| | SCOUR ANALYSIS AND REPORTING FORM 2 1/ |
|--|--|
| | Bridge Structure No. 52327364 Date 10/15/10 Initials CW Region (ABCD) Bouller |
| | Site Location First bridge downstream from Baker Park Rd |
| | Site Location First bridge downstream from Baker Park Rd Q ₁₀₀ = 3100 by: drainage area ratio regional regression eq |
| | Bridge discharge $(Q_2) = 3/00$ (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping) |
| | Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method |
| , g | 16 |
| PGRM: "RegionA", "RegionB", 'RegionC", or "RegionD" | Width (W_2) iteration = 95 |
| | Width (W_2) iteration = $\frac{9}{4}$ $\frac{9}{4}$ $\frac{66}{4}$ $\frac{73}{5}$ $\frac{72}{5}$ Avg. flow depth at bridge, y_2 iteration = $\frac{9}{4}$ $\frac{9}{6}$ $\frac{66}{2}$ $\frac{5}{5}$ $\frac{5}{5}$ $\frac{5}{9}$ $\frac{5}{5}$ $\frac{5}{6}$ $\frac{5}{7}$ Corrected channel width at bridge Section = W_2 times cos of flow angle = $\frac{72}{10}$ $\frac{1}{10}$ 1 |
| | Corrected channel width at bridge Section = W_2 times cos of flow angle = $\frac{7}{2}$ ft* $q_2 = Q_2/W_2 = \frac{43}{3}$ ft ² /s |
| | Bridge Vel, $V_2 = 7 \cdot k$ ft/s Final $y_2 = q_2/V_2 = 5 \cdot 7$ ft $\Delta h = 1/2$ ft |
| | Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 6.8$ |
| RM: gion | * NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$ |
| PGR "Reg | |
| | - 11 155 - 500 vs y 95 |
| | Water Surface Elev. = ft |
| | Low Steel Elev. = 10.3 ft |
| | $ \frac{n \text{ (Channel)} = 0.040}{n \text{ (LOB)} = 0.045} $ |
| | n(ROB) = 0.045 |
| | Pier Width = 1, 6 ft |
| | Pier Length = 10 II |
| | # Piers for 100 yr = $\frac{2}{ft}$ ft |
| | |
| PGRM: Contract | CONTRACTION SCOUR for 100 |
| | Width of main channel at approach section $W_1 = 155$ |
| | Width of left overbank flow at approach, $W_{lob} = $ ft Average left overbank flow depth, $y_{lob} = $ ft |
| | Width of right overbank flow at approach, $W_{rob} = 16$ ft Average right overbank flow depth, $y_{rob} = 16$ ft |
| I.R.M | \bigcap \bigcap |
| PC | <u>Live Bed Contraction Scour</u> (use if bed material is small cobbles or finer) |
| | $x = $ ft $y_{cs} = $ ft |
| PGRM: CWCSNEW | Clear Water Contraction Scour (use if bed material is larger than small cobbles) 2=0 /.82 |
| | Estimated bed material $D_{50} = 0.00$ ft Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = \frac{2.94}{1.57}$ ft/s |
| VCS | Estimated bed material $D_{50} = \frac{1}{2}$ It Average approach velocity, $v_1 = Q_{100}/(y_1 w_1) = \frac{1}{2}$ Its |
| . C | Critical approach velocity, $Vc = 11.52y_1^{1/6}D_{50}^{1/3} = \frac{10.29}{10.29}$ ft/s |
| iRM | If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above. |
| PO | $D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = 0.0566 \text{ ft}$ If $D_{50} > = D_{c50}, \chi = 0.0$ |
| | Otherwise, $\chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 = $ From Figure 10, $y_{cs} = $ ft |
| icr | LIER SCOUR CALCULATIONS |
| Α. Τ | L/a ratio = Correction factor for flow angle of attack (from Table 1), K2 = (1) |
| GRM: Pier | L/a ratio = Correction factor for flow angle of attack (from Table 1), $K2 = 1.0$ Using pier width a on Figure 11, $\xi = 7.4$ Pier scour $y_{ps} = 6.7$ ft |
| - | Trodae in artifact of the state |
| ī. | ABUTMENT SCOUR CALCULATIONS |
| utme | ABUTMENT SCOUR CALCULATIONS Average flow depth blocked by: left abutment, $y_{aLT} = 0.0$ ft right abutment, $y_{aRT} = ft$ Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through |
| Abı | |
