

OK 72

SCOUR ANALYSIS AND REPORTING FORM

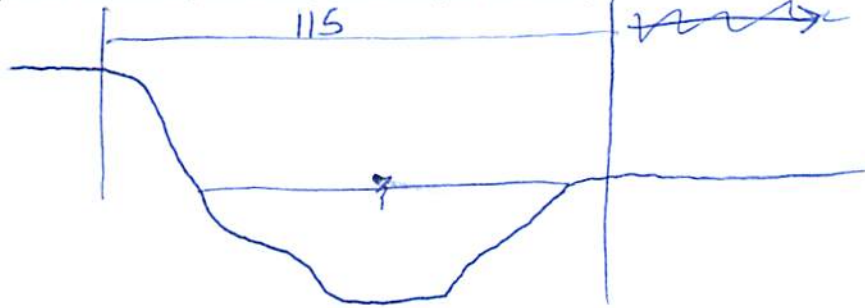
Bridge Structure No. 52435310 Date 4/15/11 Initials CW Region (A B C D)
Site Location SD 238 / St. Patrick St over Rapid creek
Q100 = 4830 by: drainage area ratio [checked] flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 4830 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 110 ft. Flow angle at bridge = 15 degrees Abut. Skew = 0 degrees Effective Skew = 15 degrees
Width (W2) iteration = 110 100 102
Avg. flow depth at bridge, y2 iteration = 5.8 6.1 6.1
Corrected channel width at bridge Section = W2 times cos of flow angle = 101.25 ft\* 98.52 q2 = Q2/W2 = 47.5 ft^2/s
Bridge Vel, V2 = 8.1 ft/s Final y2 = q2/V2 = 6.1 ft Delta h = 1.3 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 7.4 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = ft
Low Steel Elev. = 10.5 ft
n (Channel) = 0.035 0.040
n (LOB) = 0.033
n (ROB) = 0.033
Pier Width = 1.03 1.0 ft
Pier Length = 63 ft
# Piers for 100 yr = 2



CONTRACTION SCOUR

Width of main channel at approach section W1 = 115 ft
Width of left overbank flow at approach, Wlob = 0 ft Average left overbank flow depth, ylob = 0 ft
Width of right overbank flow at approach, Wrob = 0 ft Average right overbank flow depth, yrob = 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = From Figure 9 W2 (effective) = ft ycs = ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = 0.20 ft Average approach velocity, V1 = Q100/(y1 W1) = 5.68 ft/s
Critical approach velocity, Vc = 11.52 y1^(1/6) D50^(1/3) = 9.12 ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^(7/6))^3 = 0.0640 ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [q2 / (D50^(1/3) y1^(7/6))]^(6/7) - y1 = From Figure 10, ycs = 0.0 ft

PIER SCOUR CALCULATIONS

L/a ratio = 63 Correction factor for flow angle of attack (from Table 1), K2 = 2.5
Froude # at bridge = 0.54 Using pier width a on Figure 11, xi = 4.9 Pier scour yps = 11.2 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 0 ft right abutment, yaRT = 0 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = 0 and psiRT = 0
Left abutment scour, yas = psiLT (K1/0.55) = 0 ft Right abutment scour, yas = psiRT (K1/0.55) = 0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"
PRGM: Contract
PRGM: CWCSNEW
PRGM: Pier
PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

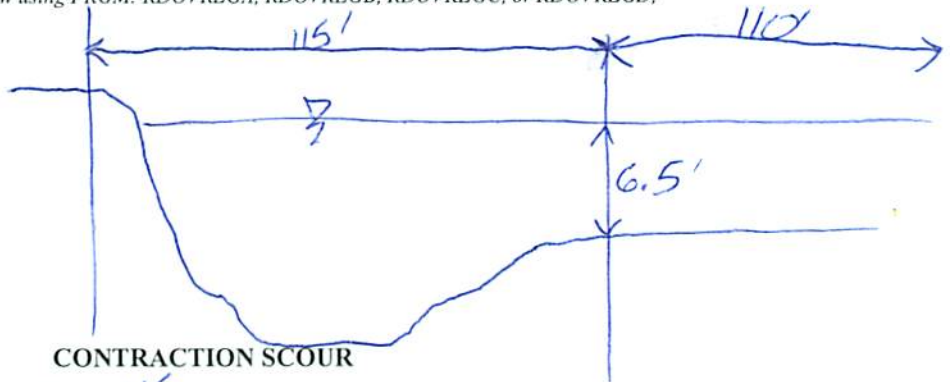
Bridge Structure No. 52435310 Date 4/15/11 Initials CLW Region (A B C D)  
 Site \_\_\_\_\_ Location SD 238/St. Patrick St. over Rapid Creek  
 $Q_{500} =$  18200 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 14165 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 110 ft. Flow angle at bridge = 15 ° Abut. Skew = 0 ° Effective Skew = 15 °  
 Width ( $W_2$ ) iteration = 110  
 Avg. flow depth at bridge,  $y_2$  iteration = 12 > 10.5 → RD Overflow  $110 \cos 15 = 106.25$   
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 106.25 ft\*  $q_2 = Q_2/W_2 = \frac{14165}{106.25} = 133.3$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  12.7 ft/s Final  $y_2 = q_2/V_2 = \frac{133.3}{12.7} = 10.5$  ft  $\Delta h =$  3.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  13.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 10.5 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.033  
 $n$  (ROB) = 0.033  
 Pier Width = 1.0 ft  
 Pier Length = 63 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  115 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  110 ft Average right overbank flow depth,  $y_{rob} =$  6.5 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  0.20 ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) = \frac{18200}{13.8 \times 115} = \frac{18200}{1587} = 11.47$  ft/s  $z = \frac{4.56}{11.47} = 0.398$   
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} = 10.12$  ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 = 0.1456$  ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0.0 ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 63 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  2.5  
 Froude # at bridge = 0.69 Using pier width  $a$  on Figure 11,  $\xi =$  4.9 Pier scour  $y_{ps} =$  11.5 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  6.5 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  17.7  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  17.7 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

SD HWY238/

Route St. Patrick Stream Rapid Creek MRM \_\_\_\_\_ Date 4/15/11 Initials CL  
 Bridge Structure No. 52435310 Location SD238/St Patrick St over Rapid Creek  
 GPS coordinates: N 44° 04' 03.3" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 103° 10' 49.9" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_  
 Drainage area = 423.38 sq. mi. 15.7  
 The average bottom of the main channel was 14.0 ft below top of guardrail at a point 89 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio \_\_\_\_\_ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>4830</u>			Q <sub>500</sub> = <u>18200</u>		
Estimated flow passing through bridge	<u>4830</u>			<u>14165</u>		
Estimated road overflow & overtopping				<u>4035</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know Upstream  
 Debris Potential?  High \_\_\_\_\_ Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?

Riprap  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_\_\_ Sand \_\_\_\_\_ Gravel  Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Photos  
 1557-1D  
 88- US  
 89- US RB  
 90- US LB  
 91- US R, Abut.  
 92- US R, Abut  
 93- US L, Abut  
 94- US L, Abut  
 95- US face of bridge  
 96- App XS RB  
 97- App XS  
 98- App XS LB

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>4830</u>	<u>14165</u>
Flow depth at left abutment (yaLT), in feet	<u>0.0</u>	<u>0.0</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>6.5</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>11.7</u>	<u>11.5</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>0.0</u>	<u>0.0</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>0.0</u>	<u>17.7</u>
Flow angle of attack	<u>15°</u>	<u>15°</u>

See Comments/Diagram for justification where required