	Bridge Structure No. 52414299 Date 4/1/11 Initials Character Region (QBCD)						
	Site Location 5th St over Rapid Creek						
	$Q_{100} = 4780$ by: drainage area ratio flood freq. anal. regional regression eq.						
	Bridge discharge $(Q_2) = \underline{4790}$ (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)						
PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method Bridge Width = 172 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 ° Width (W ₂) iteration = 173 + 159 164 166 166 Avg. flow depth at bridge, y ₂ iteration = 16 16						
	# Piers for $100 \text{ yr} = 3 \text{ ft}$						
	CONTRACTION SCOUR						
	Width of main channel at approach section $W_1 = 200$ ft						
tract	Width of left overbank flow at approach, $W_{lob} = \bigcirc, \bigcirc$ ft Average left overbank flow depth, $y_{lob} = \bigcirc, \bigcirc$ ft						
PGRM: Contract	Width of right overbank flow at approach, $W_{rob} = 0.3$ ft O						
PGR	Live Bed Contraction Scour (use if bed material is small cobbles or finer)						
	$x =$ ft $y_{cs} =$ ft						
PGRM: CWCSNEW	Clear Water Contraction Scour (use if bed material is larger than small cobbles) Estimated bed material $D_{50} = 0.3$ ft Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = 0.00/(y_1W_1) = 0.00/(y_1W_1)$ ft/s Critical approach velocity, $V_1 = Q_{100}/(y_1W_1) = 0.00/(y_1W_1) = 0.00/(y_1W_1)$ ft/s If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above. $D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = 0.00/(y_1W_1) = 0.0$						
	in the first is the first in t						
: Pier	PIER SCOUR CALCULATIONS						
PGRM: Pier	L/a ratio = $\frac{71}{1}$ Correction factor for flow angle of attack (from Table 1), K2 = $\frac{2 \cdot 0}{1}$ Correction factor for flow angle of attack (from Table 1), K2 = $\frac{2 \cdot 0}{1}$ Pier scour $y_{ps} = \frac{8 \cdot 8}{1}$ ft						
Ħ	ABUTMENT SCOUR CALCULATIONS						
PGRM: Abutment	Average flow depth blocked by: left abutment, $y_{aLT} = 0$, 0 , ft right abutment, $y_{aRT} = 0$, 0 , ft Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through Using values for y_{aLT} and y_{aRT} on figure 12, $y_{LT} = 0$, 0 and $y_{RT} = 1.4$ Left abutment scour, $y_{as} = y_{LT}(K_1/0.55) = 0$, ft Right abutment scour $y_{as} = y_{RT}(K_1/0.55) = 1.4$ ft						

	SCOUR ANALYSIS AND REPORTING FORM	
	Bridge Structure No. 52414299 Date 4/1/11 Initials CW Region (ABCD)	
	Site Location 5th St over Rapid Creek	
	Q ₅₀₀ = 18000 by: drainage area ratio flood freq. anal. regional regression eq	
	Bridge discharge $(Q_2) = 14067$ (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)	
PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method Bridge Width = $1/2$ ft. Flow angle at bridge = $1/0$ ° Abut. Skew = 0 ° Effective Skew = $1/0$ ° Width (W ₂) iteration = $1/2$ Avg. flow depth at bridge, y ₂ iteration = $1/2$ Avg. flow depth at bridge Section = W ₂ times cos of flow angle = $1/2$ ft $1/2$ Corrected channel width at bridge Section = W ₂ times cos of flow angle = $1/2$ ft $1/2$	
	Water Surface Elev. =ft	
	Low Steel Elev. = $\frac{6.1}{0.050}$ ft 172 1.5	1.
	$n \text{ (LOB)} = \underbrace{0.030}_{5}$	1
	n (ROB) = 6.033	-
	Pier Width = $\frac{1}{1}$ $\frac{0}{1}$ ft Pier Length = $\frac{1}{1}$ $\frac{0}{1}$ ft	
	# Piers for $500 \text{ yr} = 3 \text{ ft}$	
	CONTRACTION SCOUR	
	Width of main channel at approach section $W_1 = 200$ ft	
act	Width of left overbank flow at approach, $W_{lob} = \frac{172}{172}$ ft Average left overbank flow depth, $y_{lob} = \frac{1}{192}$	ft
PGRM: Contract	Width of right overbank flow at approach, $W_{rob} = \frac{1}{12}$ ft Average right overbank flow depth, $y_{rob} = \frac{4}{9}$ ft	
.₩	With or right overdank flow at approach, wrob	
PGF	Live Bed Contraction Scour (use if bed material is small cobbles or finer)	
	$x =$ ft $y_{cs} =$ ft	
PGRM: CWCSNEW		=0
ie	PIER SCOUR CALCULATIONS	
PGRM: Pie	L/a ratio = 7/ Correction factor for flow angle of attack (from Table 1), K2 = 2.0	
PGR	L/a ratio = $\frac{7}{2}$ Correction factor for flow angle of attack (from Table 1), K2 = $\frac{2}{2}$. Using pier width a on Figure 11, $\xi = \frac{4}{2}$. Pier scour $y_{ps} = \frac{9}{2}$. It	
PGRM: Abutment	ABUTMENT SCOUR CALCULATIONS Average flow depth blocked by: left abutment, $y_{aLT} = 3.0$ ft right abutment, $y_{aRT} = 4.9$ ft Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = 11.5$ and $\psi_{RT} = 14.8$ Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 11.5$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 14.8$ ft	
PGRA	Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 11.5$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 14.8$ ft	

