

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 52419299 Date 4/4/11 Initials CLW Region (A B C D)

Site \_\_\_\_\_ Location East Boulevard over Rapid Creek

$Q_{100} =$  4800 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_

Bridge discharge ( $Q_2$ ) = 4800 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 210 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °

Width ( $W_2$ ) iteration = 210 163 163

Avg. flow depth at bridge,  $y_2$  iteration = 4.0 4.6 4.6

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 162.38 ft\*  $q_2 = Q_2/W_2 =$  29.6 ft<sup>2</sup>/s

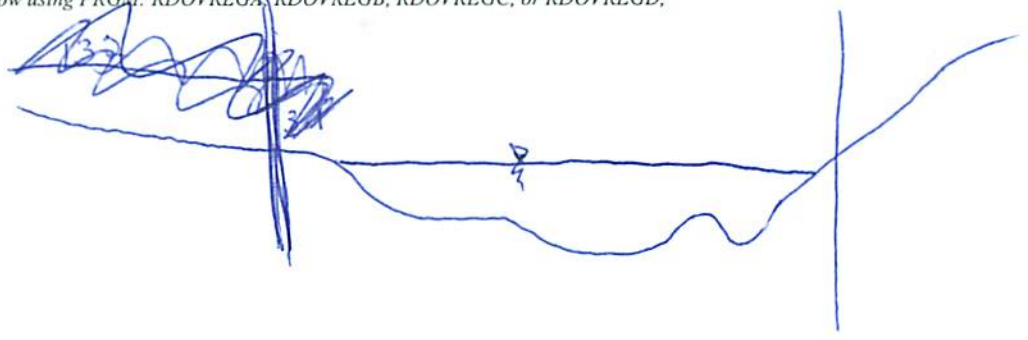
Bridge Vel,  $V_2 =$  6.4 ft/s Final  $y_2 = q_2/V_2 =$  4.6 ft  $\Delta h =$  0.8 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  5.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(a) + a \cos(a)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
Low Steel Elev. = ~~\_\_\_\_\_~~ ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
Pier Width = 1.25 ft  
Pier Length = 80 ft  
# Piers for 100 yr = 3 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  210 ft

Width of left overbank flow at approach,  $W_{lob} =$  132 ft 0 Average left overbank flow depth,  $y_{lob} =$  1.55 ft 0.0

Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) 2=0

Estimated bed material  $D_{50} =$  0.2 ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  4.23 ft/s 2=234

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  8.65 ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  0.0425 ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0.0 ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 64 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.5

Froude # at bridge = 0.53 Using pier width  $a$  on Figure 11,  $\xi =$  5.6 Pier scour  $y_{ps} =$  7.7 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0.0 ft right abutment,  $y_{aRT} =$  0.0 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0.0 and  $\psi_{RT} =$  0.0

Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  0.0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  0.0 ft

