

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 52378315 Date 11/13/10 Initials CW Region (A B C D)
Site Location Chapel Lane over Canyon Lake
Q100 = 2230 by: drainage area ratio [checked] flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 2230 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

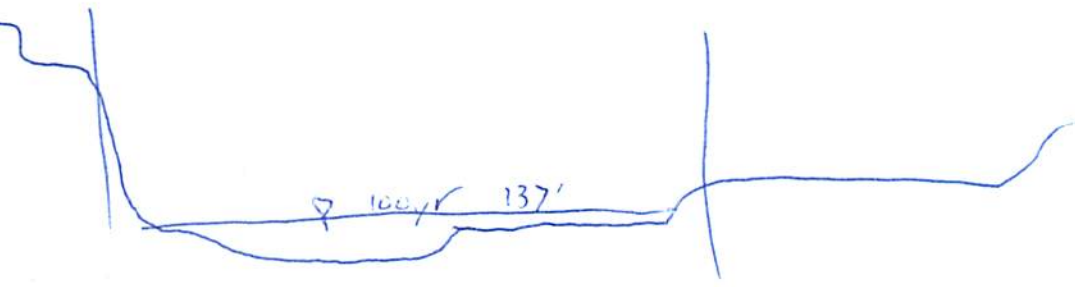
Bridge Width = 122 ft. Flow angle at bridge = 20 degrees Abut. Skew = 0 degrees Effective Skew = 20 degrees
Width (W2) iteration = ~Vert Abut

Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 114.64 ft\* q2 = Q2/W2 = 19.5 ft^2/s

Bridge Vel, V2 = 5.3 ft/s Final y2 = q2/V2 = 3.7 ft Delta h = 0.6 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 4.2 ft + 0.8' for Delta ws over weir = 5.0'
Effective pier width = L sin(q) + a cos(q)

\* NOTE: repeat above calculations until y2 changes by less than 0.2
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = ft
Low Steel Elev. = 10.2 ft
n (Channel) = 0.045
n (LOB) = 0.075
n (ROB) = 0.075
Pier Width = ft
Pier Length = ft
# Piers for 100 yr = 0



CONTRACTION SCOUR

Width of main channel at approach section W1 = 137 ft
Width of left overbank flow at approach, Wlob = 0 ft Average left overbank flow depth, ylob = 0 ft
Width of right overbank flow at approach, Wrob = 0 ft Average right overbank flow depth, yrob = 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = From Figure 9 W2 (effective) = ft ycs = ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) z = 0
Estimated bed material D50 = 0.5 ft Average approach velocity, V1 = Q100/(y1W1) = 3.88 ft/s
Critical approach velocity, Vc = 11.52y1^1/6 D50^1/3 = 11.26 ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006(q2/y1^7/6)^3 = 0.0159 ft 0.029 If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = 0.0 ft

PIER SCOUR CALCULATIONS

L/a ratio = Correction factor for flow angle of attack (from Table 1), K2 =
Froude # at bridge = Using pier width a on Figure 11, xi = Pier scour yps = ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 0 ft right abutment, yaRT = 0 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = 0 and psiRT = 0
Left abutment scour, yas = psiLT(K1/0.55) = 0 ft Right abutment scour yas = psiRT(K1/0.55) = 0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 52378315 Date 11/13/10 Initials GW Region (A B C D)

Site \_\_\_\_\_ Location Chapel Lane over Canyon Lake

$Q_{500} =$  12300 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_

Bridge discharge ( $Q_2$ ) = 12300 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 122 ft. Flow angle at bridge = 20 ° Abut. Skew = 0 ° Effective Skew = 20 °

Width ( $W_2$ ) iteration = ~ Vert Abut

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 114.64 ft\*  $q_2 = Q_2/W_2 =$  107.3 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  11.5 ft/s Final  $y_2 = q_2/V_2 =$  9.3 ft  $\Delta h =$  2.7 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  12.1 ft + 0.8 = 12.9 ~~ft~~

