

OK by RFT 3<sup>rd</sup>

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 52341445 Date 9/2/12 Initials RAT Region (A B C D)
Site Location 1.5 mi S of Harney on CR330 or Playhouse Rd
Q100 = 1820 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = 1820 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 45 ft. Flow angle at bridge = 5 degrees Abut. Skew = 0 degrees Effective Skew = 5 degrees
Width (W2) iteration =

Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 44.83 ft\* q2 = Q2/W2 = 40.6 ft^2/s

Bridge Vel, V2 = 7.4 ft/s Final y2 = q2/V2 = 5.5 ft Delta h = 1.1 ft

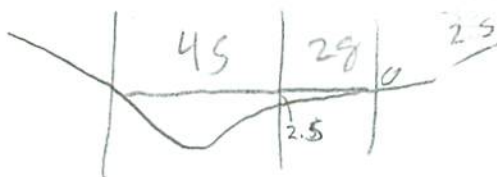
Average main channel depth at approach section, y1 = Delta h + y2 = 6.6 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2

Effective pier width = L sin(a) + a cos(a)

If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 0 ft
Low Steel Elev. = 12.5 ft
n (Channel) = 0.045
n (LOB) = 0.037
n (ROB) = 0.035
Pier Width = X ft
Pier Length = X ft
# Piers for 100 yr = X ft



Handwritten calculations on the right side of the page:
4.14
1.7
3.7
12.5
5.4
7.1
9.5
-5.4
4.1
2.5

CONTRACTION SCOUR

Width of main channel at approach section W1 = 45 ft

Width of left overbank flow at approach, Wlob = 0 ft

Width of right overbank flow at approach, Wrob = 29 ft

Average left overbank flow depth, ylob = 0 ft

Average right overbank flow depth, yrob = 1.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 0.38 From Figure 9 W2 (effective) = 44.8 ft ycs = 0.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s

Critical approach velocity, Vc = 11.17 y1^1/6 D50^1/3 = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006 (q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122 y1 [q2 / (D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio =

Correction factor for flow angle of attack (from Table 1), K2 =

Froude # at bridge =

Using pier width a on Figure 11, xi = Pier scour yps = ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 0 ft right abutment, yarT = 1.3 ft

Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for yalT and yarT on figure 12, psiLT = 0 and psiRT = 5.5

Left abutment scour, yas = psiLT (K1/0.55) = 0 ft Right abutment scour yas = psiRT (K1/0.55) = 9.9 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 52341445 Date 9/2/12 Initials PAT Region (A B C D)  
 Site \_\_\_\_\_ Location 1.5 mi S of Harney on Playhouse Rd  
 $Q_{500} =$  4400 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 4400 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 45 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 44.83 ft\*  $q_2 = Q_2/W_2 =$  99.2 ft<sup>2</sup>/s

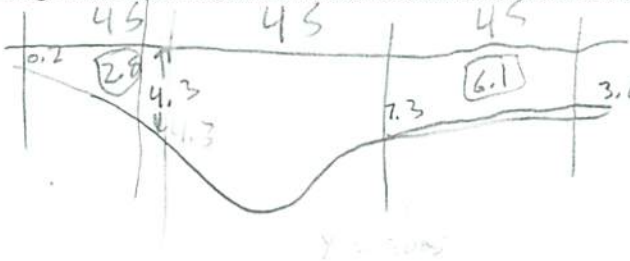
Bridge Vel,  $V_2 =$  11.1 ft/s Final  $y_2 = q_2/V_2 =$  8.9 ft  $\Delta h =$  2.5 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  11.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0 ft  
 Low Steel Elev. = 12.3 ft  
 $n$  (Channel) = 0.015  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.035  
 Pier Width = X ft  
 Pier Length = X ft  
 # Piers for 500 yr = X ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  45 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  45 ft Average left overbank flow depth,  $y_{lob} =$  2.8 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  45 ft Average right overbank flow depth,  $y_{rob} =$  6.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  6.89 From Figure 9  $W_2$  (effective) = 44.8 ft  $y_{cs} =$  7.7 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{cs} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{cs}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: -left abutment,  $y_{aLT} =$  2.8 ft right abutment,  $y_{aRT} =$  6.1 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  11.2 and  $\psi_{RT} =$  17  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  20.3 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  30.9 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Handwritten notes:  $\frac{28}{43} \rightarrow 4.3 - 0.2$   
 $7.3 - 3.6 = 3.7$   
 $3.7 \cdot \frac{2}{3} + 3.6$   
 sec notes

right on playhouse - d

103.37861  
43.8734

1030 22' 42.996  
43° 52' 25.66  
11

Route Playhouse Rd Stream IRAV ck MRM \_\_\_\_\_ Date 9/2/12 Initials DAT  
 Bridge Structure No. 52341445 Location 1.5 mi S of Harney on CR330 of Playhouse Rd  
 GPS coordinates: N 43° 52' 25.5" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 103° 22' 43.4" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 17.59 sq. mi.  
 The average bottom of the main channel was 17 ft below top of guardrail at a point 17 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> =	Q <sub>500</sub> =				
Estimated flow passing through bridge	1820	4400				
Estimated road overflow & overtopping	0	0				
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		X			X	
Chance of Pressure flow		X			X	
Armored appearance to channel		X			X	
Lateral instability of channel		X			X	

7/3  
 2 517.7  
 5 175  
 10 394  
 25 708  
 50 1180  
 100 1820  
 500 4400

Riprap at abutments? \_\_\_\_\_ Yes  No \_\_\_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know *inlet contraction*  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_\_\_ Gravel  Cobbles  Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1) left abutment  
 2) main channel  
 3) right abutment  
 4) bed material  
 5) right abutments  
 6-7) right abutments  
 8-9) left abutment  
 10) main channel  
 Note: slow flow region of bridge is gravel/cobbles. Full flow region is silt. Consider clear water scour.

Summary of Results

	Q100	Q500
Bridge flow evaluated	1820	4400
Flow depth at left abutment (yaLT), in feet	0	2.9
Flow depth at right abutment (yaRT), in feet	1.3	6.1
Contraction scour depth (yca), in feet	X 0.6	7.7
Pier scour depth (yps), in feet	X	X
Left abutment scour depth (yas), in feet	0	20.3
Right abutment scour depth (yas), in feet	9.4	30.4
Flow angle of attack	5	5

See Comments/Diagram for justification where required