Route 5th St Stream Rapid	Creek	MRM	Da	te 4/1/	// Init	tials CG					
Route 5th St Stream Rapid Creek MRM Date 4/1/11 Initials C4 Bridge Structure No. 52414299 Location 5th St over Rapid Creek											
GPS coordinates: N 440 051 06 5"	taken from:	LISI abutmen	X	centerline o	of I MRM	end					
GPS coordinates: N 440 05' 05.5" W 103° 13' 26.3"	Datum of co	oordinates: W	GS84	NAD27	of it ivitativi						
Drainage area = $\frac{416.90}{}$ se				-							
The average bottom of the main channel was 13.7 ft below top of guardrail at a point 100.0 ft from left abutment.											
Method used to determine flood flows:Freq. Analdrainage area ratioregional regression equations.											
MISCELLANEOUS CONSIDERATIONS											
Flows	$Q_{100} =$	$Q_{100} = 4780$			$Q_{500} = 18000$						
Estimated flow passing through bridge		4780			14067						
Estimated road overflow & overtopping	17				3933						
Consideration	Yes	No	Possibly	Yes	No	Possibly					
Chance of overtopping		X		→							
Chance of Pressure flow		X		^	Y						
Armored appearance to channel		*			\rightarrow						
Lateral instability of channel											
Riprap at abutments? Yes X No Marginal											
Evidence of past Scour? Yes X No Don't know											
Debris Potential?HighMedLow											
Does scour countermeasure(s) appear to have been designed?											
	Yes N	No Dor	i't know	NA							
A PRIATE											
The state of the s											
Other											
Bed Ma	nterial Classification	on Based on Me	edian Particl	e Size (Dso)							
		Gravel X			Cobbles Boulders						
		.00 2.00-64			E_4364616A35400A36463A						
Size range, in mm <0.062 0.0	362-2.00	2.00-04		64-250		>250					
Comments, Diagrams & orientation of digita	l photos										
Droto				11 1							
40	o-USRB		45- R.	Abut							
1535- 15 11 ARB 11	1-11/13										
36- App X)	1 015 215	PR									
1535- 1D 36- App X5 @ RB 37- US Face Bridgy 42- Pond on RB 38- App X5 @ LB 39- US LB 43 - Pond on RB 39- US LB 44- L. Abut											
38- ADD X5@ LB 43	5 - Yourd on	KB									
39-1151 B 115 41	t- 1. Abut										
	1 21 1011										
Summary of Results											
		Q100			Q500						
Bridge flow evaluated	4	4780			14067						
Flow depth at left abutment (yaLT), in feet		0.0			3,0						
Flow depth at right abutment (yaRT), in feet		0.3			4.9						
Contraction scour depth (ycs), in feet		0.0			0,0						
Pier scour depth (yps), in feet	4	4.4			9,1						
Left abutment scour depth (yas), in feet	0	0.0			11,5						
Right abutment scour depth (yas), in feet		1.4			14.9						

See Comments/Diagram for justification where required



1Flow angle of attack