

OK TCT

### SCOUR ANALYSIS AND REPORTING FORM

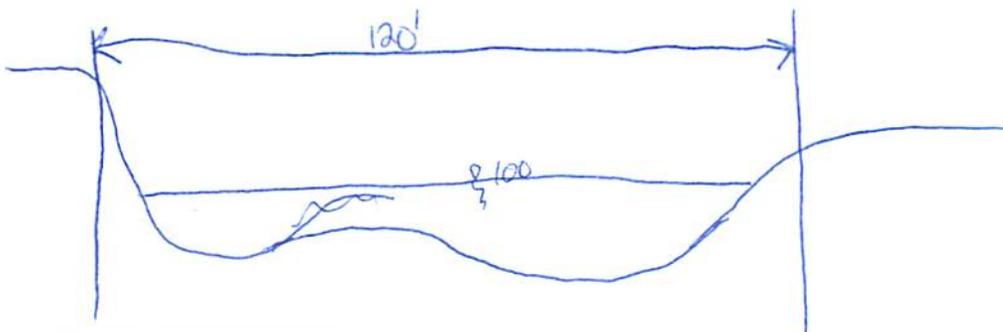
Bridge Structure No. 52384316 Date 11/13/10 Initials CW Region (A B C D) A  
 Site \_\_\_\_\_ Location Park Dr over Rapid Cr  
 $Q_{100} = \underline{4630}$  by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 4630 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 114 ft. Flow angle at bridge = 0° Abut. Skew = 0° Effective Skew = 0°  
 Width ( $W_2$ ) iteration = 114  
 Avg. flow depth at bridge,  $y_2$  iteration = 5.5 On vert Abut  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 114 ft\*  $q_2 = Q_2/W_2 = \underline{40.6}$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = \underline{7.4}$  ft/s Final  $y_2 = q_2/V_2 = \underline{5.5}$  ft  $\Delta h = \underline{1.1}$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{6.6}$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 6.0 ft  
 n (Channel) = 0.080  
 n (LOB) = 0.035  
 n (ROB) = 0.035  
 Pier Width = 2.0 ft  
 Pier Length = 2.0 ft  
 # Piers for 100 yr = 2 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = \underline{120}$  ft  
 Width of left overbank flow at approach,  $W_{lob} = \underline{0}$  ft Average left overbank flow depth,  $y_{lob} = \underline{0}$  ft  
 Width of right overbank flow at approach,  $W_{rob} = \underline{0}$  ft Average right overbank flow depth,  $y_{rob} = \underline{0}$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) 2=0

Estimated bed material  $D_{50} = \underline{0.30}$  ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) = \underline{5.85}$  ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} = \underline{10.24}$  ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} = \underline{0.054}$  ft

If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{0}$

From Figure 10,  $y_{cs} = \underline{0.0}$  ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1.0

Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1.0}$

Froude # at bridge = 0.56

Using pier width  $a$  on Figure 11,  $\xi = \underline{8}$  Pier scour  $y_{ps} = \underline{7.3}$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{0}$  ft right abutment,  $y_{aRT} = \underline{0}$  ft

Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls,  $0.55$  for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{0}$  and  $\psi_{RT} = \underline{0}$

Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) = \underline{0}$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) = \underline{0}$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

6.6  
x 7.3

**SCOUR ANALYSIS AND REPORTING FORM**

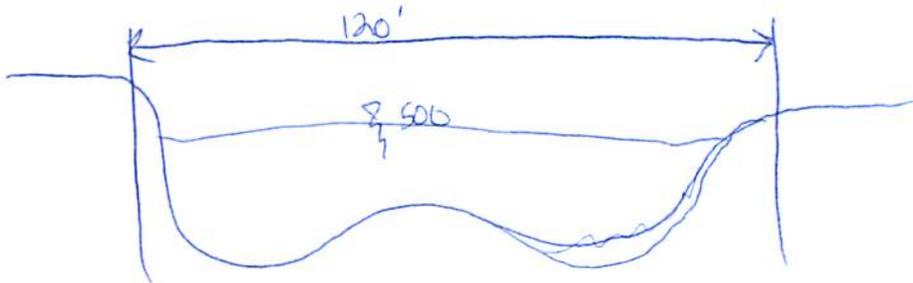
Bridge Structure No. 52384316 Date 11/13/10 Initials CW Region (A B C D)  
 Site \_\_\_\_\_ Location Park Dr over Rapid Cr  
 $Q_{500} =$  17400 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 5476 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 114 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = ~~114~~ \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = 11.3 RD Overflow \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 114 ft\*  $q_2 = Q_2/W_2 =$  48 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.0 ft/s Final  $y_2 = q_2/V_2 =$  6.0 ft  $\Delta h =$  1.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.3 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 6.0 ft  
 $n$  (Channel) = 0.030  
 $n$  (LOB) = 0.040 0.035  
 $n$  (ROB) = 0.040 0.035  
 Pier Width = 2.0 ft  
 Pier Length = 2.0 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  120 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) 2=0

Estimated bed material  $D_{50} =$  0.30 ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  6.25 ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  10.41 ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{cs0} = 0.0006 (q_2/y_1)^{7/6} =$  0.063 ft

If  $D_{50} \geq D_{cs0}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  0.0

From Figure 10,  $y_{cs} =$  0.0 ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0  
 Froude # at bridge = 0.58

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Using pier width  $a$  on Figure 11,  $\xi =$  4.0 Pier scour  $y_{ps} =$  7.3 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  0

Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment

Route Park Dr. Stream Rapid Creek MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 52384316 Location Park Dr over Rapid Creek  
 GPS coordinates: N 44° 03' 32.2" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 103° 17' 03.8" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_  
 Drainage area = 397.33 sq. mi. 10.7 29  
 The average bottom of the main channel was 10.7 ft below top of guardrail at a point 30 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal.  drainage area ratio \_\_\_ regional regression equations.

6139  
17400  
5476  
11724

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>4630</u>			Q <sub>500</sub> = <u>17400</u>		
Estimated flow passing through bridge	<u>4630</u>			<u>5476</u>		
Estimated road overflow & overtopping				<u>11924</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour? \_\_\_ Yes  No \_\_\_ Don't know  
 Debris Potential?  High \_\_\_ Med \_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_ Sand \_\_\_ Gravel \_\_\_ Cobbles  Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 Constructed channel common on L. side above bridge  
 Photos - 1477-1D 82 - L. Abut  
 78 - US 83 - Pier  
 79 - US RB 84 - R. Abut  
 80 - US LB 85 - US Face bridge  
 81 - other channel entrance

Summary of Results

	Q <sub>100</sub>	Q <sub>500</sub>
Bridge flow evaluated	<u>4630</u>	<u>5476</u>
Flow depth at left abutment (yaLT), in feet	<u>0.0</u>	<u>0.0</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>0.0</u>
Contraction scour depth (yca), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (yps), in feet	<u>7.3</u>	<u>7.3</u>
Left abutment scour depth (yas), in feet	<u>0.0</u>	<u>0.0</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<u>0.0</u>
IFlow angle of attack	<u>0°</u>	<u>0°</u>

See Comments/Diagram for justification where required