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2

Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft

Low Steel Elev. = ~~9.2~~ 10.2 ft

n (Channel) = 0.045

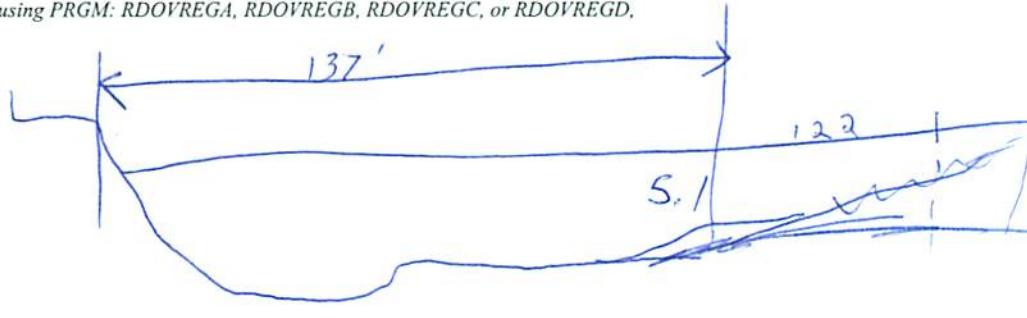
n (LOB) = 0.075

n (ROB) = 0.075

Pier Width = \_\_\_\_\_ ft

Pier Length = \_\_\_\_\_ ft

# Piers for 500 yr = 0 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  137 ft

Width of left overbank flow at approach,  $W_{lob} =$  0 ft

Average left overbank flow depth,  $y_{lob} =$  0 ft

Width of right overbank flow at approach,  $W_{rob} =$  122 ft

Average right overbank flow depth,  $y_{rob} =$  5.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  0.5 ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  6.76 ft/s 3.92 ~~3.92~~ 3.69

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  13.58 ft/s ~~13.58~~ 13.43

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water scour equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  0.696 0.12 ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0.0 ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table-1),  $K_2 =$  \_\_\_\_\_

Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  5.1 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  15.2

Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  27.6 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment

Route Chapel Ln Stream Rapid Creek MRM \_\_\_\_\_ Date 11/13/10 Initials AK  
 Bridge Structure No. 52378315 Location Chapel Lane over Canyon Lake  
 GPS coordinates: N 44° 03' 35.7" taken from: USL abutment \_\_\_\_\_ centerline of MRM end \_\_\_\_\_  
W 103° 17' 42.3" Datum of coordinates: WGS84 \_\_\_\_\_ NAD27 \_\_\_\_\_

Drainage area = 396.84 sq. mi.  
 The average bottom of the main channel was 20.0 ft below top of guardrail at a point 32 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio \_\_\_\_\_ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>2230</u>			Q <sub>500</sub> = <u>12300</u>		
Estimated flow passing through bridge	<u>2230</u>			<u>12300</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_\_\_ Yes  No \_\_\_\_\_ Marginal  
 Evidence of past Scour? \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know  
 Debris Potential?  High \_\_\_\_\_ Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_\_\_ Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles  Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Weir ~ 10 ft us from bridge will have to add ΔWS elev to approach XS  
 Not sure if Level 1.5 Method is valid on this bridge. 75- Weir  
 Photos 66- US RB 69- LB of App XS 72- L. Abut 76- Weir  
 1464- ID 67- US LB 70- RB of App XS 73- Weir us from bridge  
 65- US 68- US Face bridge 71- R. Abut 74- Bed Material

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>2230</u>	<u>12300</u>
Flow depth at left abutment (yaLT), in feet	<u>0.0</u>	<u>0.0</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>5.1</u>
Contraction scour depth (yca), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (ypp), in feet	<u>NA</u>	<u>NA</u>
Left abutment scour depth (yas), in feet	<u>0.0</u>	<u>0.0</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<u>27.6</u>
Flow angle of attack	<u>20</u>	<u>20°</u>

See Comments/Diagram for justification where required