall  
 14- US LB 18- US Face of bridge  
 15- US RB from US XS

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>867</u>	<u>1290</u>
Flow depth at left abutment (yaLT), in feet	<u>0.0</u>	<u>0.0</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>0.0</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>NA</u>	<u>NA</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>0.0</u>	<u>0.0</u>
Right abutment scour depth (y <sub>rs</sub> ), in feet	<u>0.0</u>	<u>0.0</u>
IFlow angle of attack	<u>25°</u>	<u>25°</u>

See Comments/Diagram for justification where required