| PGRM: Abutment | Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = 0.0$ and $\psi_{RT} = 0.0$ |
| PG | Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 0$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 0$ ft |

| Sheridan | 0 \ | MDM | 2 | 10-111 | / // | | | |
|---|----------------|------------------|----------|---------|-------------------|------------|--|--|
| RouteLake Rd Stream Spring Creek MRM Date 10/15/16 Initials Ch | | | | | | | | |
| Bridge Structure No. 52327364 | Location First | - bridge | downstr | eam fro | m Bak | es Park Ro | | |
| Bridge Structure No. 52327364 Location First bridge downstream from Baker Park Roges coordinates: NY3°59' 18.7" taken from: USL abutment × centerline of 11 MRM end Datum of coordinates: WGS84 NAD27 | | | | | | | | |
| $\sqrt{103^{\circ} 24' 4.7''}$ Datum of coordinates: WGS84 NAD27 | | | | | | | | |
| Drainage area = 157.49 sq. mi. | | | | | | | | |
| The average bottom of the main channel was 14.5 ft below top of guardrail at a point 33 ft from left abutment. Method used to determine flood flows: Freq. Anal. Advanage area ratio. regional regression equations | | | | | | | | |
| Method used to determine flood flows:Freq. Analdrainage area ratioregional regression equations. | | | | | | | | |
| MISCELLANEOUS CONSIDERATIONS | | | | | | | | |
| Flows | $Q_{100} =$ | $Q_{100} = 3100$ | | | $Q_{500} = 23100$ | | | |
| Estimated flow passing through bridge | | 3160 | | | 12228 | | | |
| Estimated road overflow & overtopping | | | | | 10,872 | | | |
| Consideration | Yes | No | Possibly | Yes | No | Possibly | | |
| Chance of overtopping | | Χ | | X | | | | |
| Chance of Pressure flow | | X | | | - (| <u>X</u> | | |
| Armored appearance to channel | | X | _ | | X | | | |
| Lateral instability of channel | | | | | | | | |
| Riprap at abutments? Yes No Marginal | | | | | | | | |
| Evidence of past Scour? Yes No Don't know | | | | | | | | |
| Debris Potential? High Med Low | | | | | | | | |
| Debits Fotential: | | | | | | | | |
| Does scour countermeasure(s) appear to have been designed? | | | | | | | | |
| Riprap Yes No Don't know NA | | | | | | | | |
| Spur Dike Yes No Don't know NA | | | | | | | | |
| OtherYesNoDon't knowNA | | | | | | | | |
| | | | | | | | | |
| Bed Material Classification Based on Median Particle Size (D ₅₀) | | | | | | | | |
| Material Silt/Clay Sand | | Gravel | | | Cobbles Boulders | | | |
| | | .00 2.00-64 | | | | >250 | | |
| CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTR | | | | | | | | |
| Comments, Diagrams & orientation of digital pl | idde | | | | | | | |
| 136/- 10 67-45 race & Dr. age | | | | | | | | |
| 1361-10 67-45 Face & bridge 62-45 68- App. XS looking 10ft 63-45RB 69-App XS 100king right | | | | | | | | |
| 63- USRB 69-APP XS 100King right | | | | | | | | |
| | | | | | | | | |
| 11 - L. Abut Mar | | | | | | | | |
| 66 - R. Abut | | | | | | | | |
| 46 - N. 1000 | | | | | | | | |
| Summary of Results | | | | | | | | |
| Deidos flam analysts d | | Q100 | | Q500 | | | | |
| Bridge flow evaluated Flow depth at left abutment (yaLT), in feet | | 3100 | | | 12228 | | | |
| Flow depth at right abutment (yaRT), in feet | | 0.0 | | | 2.6 | | | |
| Contraction scour depth (ycs), in feet | | 0.0 | | | 60 | | | |
| Pier scour depth (yps), in feet | 1 | 6.0 | | | 7.0 | | | |
| Left abutment scour depth (yas), in feet | | 0.0 | | 0. | 0 | | | |
| Right abutment scour depth (yas), in feet | | 2.0 | | 10. | 6 | | | |
| 1Flow angle of attack | | 0° | | | 0° | | | |