| | SCOUR ANALYSIS AND REPORTING FORM |
|----------------|--|
| | Bridge Structure No. 52399300 Date 4/1/11 Initials Ch Region (ABCD) |
| | Site Location W. Main St. over Rapit Creek |
| | Site Location <u>W. Main St. over Rapid Creek</u> Q ₁₀₀ = <u>4720</u> by: drainage area ratio flood freq. anal regional regression eq |
| | Bridge discharge $(Q_2) = 4720$ (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping) |
| | |
| | Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method Bridge Width = 310 ft.30 Flow angle at bridge = 20 ° Abut. Skew = 15 ° Effective Skew = 45 ° |
| , suon | Width (W_2) iteration = 310 242 246 |
| LD" | Avg. flow depth at bridge, y_2 iteration = 3.2 3.4 3.3 |
| egior | Corrected channel width at bridge Section = W_2 times cos of flow angle = $\frac{2811}{100}$ ft* $Q_2 = Q_2/W_2 = \frac{16}{100} \cdot \frac{1}{100}$ ft ² /s |
| or "RegionD" | Corrected channel width at bridge Section = W_2 times cos of flow angle = 281% ft* $q_2 = Q_2/W_2 = 16.6$ ft²/s Bridge Vel, $V_2 = 4.4$ ft/s Final $y_2 = q_2/V_2 = 3.3$ ft $\Delta h = 0.5$ ft |
| C", C | Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 3$ ft |
| RegionC", | * NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$ |
| Z S | If y 2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD, |
| | Water Surface Elev. = ft \\ \ \ 386' |
| | Low Steel Elev. = 9.9 ft |
| | n (Channel) = 0.045 |
| | n(LOB) = 0.035 |
| | n (ROB) = 0.055 Pier Width = 1.0 ft |
| | Pier Length = 73.0 ft |
| | # Piers for $100 \text{ yr} = \underline{5}$ ft |
| | |
| | CONTRACTION SCOUR |
| | Width of main channel at approach section $W_1 = 360$ ft Width of left querbank flow at approach $W_2 = 60$ ft |
| onua | Width of left overbank flow at approach, $W_{lob} = 0$ ft Average left overbank flow depth, $y_{lob} = 0$ ft |
| OKM. Contract | Width of right overbank flow at approach, $W_{rob} = 0$ ft Average right overbank flow depth, $y_{rob} = 0$ ft |
| 25 | Live Bed Contraction Scour (use if bed material is small cobbles or finer) |
| | $x =$ From Figure 9 W_2 (effective) = ft y_{cs} = ft |
| | |
| × 1 | Clear Water Contraction Scour (use if bed material is larger than small cobbles) |
| NIC | Estimated bed material $D_{50} = 0.3$ ft Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = 3.27$ ft/s |
| 3 | Critical approach velocity, $Vc = 11.52y_1^{-10}D_{50}^{-10} = 11.52y_1^{-10}D_{50}^{-10} = 11.52y_1^{-10}D_{50}^{-10}$ |
| UKWI. CWCSINEW | If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above. |
| 2 | $\begin{array}{c} D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = \underline{\ \ \ \ \ \ \ \ \ \ \ } \\ Otherwise, \ \chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 = \underline{\ \ \ \ \ \ \ \ \ \ \ } \\ & From \ Figure \ 10, \ y_{cs} = \underline{\ \ \ \ \ \ \ \ \ \ \ } \\ & ft \end{array}$ |
| | Otherwise, $\chi = 0.122 y_1 [q_2/(D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =ft$ |
| | |
| Ž. | PIER SCOUR CALCULATIONS Correction for flow and a fattack (from Table 1) V2 = 1.5 |
| GRIMI. PIET | L/a ratio = $\frac{73}{100}$ Correction factor for flow angle of attack (from Table 1), K2 = $\frac{1.5}{100}$ Correction factor for flow angle of attack (from Table 1), K2 = $\frac{1.5}{100}$ Froude # at bridge = $\frac{0.44}{1000}$ Pier scour $y_{ps} = \frac{6.5}{1000}$ ft |
| 4 | Froude # at orange = $\frac{0.776}{0.000}$ Using piet within a on Figure 11, $\zeta = \frac{9}{1.000}$ Fiet scoul $y_{ps} = \frac{6.000}{0.000}$ It |
| Ħ | ABUTMENT SCOUR CALCULATIONS |
| JONN. Abutment | Average flow depth blocked by: left abutment, $y_{aLT} = 0$ ft right abutment, $y_{aRT} = 6$ ft |
| . A0 | Shape coefficient K_1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through |
