	SCOUR ANALYSIS AND REPORTING FORM						
	Bridge Structure No. 52450271 Date 8/31/12 Initials 201 Region (BBCD)						
PGRM "Regio	Site Location $E K Vale Rd + Box Elder CK in RC Q_{100} = 4650$ by: drainage area ratio flood freq. anal. regional regression eq. \times						
	Q ₁₀₀ = 4650 by: drainage area ratio flood freq. anal. regional regression eq.						
	Bridge discharge $(Q_2) = 4650$ (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)						
	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method Bridge Width = 63 ft. Flow angle at bridge = 55 ° Abut. Skew = 20 ° Effective Skew = 35 °						
	Width (W_2) iteration = $6.7.99$ Avg. flow depth at bridge, y_2 iteration = 7.3						
	Avg. now depth at bridge, y_2 iteration = $\frac{1}{2}$						
	Corrected channel width at bridge Section = W_2 times cos of flow angle = 6.799 ft* $q_2 = Q_2/W_2 = 6.4$ ft²/s Bridge Vel, $V_2 = 9.4$ ft/s Final $y_2 = q_2/V_2 = 1.3$ ft $\Delta h = 1.4$ ft Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 9.4$ ft						
	Bridge Vel, $V_2 = \frac{T_1 V}{1}$ ft/s Final $y_2 = q_2/V_2 = \frac{T_1 V}{1}$ ft $\Delta h = \frac{T_1 V}{1}$ ft						
	Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \frac{7}{1}$ ft * NOTE: repeat above calculations until y 2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$						
	* NOTE: repeat above calculations until y_1 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$ If y_1 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,						
	insteadile						
	Water Surface Elev. = $\frac{d}{9.5}$ ft Assume interest 160 68 Low Steel Elev. = $\frac{9.5}{9.5}$ ft See Asst						
	Water Surface Elev. = $\frac{4}{9.5}$ ft $\frac{4}{5}$ ft $\frac{4}{$						
	Pier Width = 443 0.95 ft Pier Length = 65 1.25 ft						
	# Piers for 100 yr = $\underline{\qquad}$ ft						
	CONTRACTION SCOUR						
PGRM: Contract	Width of main channel at approach section $W_1 = 69$ ft						
	Width of left overbank flow at approach, $W_{lob} = 60$ ft Average left overbank flow depth, $y_{lob} = 60$ ft						
	Width of right overbank flow at approach, $W_{rob} = \underline{\hspace{1cm}}$ ft Average right overbank flow depth, $y_{rob} = \underline{\hspace{1cm}}$ ft						
PGF	Live Bed Contraction Scour (use if bed material is small cobbles or finer)						
	$x = 0.37$ From Figure 9 W_2 (effective) = 66, 3 ft $y_{cs} = 0.6$ ft						
≥	Clear Water Contraction Scour (use if bed material is larger than small cobbles)						
SN	Estimated bed material $D_{50} = ft/s$ Average approach velocity, $V_1 = O_{100}/(v_1 W_1) = ft/s$						
	Critical approach velocity, $Vc = 11.17y_4^{1/6}D_{50}^{1/3} =ft/s$						
Σ	If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.						
PGR							
	$\begin{split} D_{c50} &= 0.0006 (q_2/y_1^{7/6})^3 = \underbrace{\qquad \qquad \qquad }_{ft} \\ Otherwise, \ \chi &= 0.122 y_1 [\dot{q}_2/(D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underbrace{\qquad \qquad }_{ft} \\ \end{split}$						
i ci							
	PIER SCOUR CALCULATIONS 1.05						
S.E.M	Froude # at bridge = 0.61 PIER SCOUR CALCULATIONS Correction factor for flow angle of attack (from Table 1), K2 = 0.61 Using pier width a on Figure 11, $\xi = 0.61$ Pier scour $y_{ps} = 0.61$ ft						
P	Pier scour $y_{ps} = 1$ tt						
GKM: Abutment	ABUTMENT SCOUR CALCULATIONS						
	Average flow depth blocked by: left abutment, $y_{aLT} = 0$, ft right abutment, $y_{aRT} = 0$						
Ab	Shape coefficient K_1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through						
MA	Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \frac{3}{12}$ and $\psi_{RT} = \frac{3}{12}$						
<u> </u>	Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = \frac{3}{100}$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = \frac{3}{100}$ ft						

SCOUR ANALYSIS AND REPORTING FORM

75hz1'hh 52151'201

> 5.4 , b 0201 1782 , Lilih

> > 115/11- Onohoe

Route Elk Vale Rd Stream Box Elder Bridge Structure No. 5245 0271 Log GPS coordinates: N440 7 24.31 W 103 09 4.61 Drainage area = 160,57 sq. mi. The average bottom of the main channel was 13 Method used to determine flood flows: Freq.	taken from: Datum of co	USL abutmer ordinates: W	$\frac{1}{1}$ $\frac{1}$	t 50	ck f îl MRM	end			
MISCELLANEOUS CONSIDERATIONS 7/3									
Flows	$Q_{100} =$	46 50	DERMITO	Q ₅₀₀ =	1090	0			
Estimated flow passing through bridge	₹100	4650		7 55 Z		2 (15)			
Estimated now passing through order Estimated road overflow & overtopping					224	2 101			
Consideration	Yes	No	Possibly	Yes	No	Possibly	10 912		
Chance of overtopping	103	X	1 0331019	7	140	Tossibly	25 1840		
Chance of Pressure flow		×					50 3010		
Armored appearance to channel		0		X_	~		50 3010 100 4620		
Lateral instability of channel		2			-		Joe 108:00		
Riprap at abutments? Yes No Marginal Evidence of past Scour? Debris Potential? High Med Low Does scour countermeasure(s) appear to have been designed? Riprap Xes No Don't know NA Spur Dike Yes No Don't know NA Other Yes No Don't know NA Bed Material Classification Based on Median Particle Size (D50) Material Silt/Clay Sand Gravel Cobbles Boulders Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250 Comments, Diagrams & orientation of digital photos									
Summary of Results		0100		 	0500		1		
Deides Community 1	Q100			Q500			-		
Bridge flow evaluated	4650			7552			-		
Flow depth at left abutment (yaLT), in feet	0.7			3.9			-		
Flow depth at right abutment (yaRT), in feet	G			2.1					
Contraction scour depth (ycs), in feet	C. 6			2,9					
Pier scour depth (yps), in feet		4			4,1		-		
Left abutment scour depth (yas), in feet	0.7			13./			1		

35

8.6

35

Right abutment scour depth (yas), in feet

1Flow angle of attack