1.55  
2/3.1  
1.6

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment



**SCOUR ANALYSIS AND REPORTING FORM**

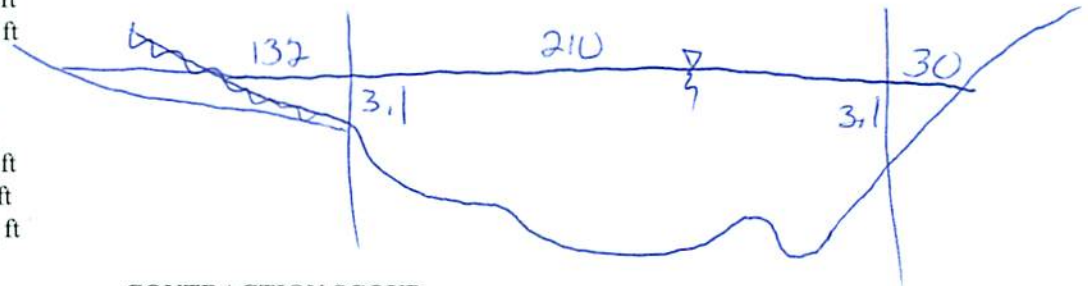
Bridge Structure No. 52419299 Date 4/4/11 Initials CV Region (A B C D)  
 Site \_\_\_\_\_ Location East Boulevard over Rapid Creek  
 $Q_{500} =$  18100 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 18100 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 210 ft. Flow angle at bridge = 5° Abut. Skew = 0° Effective Skew = 5°  
 Width ( $W_2$ ) iteration = 210 190 201 200  
 Avg. flow depth at bridge,  $y_2$  iteration = 8.3 8.8 8.5 8.5  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 199.24 ft\*  $q_2 = Q_2/W_2 =$  90.8 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  10.7 ft/s Final  $y_2 = q_2/V_2 =$  8.5 ft  $\Delta h =$  2.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  10.9 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = \_\_\_\_\_ ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 1.25 ft  
 Pier Length = 86 ft  
 # Piers for 500 yr = 3 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  210 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  132 ft Average left overbank flow depth,  $y_{lob} =$  1.55 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  30 ft Average right overbank flow depth,  $y_{rob} =$  1.55 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) 2=0

Estimated bed material  $D_{50} =$  0.12 ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  7.11 ft/s 4.46 = 2.346

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  9.73 ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  0.1051 ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0.0 ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 64 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.5  
 Froude # at bridge = 0.65 Using pier width  $a$  on Figure 11,  $\xi =$  5.6 Pier scour  $y_{ps} =$  7.9 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  1.55 ft right abutment,  $y_{aRT} =$  1.55 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  6.4 and  $\psi_{RT} =$  6.4  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  6.4 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  6.4 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route East Boulevard Stream Rapid Creek MRM Date 4/4/11 Initials CL  
 Bridge Structure No. 52419299 Location East Boulevard over Rapid Creek  
 GPS coordinates: N 44° 04' 53.1" taken from: USL abutment X centerline of MRM end \_\_\_\_\_  
W 103° 12' 52.9" Datum of coordinates: WGS84 X NAD27 \_\_\_\_\_  
 Drainage area = 419.57 sq. mi.  
 The average bottom of the main channel was 19.1 ft below top of guardrail at a point 86.0 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. ✓ drainage area ratio \_\_\_\_\_ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>4800</u>			Q <sub>500</sub> = <u>18100</u>		
Estimated flow passing through bridge	<u>4800</u>			<u>18100</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<u>X</u>			<u>X</u>	
Chance of Pressure flow		<u>X</u>			<u>X</u>	
Armored appearance to channel		<u>X</u>			<u>X</u>	
Lateral instability of channel		<u>X</u>			<u>X</u>	

Riprap at abutments? \_\_\_\_\_ Yes \_\_\_\_\_ No X Marginal L-Yes R-No  
 Evidence of past Scour? X Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  
 Debris Potential? X High \_\_\_\_\_ Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?

Riprap X Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know X NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know X NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_\_\_ Sand \_\_\_\_\_ Gravel X Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Photos

1546- ID  
 47- US  
 48- RBUS  
 49- LBUS  
 50- ID

~~51- R. Abut~~ L. Abut  
~~52- R. Abut~~ L. Abut  
 53- # R. Abut  
 54- US Face bridge  
 55- R. Abut

56- Gate @ R. Abut  
 57- New channel on RB  
 58- US face bridge  
 59- US face bridge

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>4800</u>	<u>18100</u>
Flow depth at left abutment (yaLT), in feet	<u>0.0</u>	<u>1.55</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>1.55</u>
Contraction scour depth (yca), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (yps), in feet	<u>7.7</u>	<u>7.9</u>
Left abutment scour depth (yas), in feet	<u>0.0</u>	<del>1.55</del> <u>6.4</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<del>1.55</del> <u>6.4</u>
IFlow angle of attack	<u>5</u>	<u>5</u>

See Comments/Diagram for justification where required