| N N | Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = 0.0$ and $\psi_{RT} = 0.0$ the labutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 0.0$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 0.0$ ft |
| L | Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 0.00$ It Kight abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 0.00$ It |

| Route W. Main 5t. Stream Rapid Cree Bridge Structure No. 52399300 Low | ek | MRM | Da | te 4/1/1 | / Initi | ials Ch | | |
|--|---------------|---------------|-------------|--------------------|---------------|-------------|--|--|
| Bridge Structure No. 52399.300 Loc | cation W. | Main St. | over I | Rapid (| creek | | | |
| GPS coordinates: $4.460454.0''$ taken from: USL abutment \times centerline of \cap MRM end Datum of coordinates: WGS84 NAD27 | | | | | | | | |
| Drainage area = $\frac{408.66}{1000}$ sq. mi. | | | | | | | | |
| | | | | | | | | |
| The average bottom of the main channel was 15.4 ft below top of guardrail at a point 180 ft from left abutment. | | | | | | | | |
| Method used to determine flood flows:Freq. Analdrainage area ratioregional regression equations. | | | | | | | | |
| MISCELLANEOUS CONSIDERATIONS | | | | | | | | |
| Flows | $Q_{100} =$ | 4720 | EKATIO | Q ₅₀₀ = | 17700 | | | |
| Estimated flow passing through bridge | 4720 | | | 2500 7700 | | | | |
| Estimated flow passing through bridge Estimated road overflow & overtopping | | 1120 | | 17700 | | | | |
| Consideration | Yes | No | Possibly | Yes | No | Possibly | | |
| Chance of overtopping | 103 | X | 1 0551019 | 1 65 | X | Possibly | | |
| Chance of Pressure flow | | ~ | | | $\overline{}$ | | | |
| Armored appearance to channel | | \$ | | | ~ | | | |
| Lateral instability of channel | | 7 | | | \ | | | |
| Lateral histability of chamics | | | | 1 | /\ | | | |
| Pinner et abutmente? | | | | | | | | |
| Riprap at abutments?YesX_NoMarginal | | | | | | | | |
| Evidence of past Scour?YesX_NoDon't know | | | | | | | | |
| Debris Potential?HighMedLow | | | | | | | | |
| | | | | | | | | |
| Does scour countermeasure(s) appear to have been designed? | | | | | | | | |
| Riprap Yes No Don't know NA | | | | | | | | |
| Spur Dike Yes No X Don't know NA | | | | | | | | |
| Other Yes No Don't know X NA | | | | | | | | |
| IESNODON I KNOWNA | | | | | | | | |
| Red Material | Classificatio | n Dagad on Ma | dian Dartia | la Siza (D.) | | | | |
| Bed Material Classification Based on Median Particle Size (D ₅₀) | | | | | | | | |
| Material Silt/Clay Sand | | | | Cobbles Boulders | | | | |
| Size range, in mm < 0.062 0.062-2. | .00 | 2.00-64 | | 64-250 | | >250 | | |
| | | | | | | | | |
| Comments, Diagrams & orientation of digital phot | os | | | | | | | |
| Thotos_ | | | | 33- | Approx | ch XS bokin | | |
| 1523 - Brdge 1D | 29-1. A | but | | | | | | |
| 211 114 | 20 116 | Face bridge | | | 1eft | | | |
| 24- US | 30- W | race of large | | | | | | |
| 25 - USRB | 100 | ting right | | | | | | |
| 26-4518 | | | | | | | | |
| | | | | 1 | | | | |
| 28- US Face bridge looking left | 32-Appro | rach X5 look | ing righ | <i>T</i> | | | | |
| Summary of Results | V.V. | | , , | | | | | |
| | | Q100 | | | Q500 | | | |
| Bridge flow evaluated | 4720 | | | 17700 | | | | |
| Flow depth at left abutment (yaLT), in feet | C | 0.0 | | | 0.0 | | | |
| Flow depth at right abutment (yaRT), in feet | 0.0 | | | 0.0 | | | | |
| Contraction scour depth (ycs), in feet | 0.0 | | | 0.0 | | | | |
| Pier scour depth (yps), in feet | 6.5 | | | 6.8 | | | | |
| Left abutment scour depth (yas), in feet | 0.0 | | | 0,0 | | | | |
| Right abutment scour depth (yas), in feet 0.0 | | | | | | | | |
| 1Flow angle of attack | 5° | | | 5° | | | | |